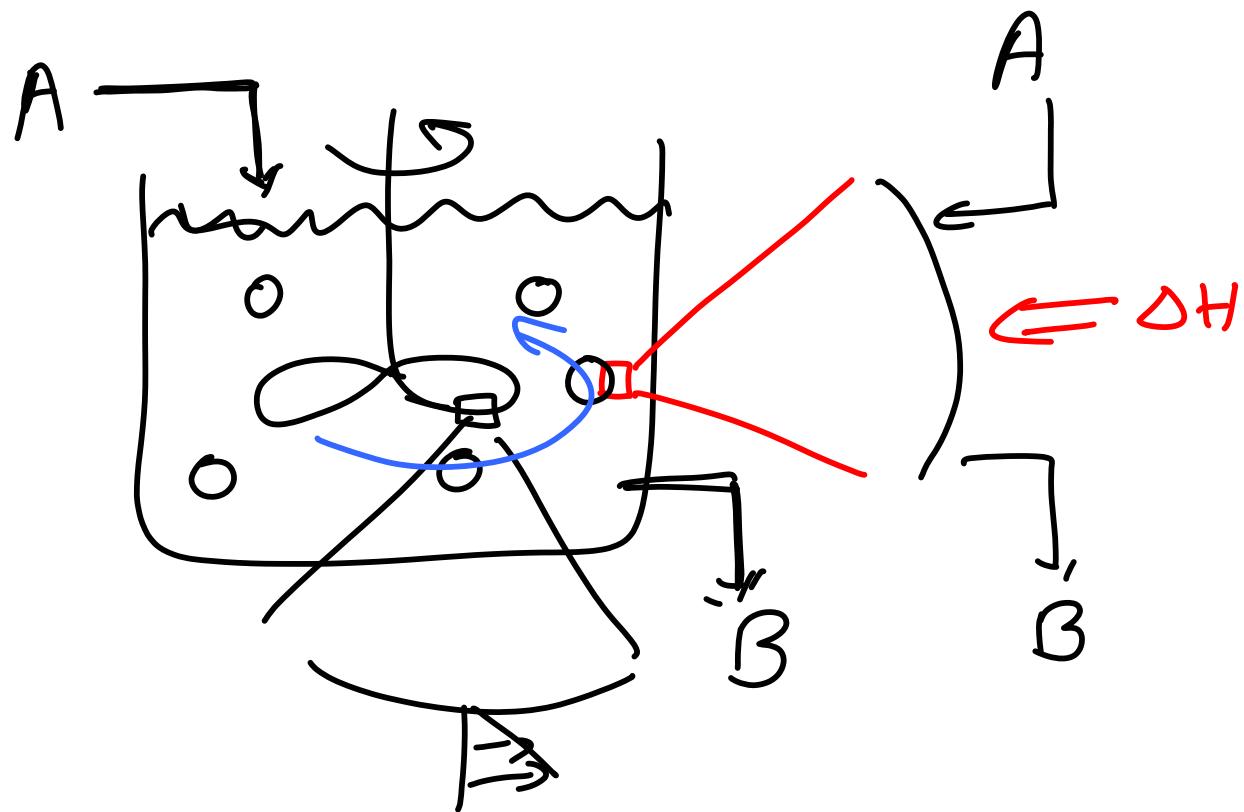
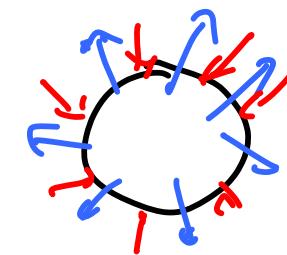
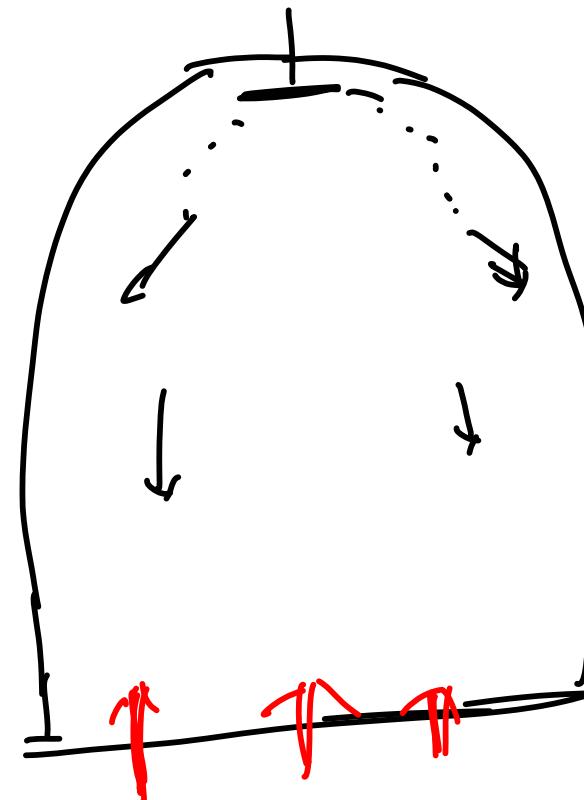
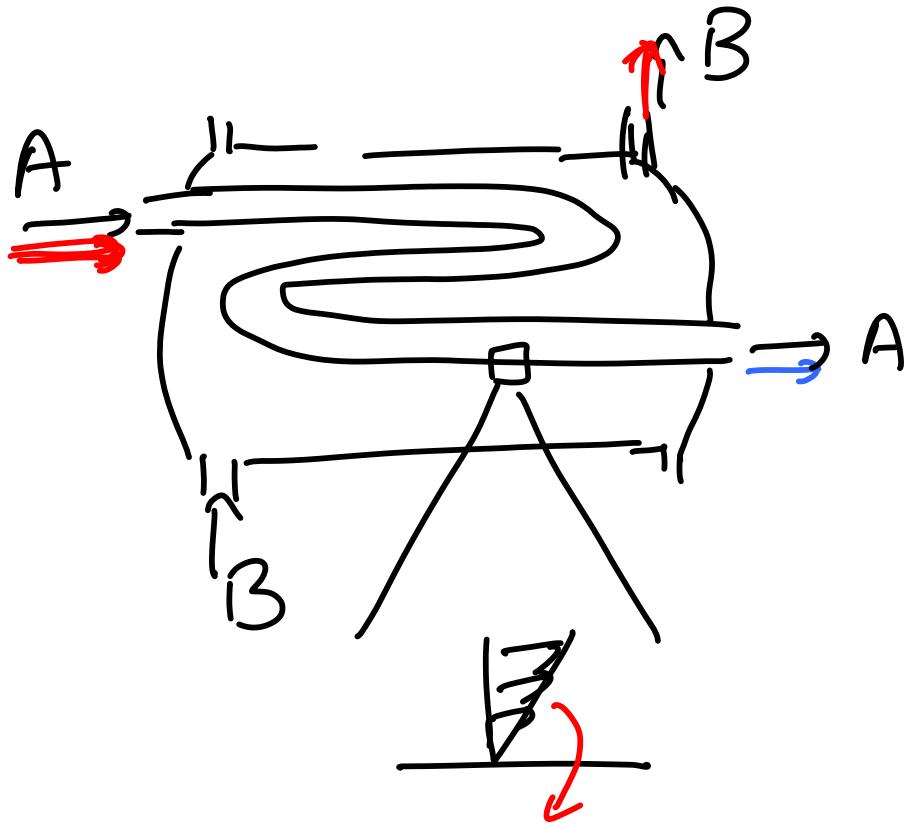


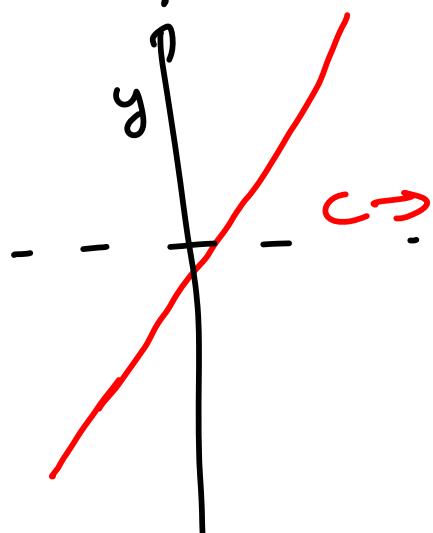
FUNDAMENTALS OF TRANSPORT PROCESSES -II





CONVECTION

Due to mean flow
of fluid carrying
mass / energy

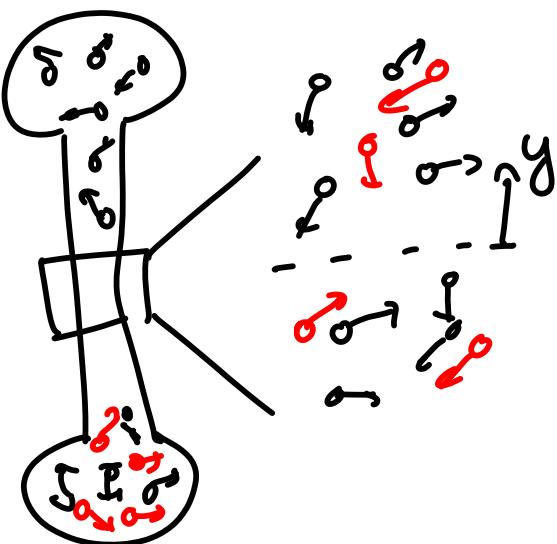


DIFFUSION

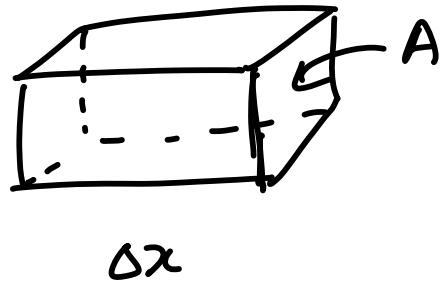
Molecular motion

$$\frac{1}{2}mv^2 = \frac{3}{2}kT$$

$$j = \frac{\text{Mass transported}}{\text{Area time}}$$



$$\left[j_x = \bar{D} \frac{\bar{\Delta C}}{\Delta x} \right]; \frac{\text{Mass transferred}}{\text{Area} \times \text{Time}} = -D \left[\frac{\text{Change in mass density}}{\text{Distance}} \right]$$



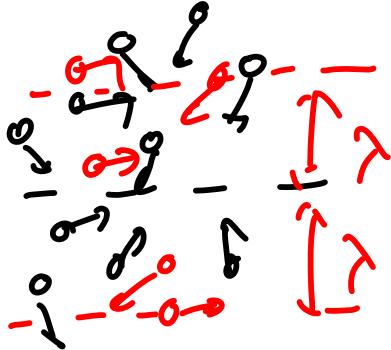
$$D = L^2 T^{-1}$$

$$\frac{\text{Heat transferred}}{\text{Area} \times \text{Time}} = \alpha \left[\frac{\text{Change in energy density}}{\text{Distance}} \right]$$

$$\alpha = \left(\frac{k}{\rho C_p} \right)$$

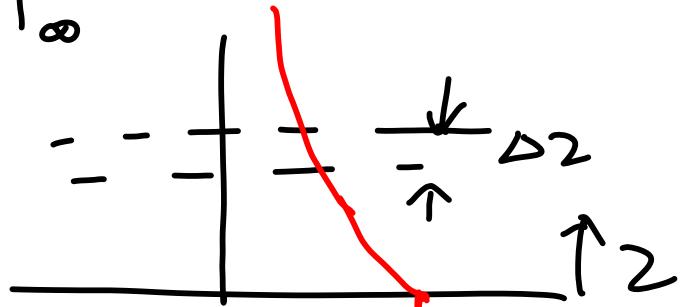
Dx [5 nm, 2]

$$\Delta c \propto \gamma \frac{\Delta c}{\Delta x}$$



$$\left(\begin{array}{l} \text{Change in} \\ \text{mass (momentum)} \\ \text{energy} \\ \text{in time } \Delta t \end{array} \right) = \left(\begin{array}{l} \text{Mass (momentum)} \\ \text{energy} \\ \text{IN} \end{array} \right) - \left(\begin{array}{l} \text{Mass (momentum)} \\ \text{energy} \\ \text{OUT} \end{array} \right) + (\text{Accumulation})$$

$$T = T_\infty$$



$$\text{At } t=0 \quad T=T_0$$

$$\frac{\Delta T}{\Delta t} = - \frac{\Delta q_{12}}{\Delta z}$$

Take limit $\Delta t \rightarrow 0$ & $\Delta z \rightarrow 0$

$$\frac{\partial T}{\partial t} = - \frac{\partial q_{12}}{\partial z}$$

$$q_{12} = -\alpha \frac{\Delta T}{\Delta z} = -\alpha \frac{\partial T}{\partial z}$$

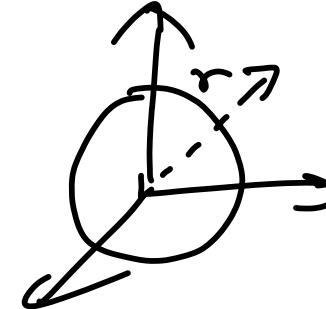
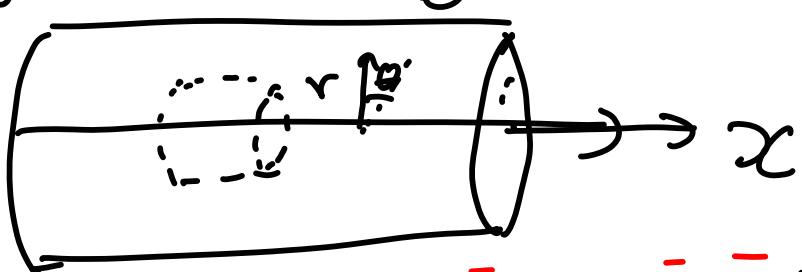
$$\frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial z^2}$$

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial z^2}$$

$$\frac{\partial T}{\partial t} = \lim_{\Delta t \rightarrow 0} \frac{T(z, t + \Delta t) - T(z, t)}{\Delta t}$$

$$\frac{\partial T}{\partial z} = \lim_{\Delta z \rightarrow 0} \frac{T(z + \Delta z, t) - T(z, t)}{\Delta z}$$

Cylindrical co-ordinate system



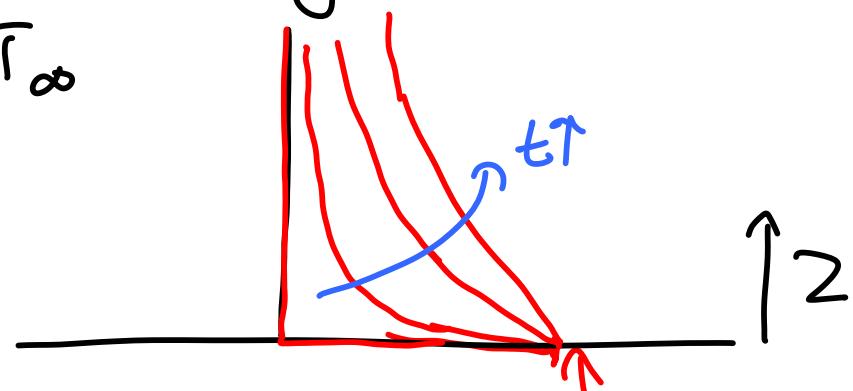
$$\frac{\partial T}{\partial t} = \alpha \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) \right]$$

$$\frac{\partial T}{\partial t} = \alpha \left[\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) \right]$$

$$\frac{\partial C}{\partial t} = D \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) \right]$$

① Similarity solutions

$$T = T_\infty$$

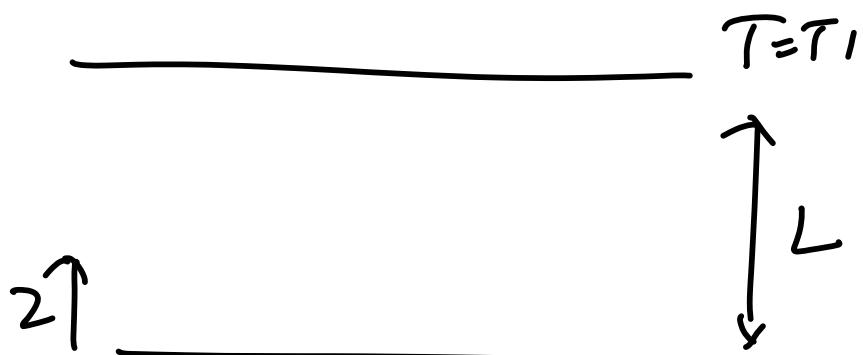


$$\frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial z^2}$$

$$T = \frac{T - T_\infty}{T_0 - T_\infty}$$

$$\frac{T - T_\infty}{T_0 - T_\infty} = 1 - \frac{1}{\sqrt{\pi}} \int_0^{z/\sqrt{\alpha t}} d\xi e^{-\xi^2/4}$$

$$\eta = \frac{z}{\sqrt{\alpha t}}$$



$$T^* = \frac{T - T_0}{T_1 - T_0} \quad z^* = \frac{z}{L}$$

$$T^*(z^*, t^*)$$

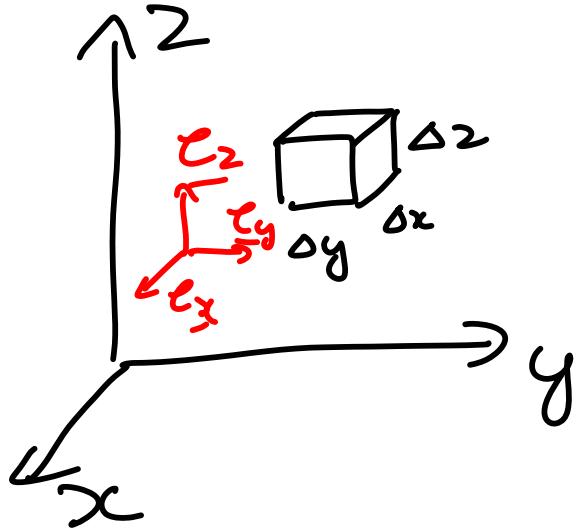
$$t^* = \frac{t \alpha}{L^2}$$

$$\begin{aligned} T^* &= Z(z^*) F(t^*) \\ T^* &= (1 - z^*) - \sum_n \left(\frac{2}{n\pi} \right) \sin(n\pi z^*) e^{-n^2 \bar{T}^2 t^*} \end{aligned}$$

$$\frac{\partial T^*}{\partial t^*} = \frac{\partial^2 T^*}{\partial z^{*2}}$$

$$\frac{1}{F} \frac{dF}{dt^*} = \frac{1}{Z} \frac{d^2 Z}{dz^{*2}} = -(n\pi)^2$$

$$T^* = \sum_{n=1}^{\infty} C_n \underbrace{\sin(n\pi z^*)}_{-n^2 \bar{T}^2 t^*} e$$



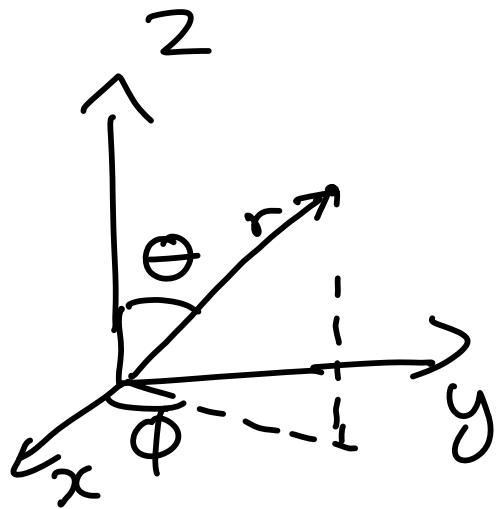
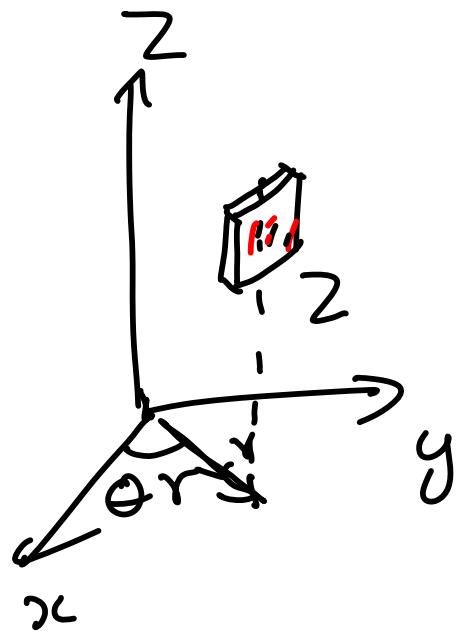
$$\begin{aligned}
 & \frac{\partial c}{\partial t} + \frac{\partial}{\partial x}(u_x c) + \frac{\partial}{\partial y}(u_y c) + \frac{\partial}{\partial z}(u_z c) \\
 &= -\frac{\partial j_x}{\partial x} - \frac{\partial j_y}{\partial y} - \frac{\partial j_z}{\partial z} \\
 & ; \quad \frac{\partial c}{\partial t} + \nabla \cdot (\underline{u} c) = -\nabla \cdot \underline{j} \\
 & = D \nabla^2 c
 \end{aligned}$$

$$\underline{j} = j_x \underline{e_x} + j_y \underline{e_y} + j_z \underline{e_z}$$

$$\underline{u} = u_x \underline{e_x} + u_y \underline{e_y} + u_z \underline{e_z}$$

$$\nabla = \underline{e_x} \frac{\partial}{\partial x} + \underline{e_y} \frac{\partial}{\partial y} + \underline{e_z} \frac{\partial}{\partial z}$$

$$\begin{aligned}
 \underline{j} &= -D \nabla c \\
 &= -D \left(\underline{e_x} \frac{\partial c}{\partial x} + \underline{e_y} \frac{\partial c}{\partial y} + \underline{e_z} \frac{\partial c}{\partial z} \right)
 \end{aligned}$$



$$\frac{\partial c}{\partial r} + \nabla \cdot (\underline{u}_c) = D \nabla^2 c$$

$$\nabla \cdot (\underline{u}_c) = \frac{1}{r} \frac{\partial}{\partial r} (r u_r c) + \frac{1}{r} \frac{\partial}{\partial \theta} (u_\theta c) + \frac{\partial}{\partial z} (u_z c)$$

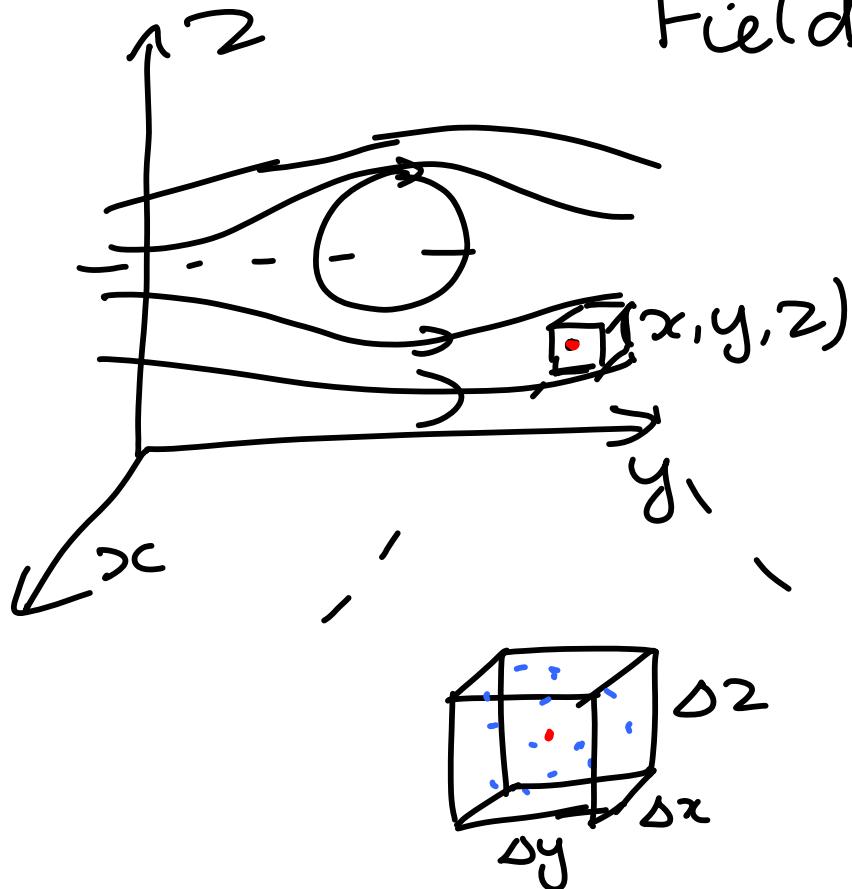
$$\nabla^2 c = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial c}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 c}{\partial \theta^2} + \frac{\partial^2 c}{\partial z^2}$$

$$\begin{aligned} \nabla \cdot (\underline{u}_c) &= \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 u_r c \right) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta u_\theta c \right) \\ &\quad + \frac{1}{r^2} \frac{\partial^2 c}{\partial \phi^2} \end{aligned}$$

$$\begin{aligned} \nabla^2 c &= \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial c}{\partial r} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 c}{\partial \theta^2} \left(\sin \theta \frac{\partial c}{\partial \theta} \right) \\ &\quad + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 c}{\partial \phi^2} \end{aligned}$$

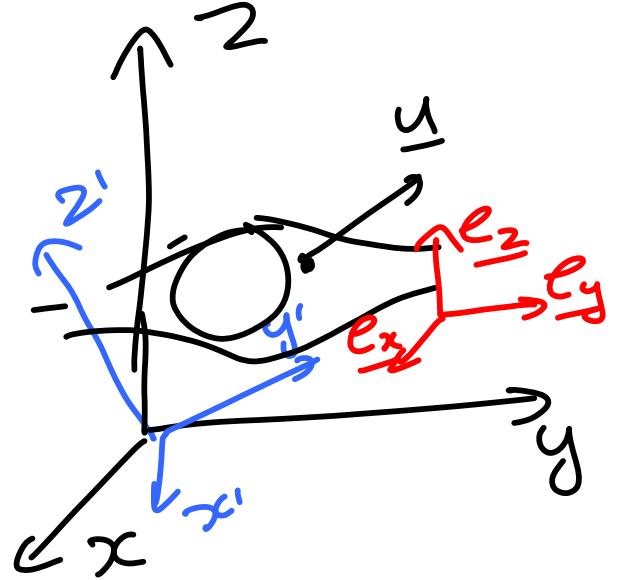
FLUID MECHANICS:

CONTINUUM APPROXIMATION



Fields Density $\underline{\rho} = \lim_{\Delta V \rightarrow 0} \frac{m}{\Delta V}$

$$\underline{\rho} = \lim_{\Delta V \rightarrow 0} \frac{\sum_{i=1}^n m_i \underline{u}_i}{\Delta V}$$



$$\underline{u} = u_x \underline{e}_x + u_y \underline{e}_y + u_z \underline{e}_z$$

$$= u_x' \underline{e}'_x + u_y' \underline{e}'_y + u_z' \underline{e}'_z$$

$$|\underline{u}| = \sqrt{u_x^2 + u_y^2 + u_z^2}$$

$$= \sqrt{u_x'^2 + u_y'^2 + u_z'^2}$$

$$\underline{A} \cdot \underline{B} = A_x B_x + A_y B_y + A_z B_z$$

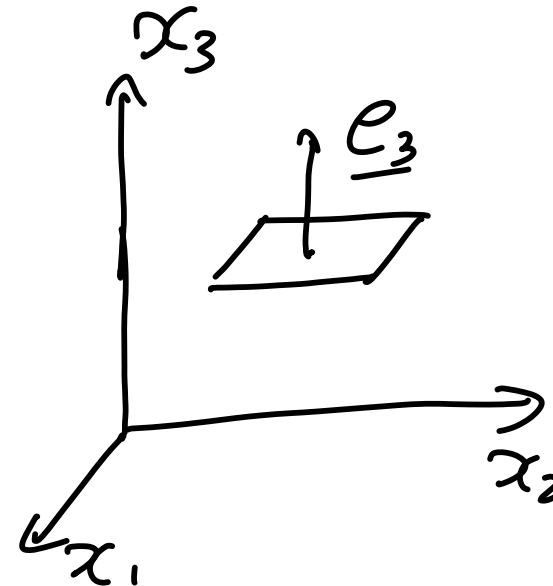
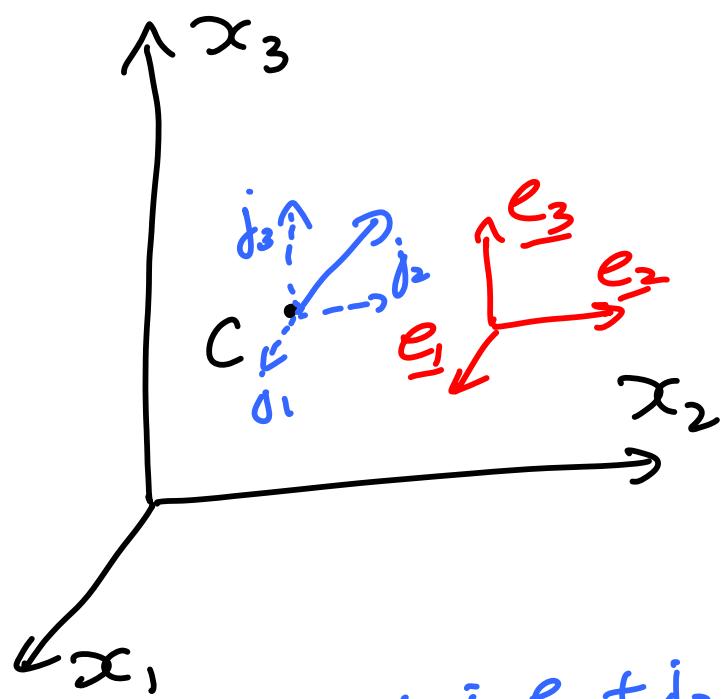
$$= A_x' B_x' + A_y' B_y' + A_z' B_z'$$

$$\underline{q}_r = q_x \underline{e}_x + q_y \underline{e}_y + q_z \underline{e}_z$$

$$\nabla C = \underline{e}_x \frac{\partial C}{\partial x} + \underline{e}_y \frac{\partial C}{\partial y} + \underline{e}_z \frac{\partial C}{\partial z}$$

$$\dot{j} = -D \nabla C$$

$$q_r = -k \nabla T$$



$$j = j_1 e_1 + j_2 e_2 + j_3 e_3$$

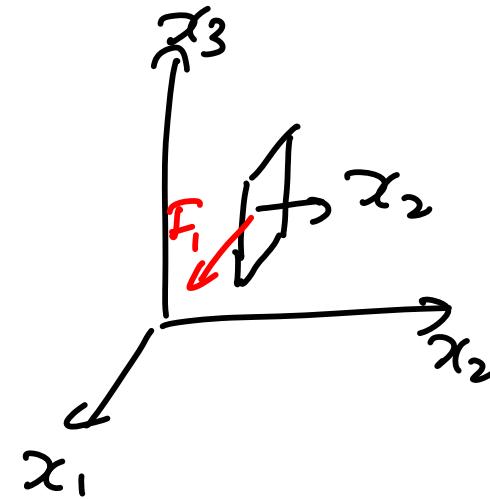
$\underline{\tau}$ = Force / unit area
at a surface with unit
normal

$$\begin{aligned} &= \tau_{11} e_1 e_1 + \tau_{12} e_1 e_2 + \tau_{13} e_1 e_3 \\ &\quad + \dots + \tau_{33} e_3 e_3 \end{aligned}$$

τ_{11} = Force / Area in x_1 direction
acting at a surface with
'outward' unit normal
in x_1 direction

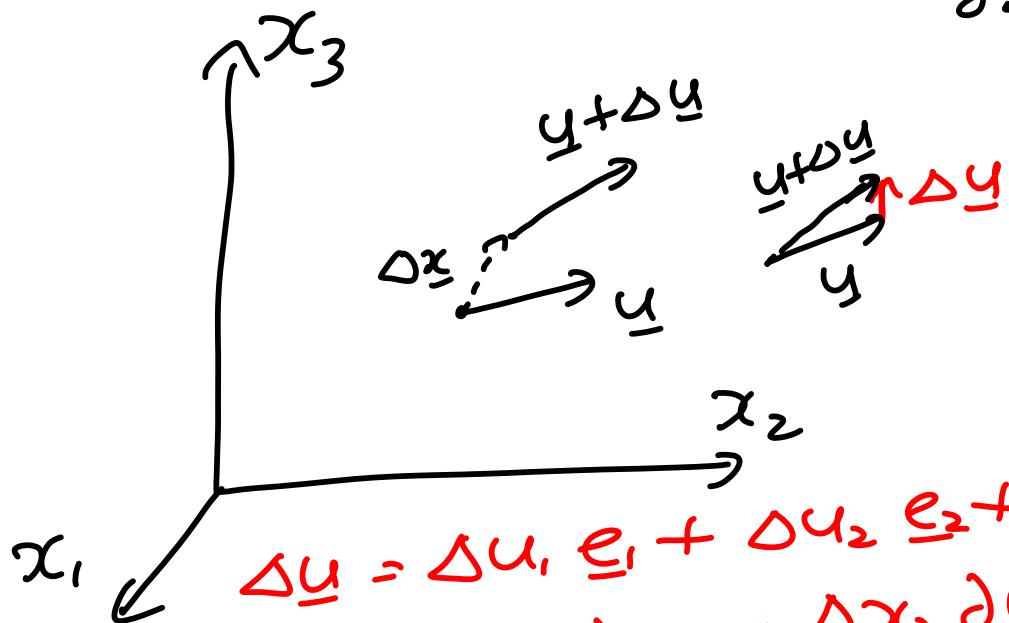
τ_{12} = Force / Area in x_1 direction
acting at surface with
unit normal in x_2 direction

τ_{ij} = Force / Area in x_i direction
acting at a surface with
unit normal in x_j direction
'outward'



$$\nabla \underline{u} = e_1 \underline{e}_1 \frac{\partial \underline{u}_1}{\partial x_1} + e_1 \underline{e}_2 \frac{\partial \underline{u}_2}{\partial x_1} + e_1 \underline{e}_3 \frac{\partial \underline{u}_3}{\partial x_1} + \dots$$

$$+ e_3 \underline{e}_3 \frac{\partial \underline{u}_3}{\partial x_3}$$



$$\Delta \underline{u} = \Delta \underline{u}_1 \underline{e}_1 + \Delta \underline{u}_2 \underline{e}_2 + \Delta \underline{u}_3 \underline{e}_3$$

$$\Delta \underline{u}_1 = \Delta x_1 \frac{\partial \underline{u}_1}{\partial x_1} + \Delta x_2 \frac{\partial \underline{u}_1}{\partial x_2} + \Delta x_3 \frac{\partial \underline{u}_1}{\partial x_3}$$

$$= \Delta \underline{x} \cdot \nabla \underline{u}_1$$

$$\Delta \underline{u}_2 = \Delta \underline{x} \cdot \nabla \underline{u}_2$$

$$\Delta \underline{u}_3 = \Delta \underline{x} \cdot \nabla (\underline{u}_1 \underline{e}_1 + \underline{u}_2 \underline{e}_2 + \underline{u}_3 \underline{e}_3) = \Delta \underline{x} \cdot \nabla \underline{u}$$

$$\vec{\nabla} \vec{u} = e_1 e_1 \frac{\partial u_1}{\partial x_1} + e_1 e_2 \frac{\partial u_2}{\partial x_1} + e_1 e_3 \frac{\partial u_3}{\partial x_1} + \dots + e_3 e_3 \frac{\partial u_3}{\partial x_3}$$

$$\frac{\partial c}{\partial t} + \vec{\nabla} \cdot (\vec{u} c) = D \vec{\nabla}^2 c$$

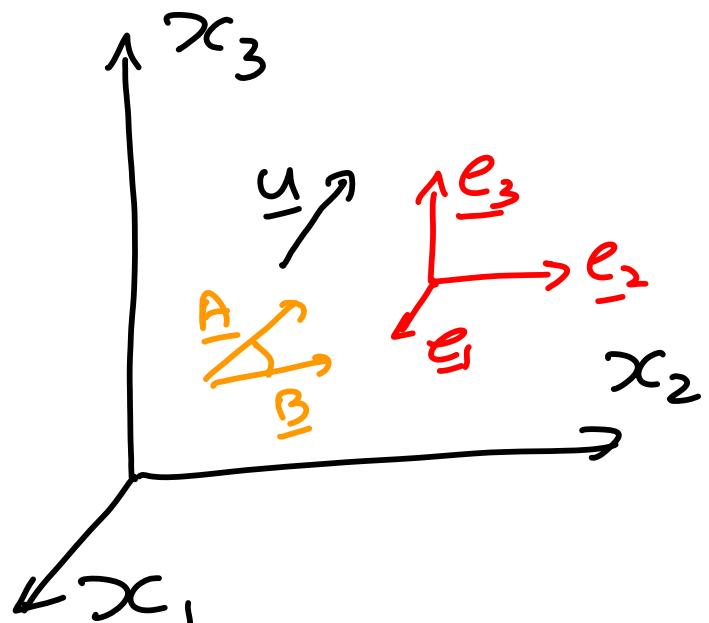
Diffusion dominated
Convection dominated

$$\frac{\partial s}{\partial t} + \vec{\nabla} \cdot (\vec{u} s) = 0$$

$$s \left[\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \vec{\nabla} \vec{u} \right] = - \vec{\nabla} p + \mu \vec{\nabla} \left[\vec{\nabla} u + \vec{\nabla} u^T - \frac{2}{3} \vec{\nabla} \vec{\nabla} \cdot \vec{u} \right]$$

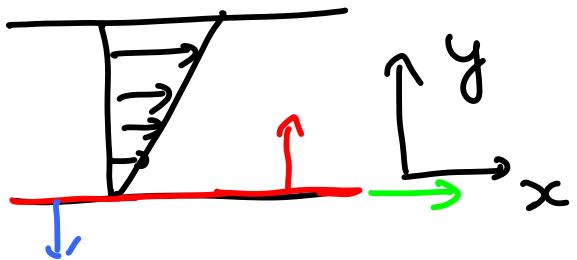
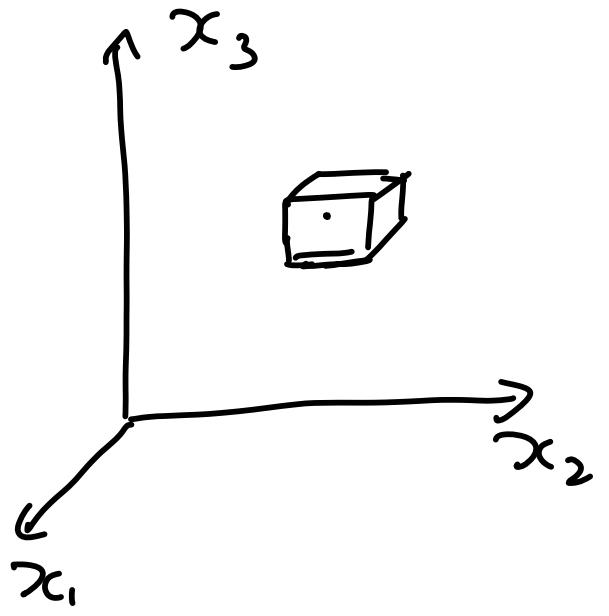
$$\text{Reynolds number} = \frac{s U D}{\mu} = \frac{U D}{N}$$

VECTORS & TENSORS:



$$\begin{aligned} \underline{u} &= \underline{u}_1 \underline{e}_1 + \underline{u}_2 \underline{e}_2 + \underline{u}_3 \underline{e}_3 \\ &= \sum_{i=1}^3 \underline{u}_i \underline{e}_i \\ &= \underline{u}_i \end{aligned}$$

$$\begin{aligned} \underline{A} &= A_1 \underline{e}_1 + A_2 \underline{e}_2 + A_3 \underline{e}_3 = \sum_{i=1}^3 A_i \underline{e}_i = A_i \\ \underline{B} &= B_1 \underline{e}_1 + B_2 \underline{e}_2 + B_3 \underline{e}_3 = \sum_{i=1}^3 B_i \underline{e}_i = B_i \\ \underline{A} \cdot \underline{B} &= |A| |B| \cos \theta \\ &= A_1 B_1 + A_2 B_2 + A_3 B_3 = \sum_{i=1}^3 A_i B_i = A_i B_i \end{aligned}$$



$$T_{xy} = \mu \frac{du_x}{dy}$$

= Force/unit area in x direction
at a surface with unit
normal (**outward**) in y dir.

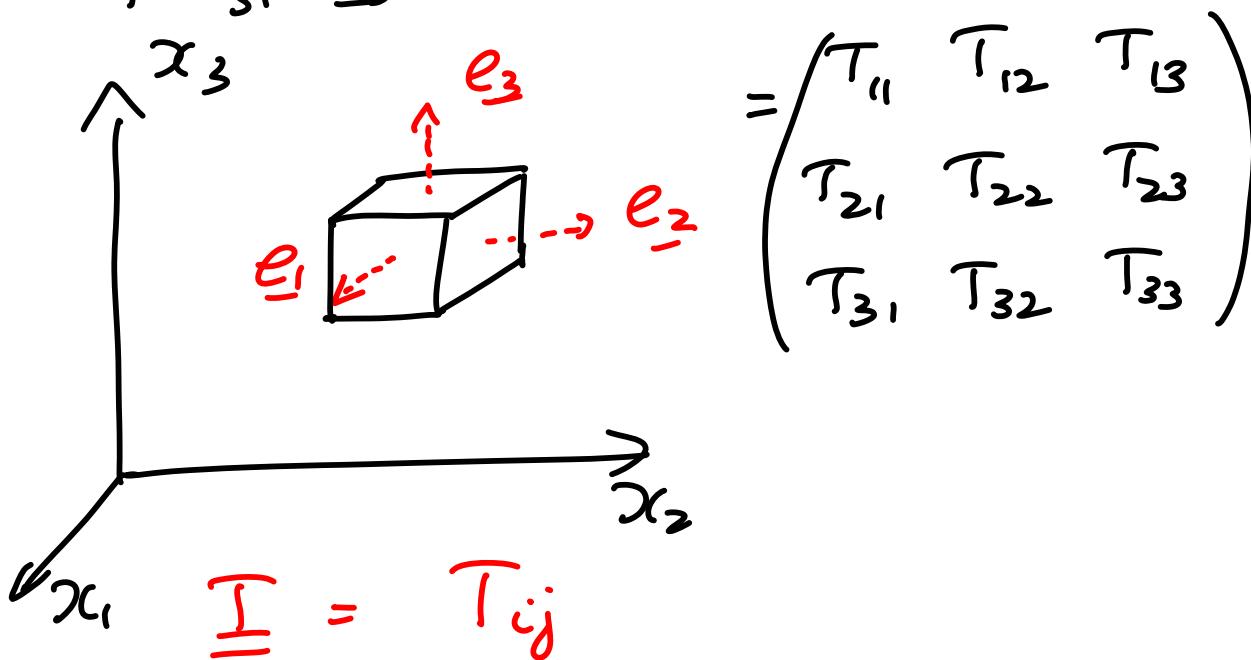
$$T_{ij} = \text{Force/Area in the } x_i \text{ direction}
acting at a surface with
outward unit normal in x_j dir.$$

$$\begin{aligned}
 \underline{y} &= u_1 \underline{e}_1 + u_2 \underline{e}_2 + u_3 \underline{e}_3 \\
 \underline{T} &= T_{11} \underline{e}_1 \underline{e}_1 + T_{12} \underline{e}_1 \underline{e}_2 + T_{13} \underline{e}_1 \underline{e}_3 \\
 &\quad + T_{21} \underline{e}_2 \underline{e}_1 + T_{22} \underline{e}_2 \underline{e}_2 + T_{23} \underline{e}_2 \underline{e}_3 \\
 &\quad + T_{31} \underline{e}_3 \underline{e}_1 + T_{32} \underline{e}_3 \underline{e}_2 + T_{33} \underline{e}_3 \underline{e}_3
 \end{aligned}$$

$$= \sum_{i=1}^3 u_i \underline{e}_i$$

$$= \sum_{i=1}^3 \sum_{j=1}^3 T_{ij} \underline{e}_i \underline{e}_j$$

$$= T_{ij}$$



$$\underline{I} = T_{ij}$$

$$\underline{A} \cdot \underline{B} = \left[\sum_{i=1}^3 (A_i \cdot e_i) \right] \cdot \left[\sum_{j=1}^3 B_j \cdot e_j \right]$$

$$[\delta_{ij}] = \sum_{i=1}^3 \sum_{j=1}^3 \delta_{ij} e_i \cdot e_j$$

$$= \sum_{i=1}^3 \sum_{j=1}^3 [A_i B_j e_i \cdot e_j]$$

'Identity tensor'

$$= \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$e_i \cdot e_j = 1 \text{ if } i=j \\ = 0 \text{ if } i \neq j$$

$$= \delta_{ij}$$

$$\underline{A} \cdot \underline{B} = \sum_{i=1}^3 \sum_{j=1}^3 A_i \underline{B_j} \delta_{ij}$$

$$= \sum_{i=1}^3 A_i \underline{B_i}$$

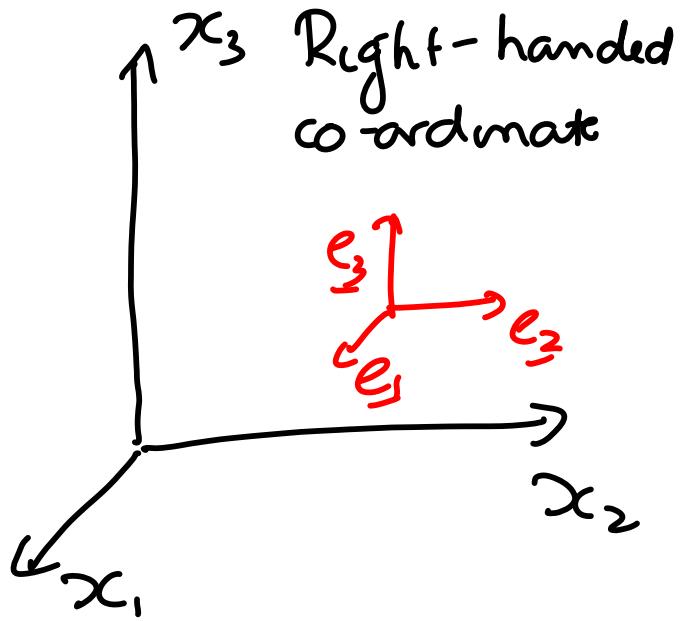
$$\underline{A} \times \underline{B} = \begin{vmatrix} \underline{e}_1 & \underline{e}_2 & \underline{e}_3 \\ A_1 & A_2 & A_3 \\ B_1 & B_2 & B_3 \end{vmatrix} = \underline{e}_1(A_2B_3 - A_3B_2) + \underline{e}_2(A_3B_1 - A_1B_3) + \underline{e}_3(A_1B_2 - A_2B_1)$$

$$\underline{A} \times \underline{B} = \sum_{i=1}^3 \sum_{j=1}^3 \sum_{k=1}^3 \underline{e}_i \epsilon_{ijk} (A_j B_k) = \underline{e}_1(A_2B_3 - A_3B_2) + \underline{e}_2(A_3B_1 - A_1B_3) + \underline{e}_3(A_1B_2 - A_2B_1)$$

Antisymmetric tensor $\underline{A} \times \underline{B} = \epsilon_{ijk} A_j B_k$

$$\begin{aligned} \epsilon_{ijk} &= 1 \text{ if } (ijk) = (123), (312), (231) \\ &= -1 \text{ if } (ijk) = (132), (321), (213) \\ &= 0 \text{ otherwise} \end{aligned}$$

$$\epsilon_{ijk} = -\epsilon_{ikj}$$



$$\underline{e}_1 \times \underline{e}_2 = \underline{e}_3$$

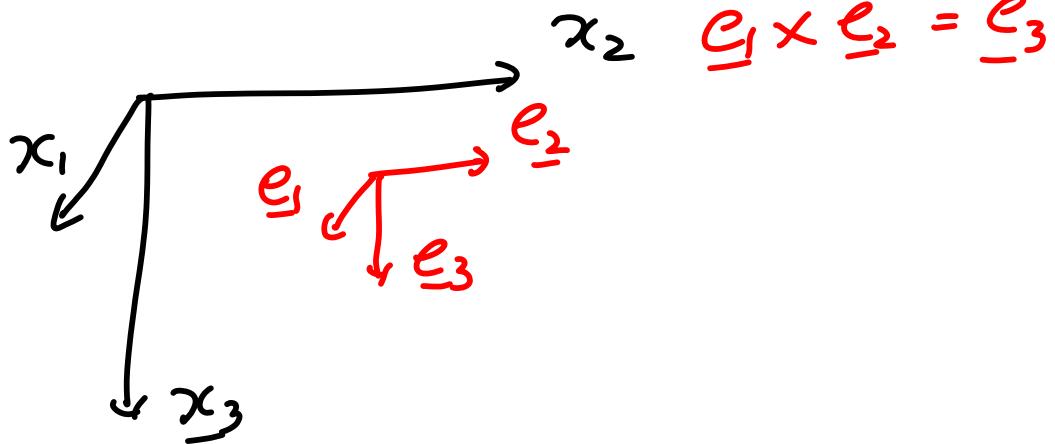
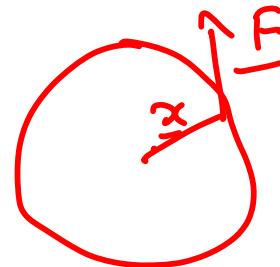
$$\underline{\tau} = \underline{x} \times \underline{F}$$

↓

$$= G_{ijk} x_j F_k$$

Pseudo-vector

$$\underline{\omega} = \underline{r} \times \underline{\omega}$$



Vectors & Tensors:

$$\underline{u} = \sum_{i=1}^3 u_i \underline{e}_i$$

$$\underline{\underline{T}} = \sum_{i=1}^3 \sum_{j=1}^3 T_{ij} \underline{e}_i \underline{e}_j$$

$$\underline{A} \cdot \underline{B} = \sum_{i=1}^3 \sum_{j=1}^3 A_i B_j \underline{e}_i \underline{e}_j$$

$$\begin{aligned} \underline{A} \times \underline{B} &= \epsilon_{ijk} A_i B_k \\ &= -\epsilon_{ikj} A_j B_k \end{aligned}$$

$$= -(\underline{B} \times \underline{A})$$

$$T_{ii} = \sum_{i=1}^3 T_{ii} = T_{11} + T_{22} + T_{33}$$

$$\underline{A} \underline{B} = \sum_{i=1}^3 \sum_{j=1}^3 A_i B_j \underline{e}_i \underline{e}_j = A_i B_j$$

Rules:

- | ① Unrepeated index - fundamental direction
- | Summation + Unit vector
- | ② Index repeated two times
- dot product
- | Summation
- | ③ Index repeated three times
MISTAKE !!!

Dyadic product

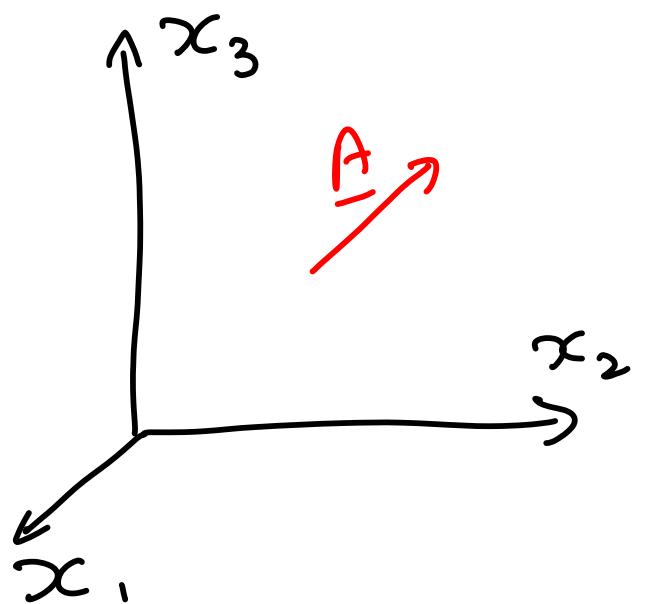
$$A_i S_{jkl} = \sum_{i=1}^3 \sum_{j=1}^3 \sum_{k=1}^3 A_i S_{jkl} \underline{e_i} \underline{e_j} \underline{e_k} \quad A_i B_{kk} + S_{lm} H_{lm} = C_i$$

$$A_i S_{ikl} = \sum_{i=1}^3 \sum_{k=1}^3 A_i S_{ikl} \underline{e_k}$$

④ In equations, the order and unpeated indices of all terms are the same.

⑤ All terms have same parity when going from right-left handed co-ordinate system

Vectors & Tensors:



$$\underline{A} = A_1 \underline{e}_1 + A_2 \underline{e}_2 + A_3 \underline{e}_3$$

$$= A_i$$

$$\underline{\underline{I}} = T_{ij}$$

T_{ij} = Force/Area in i direction at surface with outward unit normal in j direction

$$\underline{A} \cdot \underline{B} = A_i B_i$$

$$> \sum_{i=1}^3 \sum_{j=1}^3 A_i B_j (\underline{e}_i \cdot \underline{e}_j)$$

$$= \sum_{i=1}^3 \sum_{j=1}^3 A_i B_j \delta_{ij}$$

$$\delta_{ij} = 1 \text{ if } i=j$$
$$= 0 \text{ if } i \neq j$$

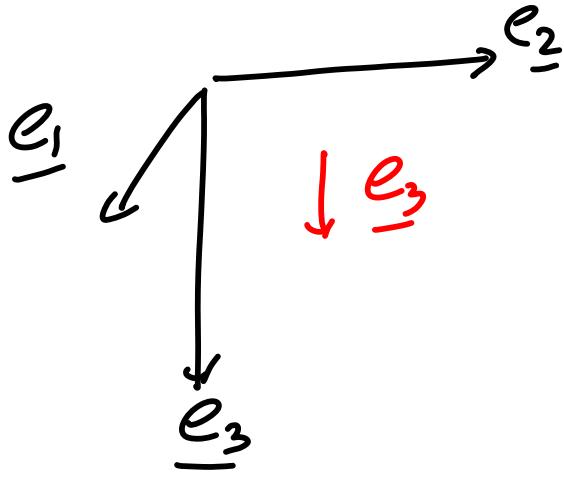
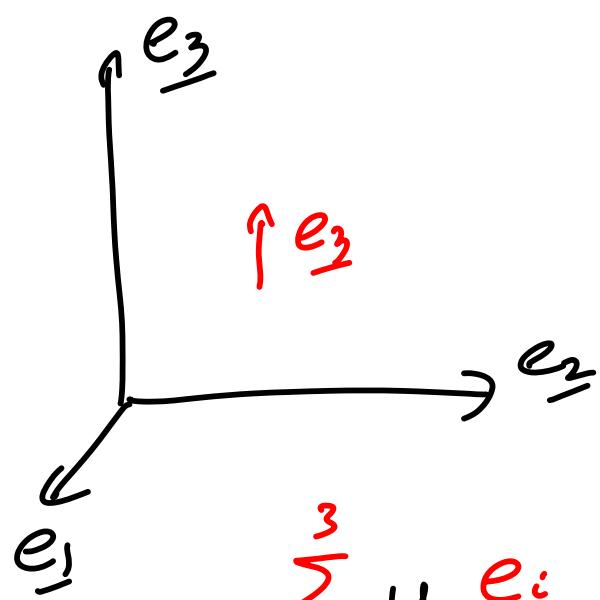
$$\underline{A} \cdot \underline{B} = \sum_{i=1}^3 \sum_{j=1}^3 A_i B_j \delta_{ij}$$

$$\epsilon_{ijk} = \text{Antisymmetric tensor}$$
$$= 1 \text{ for } (ijk) = (123), (312), (231)$$
$$= -1 \text{ for } (ijk) = (132), (321), (213)$$
$$= 0 \text{ otherwise}$$

$$\underline{A} \times \underline{B} = \begin{vmatrix} \underline{e}_1 & \underline{e}_2 & \underline{e}_3 \\ A_1 & A_2 & A_3 \\ B_1 & B_2 & B_3 \end{vmatrix}$$

$$= \epsilon_{ijk} A_j B_k$$

$$\underline{e}_1 \times \underline{e}_2 = \underline{e}_3$$



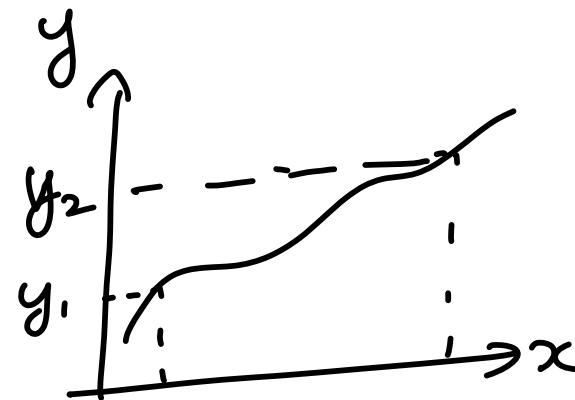
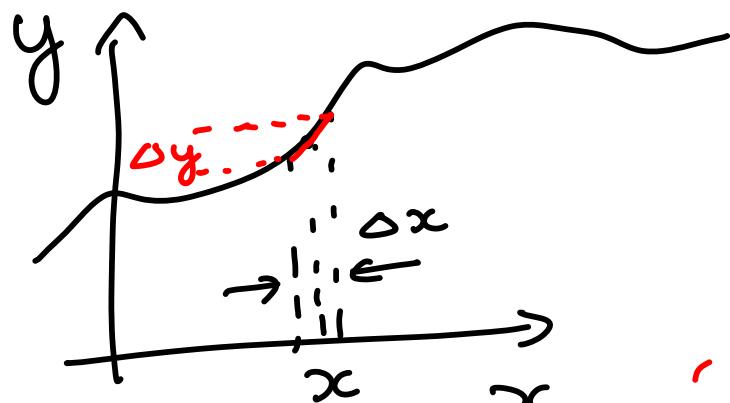
$$\underline{u} = \sum_{i=1}^3 u_i \underline{e}_i$$

$$\underline{T} = \sum_{i=1}^3 \sum_{j=1}^3 T_{ij} \underline{e}_i \cdot \underline{e}_j$$

$$\underline{A} \cdot \underline{B} = \sum_{i=1}^3 A_i B_i$$

$$\underline{A} \times \underline{B} = \epsilon_{ijk} A_j B_k$$

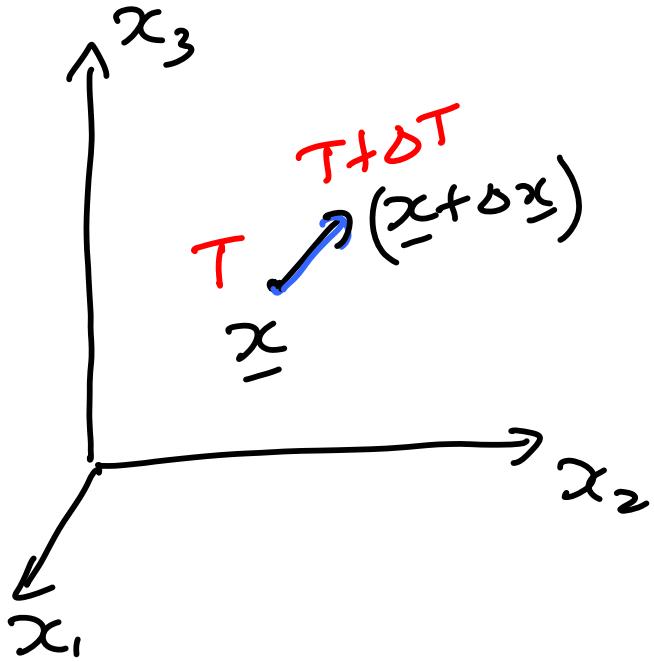
Vector calculus:



$$\frac{dy}{dx} = \lim_{\Delta x \rightarrow 0} \frac{\Delta y}{\Delta x}$$

$$\lim_{\Delta x \rightarrow 0} \Delta x \left(\frac{dy}{dx} \right) = \Delta y$$

$$\int_{x_1}^{x_2} dx \left(\frac{dy}{dx} \right) = y_2 - y_1$$



$$\begin{aligned}\Delta T &= \frac{\partial T}{\partial x_1} \Delta x_1 + \frac{\partial T}{\partial x_2} \Delta x_2 + \frac{\partial T}{\partial x_3} \Delta x_3 \\ &= \left(\underline{e}_1 \frac{\partial T}{\partial x_1} + \underline{e}_2 \frac{\partial T}{\partial x_2} + \underline{e}_3 \frac{\partial T}{\partial x_3} \right) \cdot (\Delta x_1 \underline{e}_1 + \Delta x_2 \underline{e}_2 + \Delta x_3 \underline{e}_3)\end{aligned}$$

$$\Delta T = \nabla T \cdot \Delta \underline{x}$$

grad T · Δx

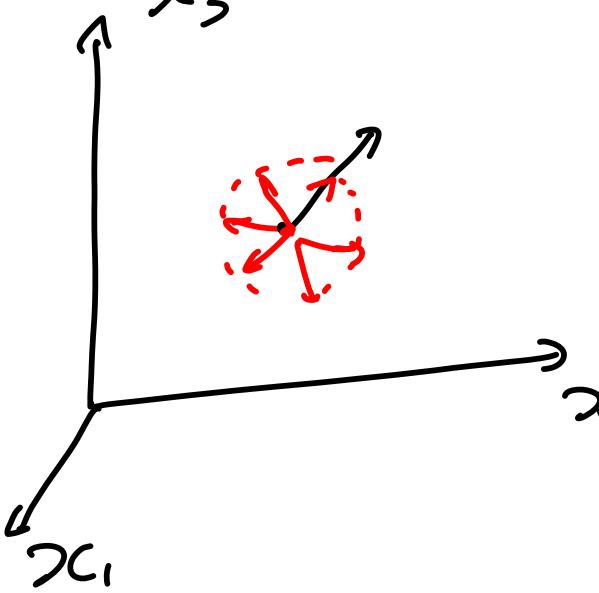
$$\underline{x} = (x_1, x_2, x_3)$$

$$(\underline{x} + \Delta \underline{x}) = (x_1 + \Delta x_1, x_2 + \Delta x_2, x_3 + \Delta x_3)$$

$$\frac{\partial T}{\partial x_i}, \lim_{\Delta x_i \rightarrow 0} \left(\frac{T(x_1 + \Delta x_1, x_2, x_3) - T(x_1, x_2, x_3)}{\Delta x_1} \right)$$

$$|\text{grad } T| = \left[\left(\frac{\partial T}{\partial x_1} \right)^2 + \left(\frac{\partial T}{\partial x_2} \right)^2 + \left(\frac{\partial T}{\partial x_3} \right)^2 \right]^{1/2}$$

$(\text{grad } T) \cdot \underline{\Delta x} = \underline{\Delta T}$ in the limit $\underline{\Delta x} \rightarrow 0$



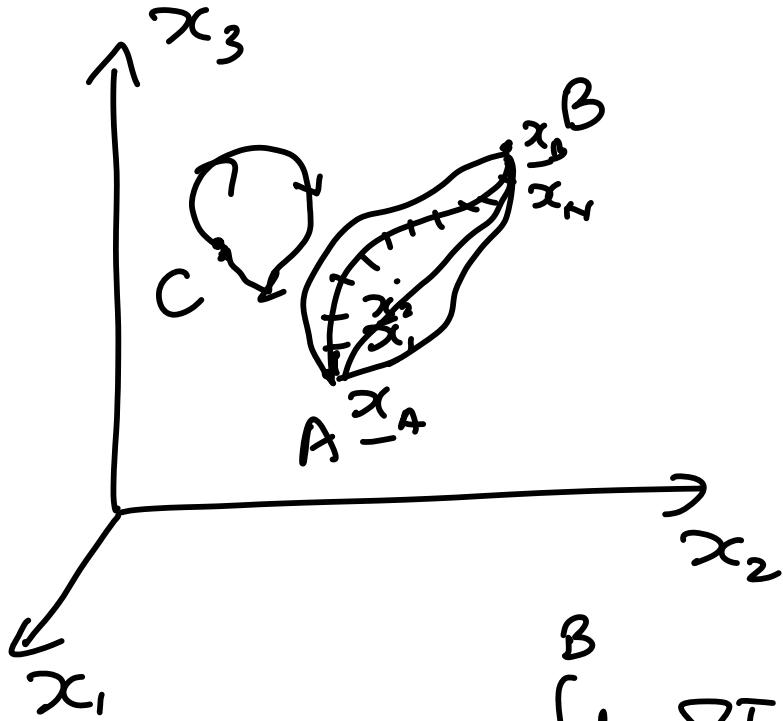
ΔT for equal $|\Delta \underline{x}|$ is maximum when
 $(\text{grad } T)$ is parallel to $\underline{\Delta x}$.

$$\Delta T = |\text{grad } T| |\Delta \underline{x}| \cos \theta$$

- ① $(\text{grad } T)$ is in direction of maximum variation of T .
② $(\text{grad } T)$ is perpendicular to surfaces of constant T .

$$\underline{j} = -D \nabla C$$

$$\underline{q} = -k \nabla T$$

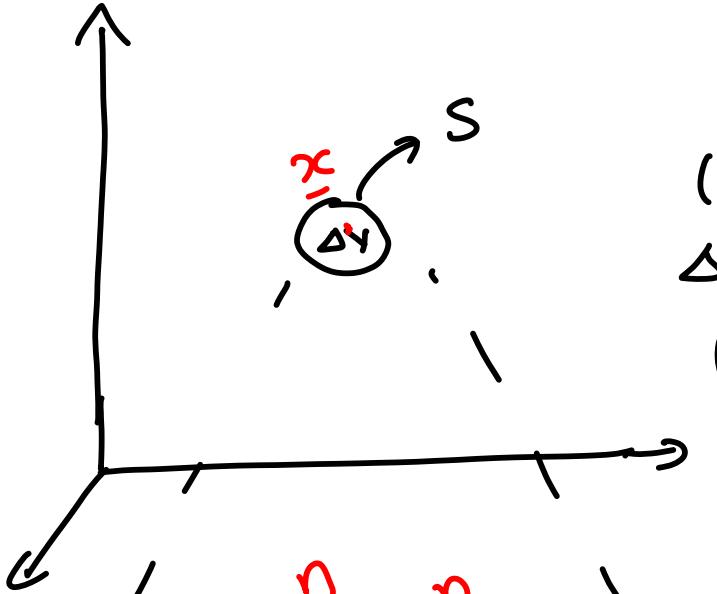


$$\int d\bar{x} \cdot \nabla T = T(\underline{x}_B) - T(\underline{x}_A)$$

$$\begin{aligned} \int_{\underline{x}_A}^{\underline{x}_C} d\bar{x} \cdot \nabla T &= T(\underline{x}_C) - T(\underline{x}_A) \\ &= 0 \end{aligned}$$

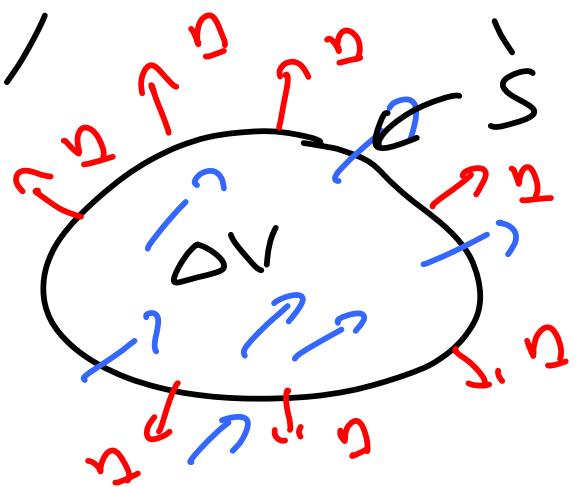
$$\begin{aligned} \int d\bar{x} \cdot \nabla T &= T_B - T_A \\ \sum_{i=1}^n \nabla T \cdot \Delta \bar{x}_i &= \frac{\Delta \underline{x}_1 \cdot (\nabla T)|_{\underline{x}_1}}{\text{---}} + \frac{\Delta \underline{x}_2 \cdot (\nabla T)|_{\underline{x}_2}}{\text{---}} \\ &\quad + \dots + \frac{\Delta \underline{x}_N \cdot (\nabla T)|_{\underline{x}_N}}{\text{---}} \\ &= \left[T(\underline{x}_1) - T(\underline{x}_A) \right] + \left[T(\underline{x}_2) - T(\underline{x}_1) \right] + \\ &\quad \dots + \left[T(\underline{x}_N) - T(\underline{x}_{N-1}) \right] \\ &\quad + \left[T(\underline{x}_B) - T(\underline{x}_N) \right] \end{aligned}$$

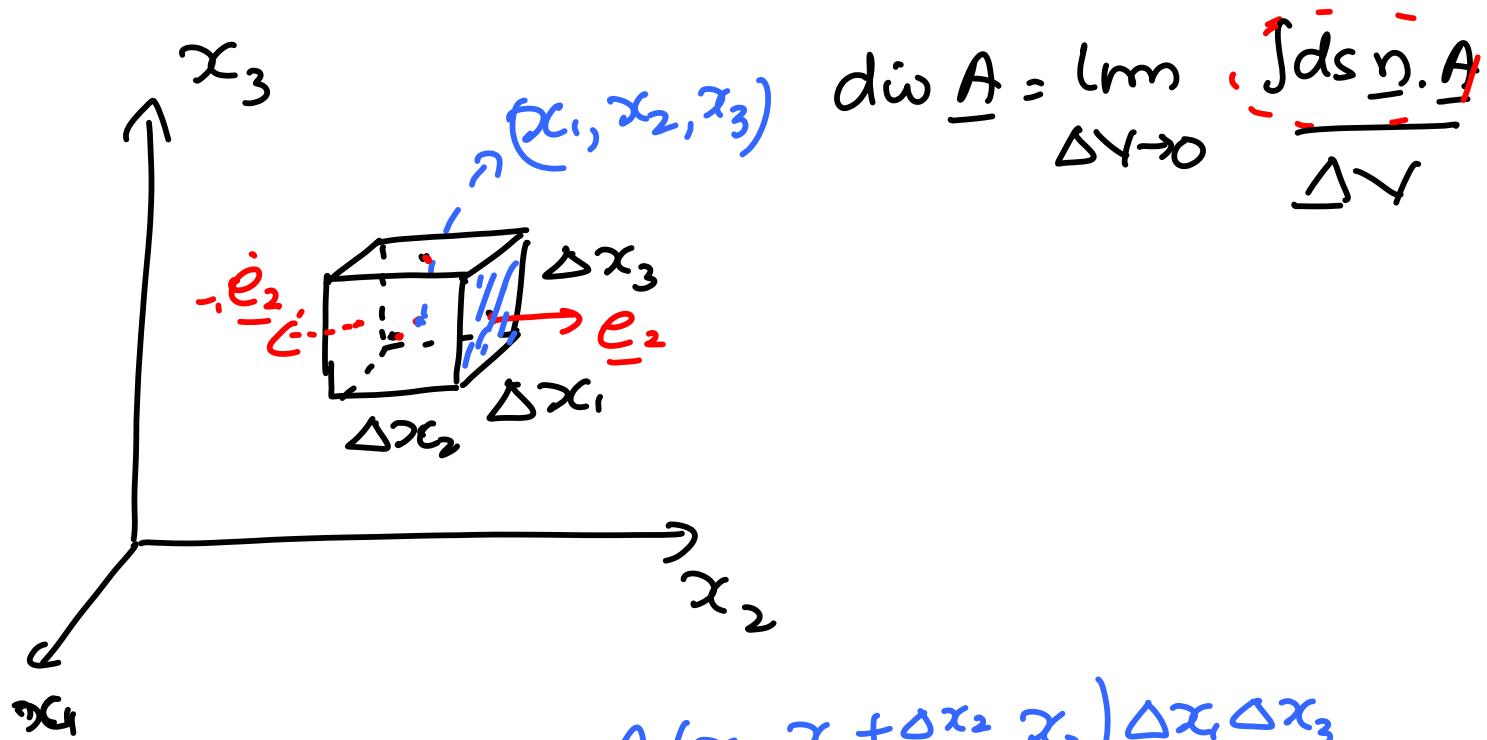
Divergence: $\text{div } \underline{A} = \lim_{\Delta V \rightarrow 0} \frac{\int dS \cdot \underline{n} \cdot \underline{A}}{\Delta V}$



$$\lim_{\Delta V \rightarrow 0} \left[\Delta V \text{ div } \underline{A} = \int dS \underline{n} \cdot \underline{A} \right]$$

$$\lim_{\Delta V \rightarrow 0} \left[\Delta V \text{ div } \underline{q}_r = \int dS \underline{n} \cdot \underline{q}_r \right]$$





$$d\omega \underline{A} = \lim_{\Delta V \rightarrow 0} \frac{\int ds \underline{n} \cdot \underline{A}}{\Delta V}$$

$$\begin{aligned} \int ds \underline{n} \cdot \underline{A} &= e_2 \cdot \underline{A}(x_1, x_2 + \frac{\Delta x_2}{2}, x_3) \Delta x_1 \Delta x_3 \\ &\quad + (-e_2) \cdot \underline{A}(x_1, x_2 - \frac{\Delta x_2}{2}, x_3) \Delta x_1 \Delta x_3 \\ &\quad + e_1 \cdot \underline{A}(x_1 + \frac{\Delta x_1}{2}, x_2, x_3) \Delta x_2 \Delta x_3 \\ &\quad + (-e_1) \cdot \underline{A}(x_1 - \frac{\Delta x_1}{2}, x_2, x_3) \Delta x_2 \Delta x_3 \\ &\quad + e_3 \cdot \underline{A}(x_1, x_2, x_3 + \frac{\Delta x_3}{2}) \Delta x_1 \Delta x_2 \\ &\quad + (-e_3) \cdot \underline{A}(x_1, x_2, x_3 - \frac{\Delta x_3}{2}) \Delta x_1 \Delta x_2 \end{aligned}$$

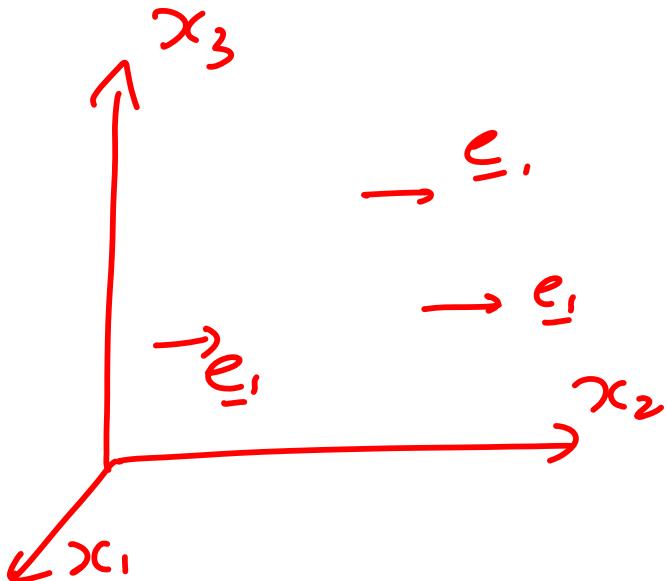
$$\int d\mathbf{s}(\underline{\eta}, \underline{A}) = \Delta x_1 \Delta x_3 \left[A_2(x_1, x_2 + \frac{\Delta x_2}{2}, x_3) - A_2(x_1, x_2 - \frac{\Delta x_2}{2}, x_3) \right] \\ + \Delta x_2 \Delta x_3 \left[A_1(x_1 + \frac{\Delta x_1}{2}, x_2, x_3) - A_1(x_1 - \frac{\Delta x_1}{2}, x_2, x_3) \right] \\ + \Delta x_1 \Delta x_2 \left[A_3(x_1, x_2, x_3 + \frac{\Delta x_3}{2}) - A_3(x_1, x_2, x_3 - \frac{\Delta x_3}{2}) \right]$$

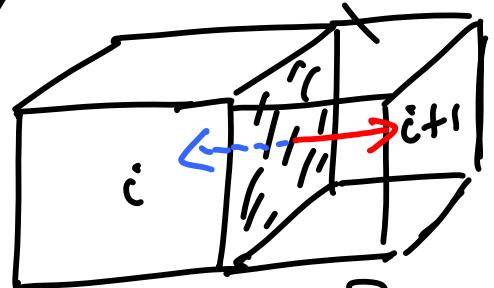
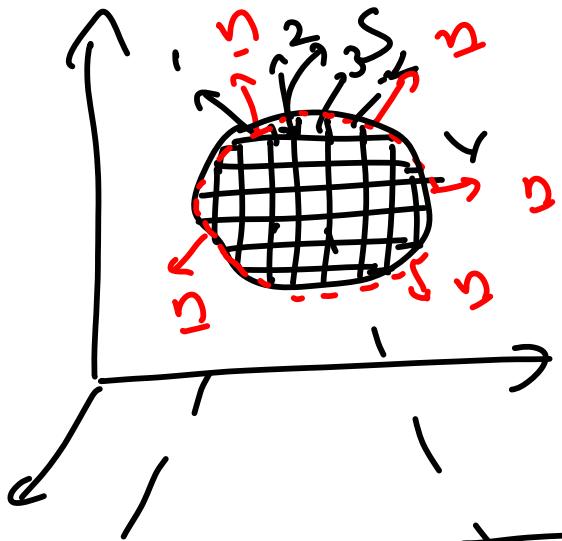
$$\frac{\int d\mathbf{s} \underline{\eta} \cdot \underline{A}}{\Delta V} = \frac{A_2(x_1, x_2 + \frac{\Delta x_2}{2}, x_3) - A_2(x_1, x_2 - \frac{\Delta x_2}{2}, x_3)}{\Delta x_2} \\ + \frac{A_1(x_1 + \frac{\Delta x_1}{2}, x_2, x_3) - A_1(x_1 - \frac{\Delta x_1}{2}, x_2, x_3)}{\Delta x_1} \\ + \frac{A_3(x_1, x_2, x_3 + \frac{\Delta x_3}{2}) - A_3(x_1, x_2, x_3 - \frac{\Delta x_3}{2})}{\Delta x_3} \\ = \frac{\partial A_2}{\partial x_2} + \frac{\partial A_1}{\partial x_1} + \frac{\partial A_3}{\partial x_3}$$

$$d\omega \underline{A} = \frac{\partial A_1}{\partial x_1} + \frac{\partial A_2}{\partial x_2} + \frac{\partial A_3}{\partial x_3} \quad \frac{\partial}{\partial x_i}(A, \underline{e}_i) = \underline{e}_i \frac{\partial A}{\partial x_i}$$

$$= \left(\underline{e}_1 \frac{\partial}{\partial x_1} + \underline{e}_2 \frac{\partial}{\partial x_2} + \underline{e}_3 \frac{\partial}{\partial x_3} \right) \cdot (A, \underline{e}_1 + A_2 \underline{e}_2 + A_3 \underline{e}_3)$$

$$= \nabla \cdot \underline{A}$$





$$\int d\mathbf{s} \cdot \underline{n} \cdot \underline{A} = \int dV (\text{div } \underline{A})$$

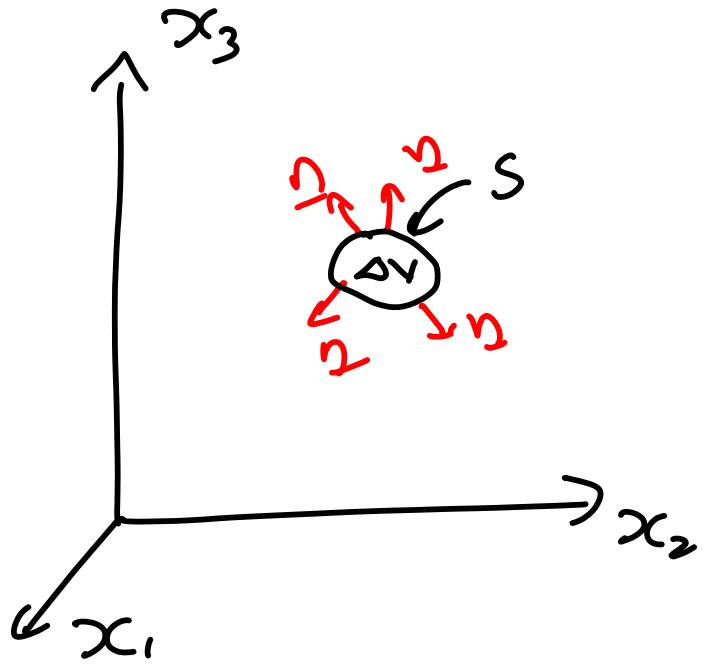
Divergence theorem

$$\begin{aligned} \int dV \text{div } \underline{q} &= (\text{div } \underline{A}|_{x_i} \Delta V_i) + (\text{div } \underline{A}|_{x_{i+1}} \Delta V_{i+1}) + \dots \\ &\quad + (\text{div } \underline{A}|_{x_i} \Delta V_i) + (\text{div } \underline{A}|_{x_{i+1}} \Delta V_{i+1}) + \dots \\ &= \int_S d\mathbf{s} \cdot \underline{n} \cdot \underline{q} \end{aligned}$$

$$\begin{aligned} [\text{div } \underline{A}|_{x_i} \Delta V_i] &= \int_{S_i} d\mathbf{s} \cdot \underline{n} \cdot \underline{A} \\ [\text{div } \underline{A}|_{x_{i+1}} \Delta V_{i+1}] &= \int_{S_{i+1}} d\mathbf{s} \cdot \underline{n} \cdot \underline{A} \end{aligned}$$

$$\operatorname{curl} \underline{A} = \lim_{\Delta V \rightarrow 0} \frac{\int ds \hat{n} \times \underline{A}}{\Delta V} = \lim_{\Delta V \rightarrow 0} \frac{\int ds \epsilon_{ijk} \hat{n}_j A_k}{\Delta V}$$

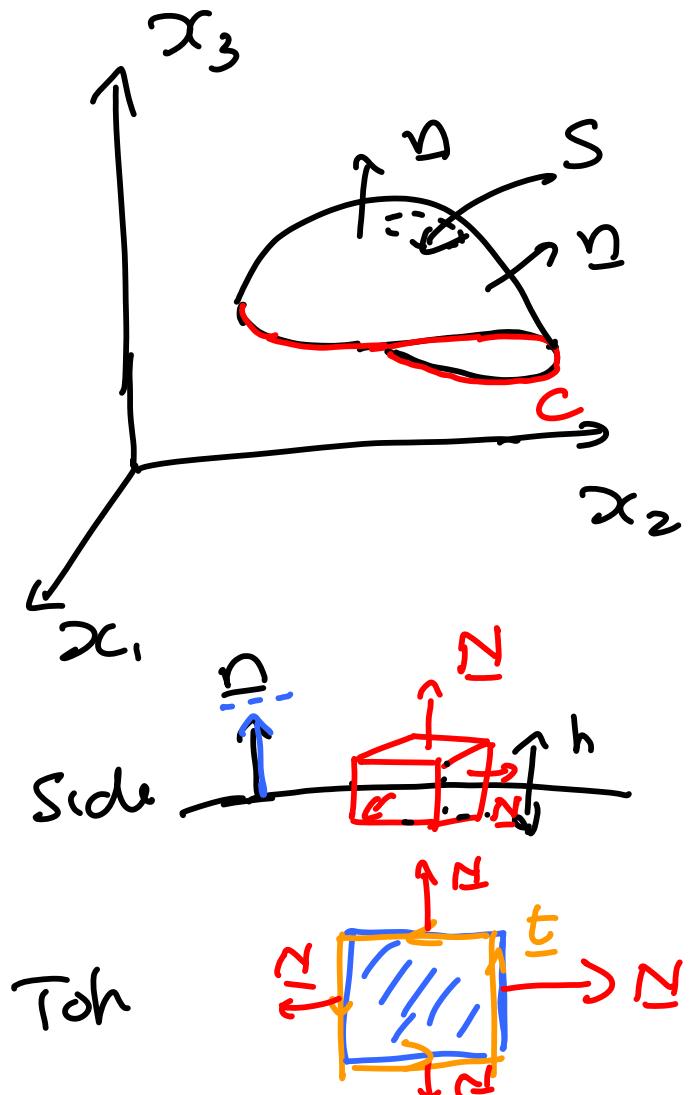
$$= \epsilon_{ijk} \lim_{\Delta V \rightarrow 0} \frac{\int ds \hat{n}_j A_k}{\Delta V}$$



$$= \epsilon_{ijk} \frac{\partial A_k}{\partial x_j} = \nabla \times \underline{A}$$

$$= \begin{vmatrix} \underline{e}_1 & \underline{e}_2 & \underline{e}_3 \\ \frac{\partial}{\partial x_1} & \frac{\partial}{\partial x_2} & \frac{\partial}{\partial x_3} \\ A_1 & A_2 & A_3 \end{vmatrix}$$

Curl - Integral relation:



$$\int d\mathbf{s} \cdot \underline{n} \cdot \text{curl } \underline{A} = \oint_C d\underline{x} \cdot \underline{A}$$

$$\underline{n} \cdot \text{curl } \underline{A} = \frac{1}{\Delta V} \int d\sigma \underline{n} \cdot (\underline{N} \times \underline{A})$$

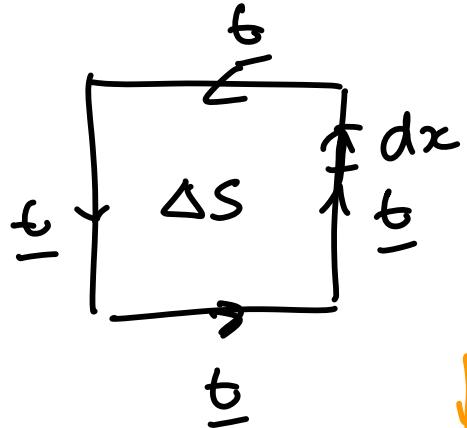
$$= \frac{1}{\Delta V} \int d\sigma \underline{A} \cdot (\underline{N} \times \underline{N})$$

$$= \frac{1}{\Delta V} \int_{\text{side}} d\sigma \underline{A} \cdot (\underline{n} \times \underline{N})$$

$$= \frac{1}{\Delta V} \int_{\text{side}} d\sigma \underline{A} \cdot \underline{t}$$

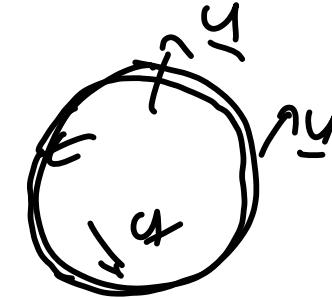
$$= \frac{1}{\Delta S K} \int_{\text{side}} K dx \underline{A} \cdot \underline{t}$$

$$= \frac{1}{\Delta S} \int dx \underline{A} \cdot \underline{t} = \frac{1}{\Delta S} \int dx \underline{A}$$



$$\underline{n} \cdot \text{curl } \underline{A} = \frac{1}{\Delta S} \oint_{\partial S} \underline{dx} \cdot \underline{A}$$

$$\underline{\Delta S} \cdot \underline{n} \cdot \text{curl } \underline{A} = \oint_{\partial S} \underline{dx} \cdot \underline{A}$$



$$\int d\underline{s} \underline{n} \cdot \text{curl } \underline{A} = \sum_i \underline{\Delta S}_i \underline{n} \cdot \text{curl } \underline{A}$$

$$\underline{\Delta S}_i \underline{n} \cdot \text{curl } \underline{A} + \frac{\int_{C_i} \underline{dx} \cdot \underline{A}}{\underline{\Delta S}_i}$$

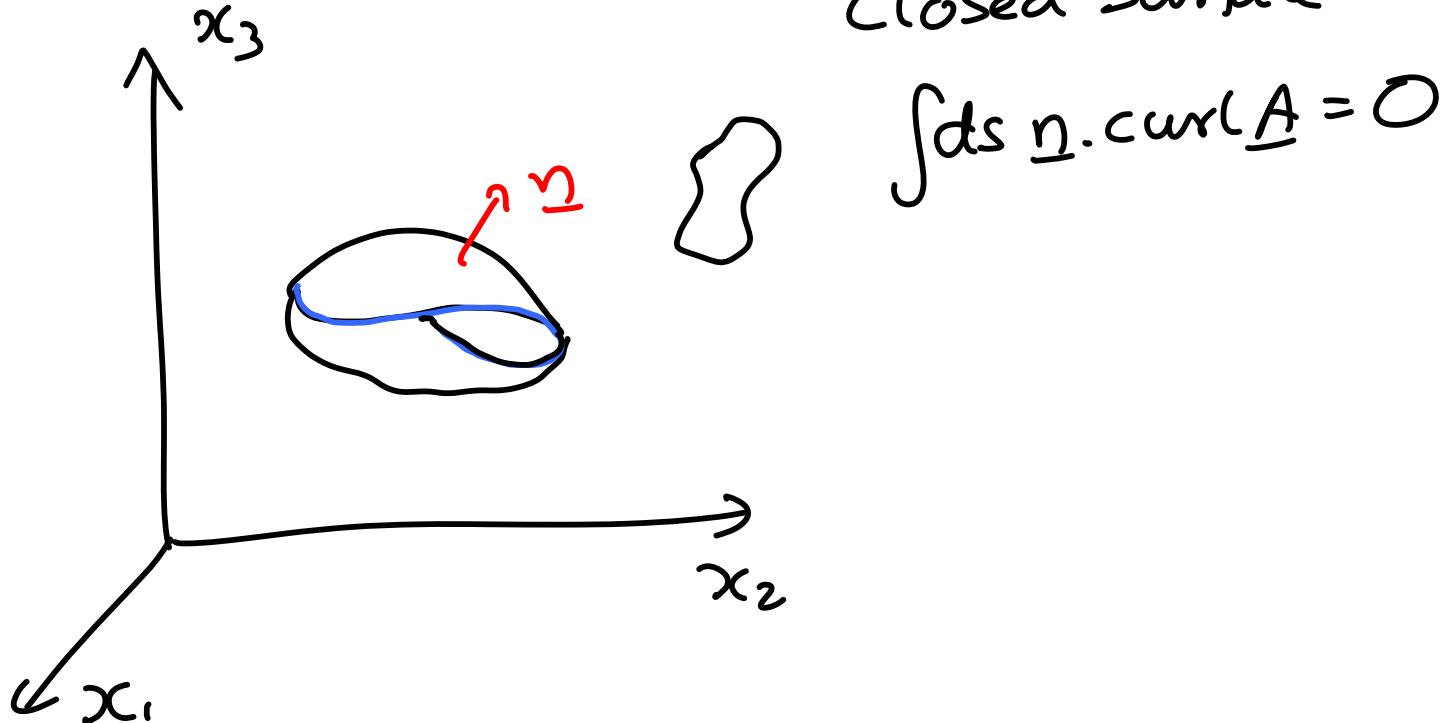
$$\underline{\Delta S}_{i+1} \underline{n} \cdot \text{curl } \underline{A} = \frac{\int_{C_{i+1}} \underline{dx} \cdot \underline{A}}{\underline{\Delta S}_{i+1}}$$

$$\int d\underline{s} \underline{n} \cdot \text{curl } \underline{A} = \oint_C \underline{dx} \cdot \underline{A}$$

Integral theorem for curl

$$\int \underline{ds} \cdot \underline{n} \cdot \text{curl } \underline{A} = \oint \underline{dx} \cdot \underline{A}$$

Closed surface



Vector Calculus:

$$y = \underline{u_i}$$

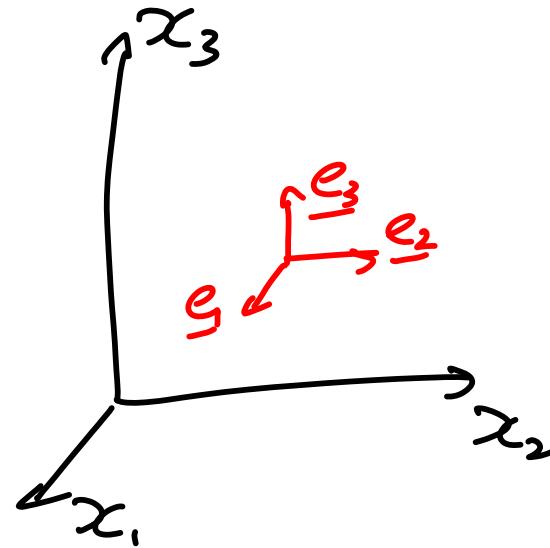
$$\underline{\underline{I}} = \underline{\underline{T_{ij}}}$$

$$\begin{aligned}\underline{A} \cdot \underline{B} &= A_1 B_1 + A_2 B_2 + A_3 B_3 \\ &= A_i B_i\end{aligned}$$

$$\underline{A} \times \underline{B} = \underline{\epsilon_{ijk}} A_j B_k$$

$$\begin{aligned}\delta_{ij} &> 1 \text{ for } i = j = \underline{\epsilon_i} \cdot \underline{\epsilon_j} \\ &= 0 \text{ for } i \neq j\end{aligned}$$

$$\underline{A} \cdot \underline{B} = A_i B_j \delta_{ij}$$



Elements of vector calculus:

$$(\text{grad } T) \cdot \underline{\Delta x} = \frac{T(\underline{x} + \underline{\Delta x}) - T(\underline{x})}{\underline{\Delta x}}$$

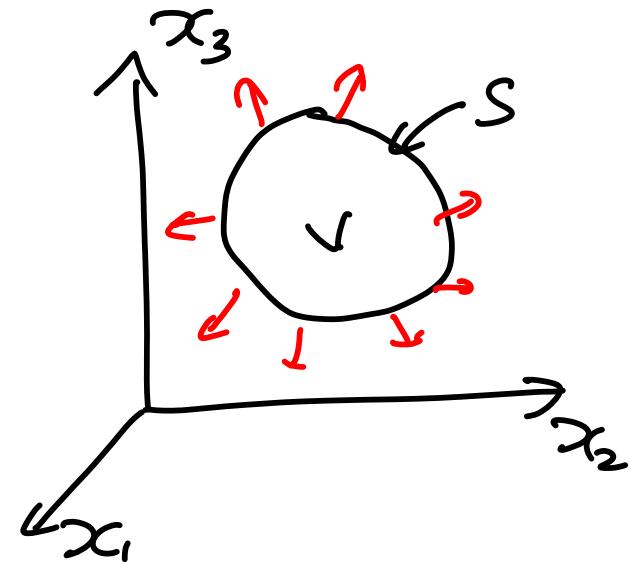
$$\text{grad } T = \underline{e}_1 \frac{\partial T}{\partial x_1} + \underline{e}_2 \frac{\partial T}{\partial x_2} + \underline{e}_3 \frac{\partial T}{\partial x_3}$$

$$\int_A^B d\underline{x} \cdot \text{grad } T = \underline{T_B} - \underline{T_A}$$

$$\text{div } \underline{A} = \lim_{\Delta V \rightarrow 0} \frac{\int d\underline{s} \underline{A} \cdot \underline{n}}{\Delta V}$$

$$\text{div } \underline{A} = \frac{\partial A_1}{\partial x_1} + \frac{\partial A_2}{\partial x_2} + \frac{\partial A_3}{\partial x_3} = \nabla \cdot \underline{A}$$

$$\int_V dV \text{div } \underline{A} = \int_S d\underline{s} \underline{n} \cdot \underline{A}$$

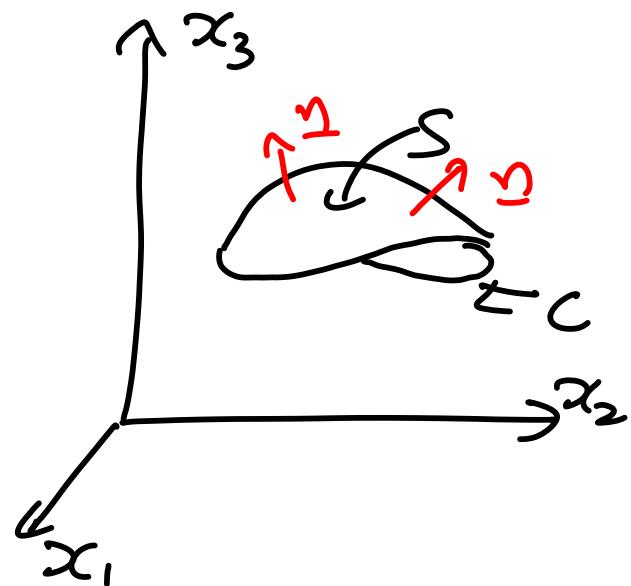


$$\int d\underline{s} \underline{n} \cdot \underline{q} = \int_V dV \text{div } \underline{q}$$

$$\text{curl } \underline{A} = \lim_{\Delta V \rightarrow 0} \frac{\int d\underline{s} \cdot \underline{n} \times \underline{A}}{\Delta V}$$

$$\text{curl } A = \epsilon_{ijk} \frac{\partial}{\partial x_j} (A_k) = \nabla \times \underline{A}$$

$$= \begin{pmatrix} \underline{e}_1 & \underline{e}_2 & \underline{e}_3 \\ \frac{\partial}{\partial x_1} & \frac{\partial}{\partial x_2} & \frac{\partial}{\partial x_3} \\ A_1 & A_2 & A_3 \end{pmatrix}$$



$$\int d\underline{s} \cdot \underline{n} \cdot \text{curl } \underline{A} = \oint d\underline{x} \cdot \underline{A}$$

$\nabla \cdot T = \sum_{i,j}^3 \frac{\partial T_{ij}}{\partial x_j} e_i$

$$\nabla u = \sum_{i=1}^3 \sum_{j=1}^3 \frac{\partial u_i}{\partial x_j} e_i e_j ; \quad \nabla \cdot T = \frac{\partial}{\partial x_k} (T_{ij})$$

$$\nabla \times \nabla T = 0 = \epsilon_{ijk} \frac{\partial}{\partial x_j} \left(\frac{\partial T}{\partial x_k} \right) = -\epsilon_{ikj} \frac{\partial}{\partial x_k} \left(\frac{\partial T}{\partial x_j} \right) = -\nabla \times \nabla T$$

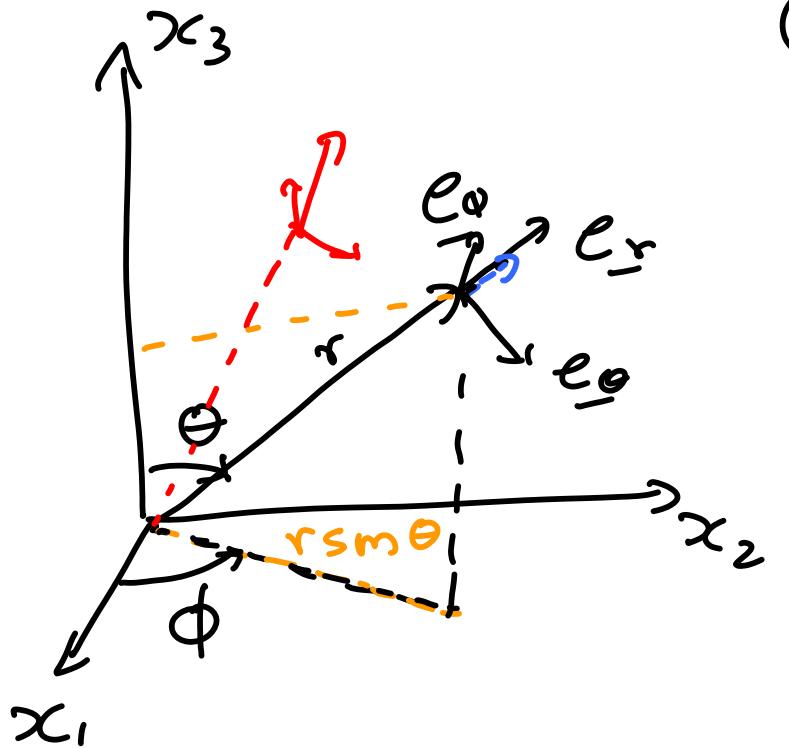
If $\nabla \times \underline{A} = 0$, then \underline{A} can be written as $\nabla \phi$

$$\nabla \cdot (\nabla \times \underline{A}) = 0$$

If $\nabla \cdot \underline{B} = 0$, then \underline{B} can be expressed as $\nabla \times \underline{A}$

$$A \times B \times C = \underbrace{\epsilon_{ijk}}_{i,j,k} \underbrace{A_i}_{j} \underbrace{(\epsilon_{klm}}_{k,l,m} B_l C_m)$$

$$\epsilon_{ijk} \epsilon_{klm} = \delta_{il} \delta_{jm} - \delta_{im} \delta_{jl}$$


 (r, θ, ϕ)

$(r \rightarrow r + \Delta r)$

$(\theta \rightarrow \theta + \Delta \theta)$

$(\phi \rightarrow \phi + \Delta \phi)$

Dustana taweled

Δr

$r \Delta \theta$

$r \sin \theta \Delta \phi$

$$\begin{aligned}\Delta \underline{x} &= \Delta r \underline{e}_r + r \Delta \theta \underline{e}_\theta + r \sin \theta \Delta \phi \underline{e}_\phi \\ &= S_a \underline{e}_a \Delta x_a + S_b \underline{e}_b \Delta x_b + S_c \underline{e}_c \Delta x_c\end{aligned}$$

$\Delta T = \Delta \underline{x} \cdot \nabla T$

$$\begin{aligned}\nabla T &= \underline{e}_1 \frac{\partial T}{\partial x_1} + \underline{e}_2 \frac{\partial T}{\partial x_2} + \underline{e}_3 \frac{\partial T}{\partial x_3} \\ &= \underline{e}_r \frac{\partial T}{\partial r} + \frac{\underline{e}_\theta}{r} \frac{\partial T}{\partial \theta} + \frac{\underline{e}_\phi}{r \sin \theta} \frac{\partial T}{\partial \phi}\end{aligned}$$

$$\nabla T = \frac{\underline{e}_a}{S_a} \frac{\partial T}{\partial x_a} + \frac{\underline{e}_b}{S_b} \frac{\partial T}{\partial x_b} + \frac{\underline{e}_c}{S_c} \frac{\partial T}{\partial x_c}$$

$$\nabla A = \left(\frac{\underline{e}_a}{S_a} \frac{\partial}{\partial x_a} + \frac{\underline{e}_b}{S_b} \left(\frac{\partial}{\partial x_b} + \frac{\underline{e}_c}{S_c} \frac{\partial}{\partial x_c} \right) \right) \cdot \left(A_a \underline{e}_a + A_b \underline{e}_b + A_c \underline{e}_c \right)$$

$$\Delta \underline{x} = \underline{e}_a S_a \Delta x_a + \underline{e}_b S_b \Delta x_b + \underline{e}_c S_c \Delta x_c$$

$$\frac{\partial \underline{x}}{\partial x_a} = \underline{e}_a S_a$$

$$\frac{\partial \underline{x}}{\partial x_b} = \underline{e}_b S_b$$

$$\frac{\partial}{\partial x_b} \left(\frac{\partial \underline{x}}{\partial x_a} \right) = \boxed{S_a \frac{\partial \underline{e}_a}{\partial x_b}} + \underline{e}_a \frac{\partial S_a}{\partial x_b} \quad ; \quad \frac{\partial}{\partial x_a} \left(\frac{\partial \underline{x}}{\partial x_b} \right) = \frac{\partial \underline{e}_b}{\partial x_a} S_b + \boxed{\underline{e}_b \frac{\partial S_b}{\partial x_a}}$$

$$\frac{\partial \underline{e}_a}{\partial x_b} = \frac{\underline{e}_b}{S_a} \frac{\partial S_b}{\partial x_a}$$

Spherical co-ordinate system

$$S_r = 1 \quad S_\theta = r \quad S_\phi = rs\sin\theta$$

$$\frac{\partial \underline{e}_a}{\partial x_b} = \frac{\underline{e}_b}{S_a} \frac{\partial S_b}{\partial x_a}$$

$$\frac{\partial \underline{e}_r}{\partial \theta} = \frac{\underline{e}_\theta}{S_r} \frac{\partial S_\theta}{\partial r} = \underline{e}_\theta$$

$$\frac{\partial \underline{e}_r}{\partial \phi} = \frac{\underline{e}_\phi}{S_r} \frac{\partial S_\phi}{\partial r} = \sin\theta \underline{e}_\phi$$

$$\begin{aligned}\frac{\partial \underline{e}_a}{\partial x_a} &= \frac{\partial}{\partial x_a} (\underline{e}_b \times \underline{e}_c) = \frac{\partial \underline{e}_b}{\partial x_a} \times \underline{e}_c + \underline{e}_b \times \frac{\partial \underline{e}_c}{\partial x_a} \\ &= \frac{\underline{e}_a}{S_b} \frac{\partial S_b}{\partial x_a} \times \underline{e}_c + \underline{e}_b \times \frac{\underline{e}_a}{S_c} \frac{\partial S_c}{\partial x_a} \\ &= -\frac{\underline{e}_b}{S_b} \frac{\partial S_a}{\partial x_b} - \frac{\underline{e}_c}{S_c} \frac{\partial S_a}{\partial x_c}\end{aligned}$$

$$\operatorname{div} \underline{A} = \left(\frac{e_a}{S_a} \frac{\partial}{\partial x_a} + \frac{e_b}{S_b} \frac{\partial}{\partial x_b} + \frac{e_c}{S_c} \frac{\partial}{\partial x_c} \right) \cdot \left(\underline{A}_a \underline{e}_a + A_b \underline{e}_b + A_c \underline{e}_c \right)$$

$$= \frac{e_a}{S_a} \frac{\partial}{\partial x_a} \cdot (A_a \underline{e}_a + A_b \underline{e}_b + A_c \underline{e}_c)$$

$$= \frac{e_a}{S_a} \cdot \left(e_a \frac{\partial A_a}{\partial x_a} + A_a \frac{\partial \underline{e}_a}{\partial x_a} + e_b \frac{\partial A_b}{\partial x_a} + A_b \frac{\partial \underline{e}_b}{\partial x_a} + e_c \frac{\partial A_c}{\partial x_a} + A_c \frac{\partial \underline{e}_c}{\partial x_a} \right)$$

$$= \frac{1}{S_a} \frac{\partial A_a}{\partial x_a} + \frac{e_a}{S_a} \cdot \left(A_b \frac{e_a}{S_b} \frac{\partial S_b}{\partial x_b} \right) + \frac{e_a}{S_a} \cdot \left(A_c \frac{e_a}{S_c} \frac{\partial S_c}{\partial x_c} \right)$$

$$= \frac{1}{S_a} \frac{\partial A_a}{\partial x_a} + \frac{A_b}{S_a S_b} \frac{\partial S_b}{\partial x_b} + \frac{A_c}{S_a S_c} \frac{\partial S_c}{\partial x_c}$$

$$+ \frac{1}{S_b} \frac{\partial A_b}{\partial x_b} + \frac{A_a}{S_a S_b} \frac{\partial S_a}{\partial x_a} + \frac{A_c}{S_b S_c} \frac{\partial S_c}{\partial x_c}$$

$$+ \frac{1}{S_c} \frac{\partial A_c}{\partial x_c} + \frac{A_a}{S_a S_c} \frac{\partial S_a}{\partial x_a} + \frac{A_b}{S_b S_c} \frac{\partial S_b}{\partial x_b}$$

$$d\omega A = \frac{1}{S_a S_b S_c} \left[\frac{\partial}{\partial x_a} (S_b S_c A_a) + \frac{\partial}{\partial x_b} (S_c S_a A_b) + \frac{\partial}{\partial x_c} (S_a S_b A_c) \right]$$

$$S_r = 1 \quad S_\theta = r \quad S_\phi = r \sin \theta$$

$$\begin{aligned} d\omega A &= \frac{1}{r^2 \sin \theta} \left[\frac{\partial}{\partial r} (r^2 \sin \theta A_r) + \frac{\partial}{\partial \theta} (r \sin \theta A_\theta) + \frac{\partial}{\partial \phi} (r A_\phi) \right] \\ &= \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 A_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta A_\theta) + \frac{1}{r \sin \theta} \frac{\partial A_\phi}{\partial \phi} \end{aligned}$$

$$\text{curl } \underline{A} = \frac{1}{S_a S_b S_c} \begin{vmatrix} S_a \underline{e}_q & S_b \underline{e}_b & S_c \underline{e}_c \\ \frac{\partial}{\partial x_a} & \frac{\partial}{\partial x_b} & \frac{\partial}{\partial x_c} \\ \underline{S_a A_a} & \underline{S_b A_b} & \underline{S_c A_c} \end{vmatrix}$$

$$\nabla \cdot \nabla T = \nabla^2 T$$

$$= \frac{1}{S_a S_b S_c} \left[\frac{\partial}{\partial x_a} \left(S_b S_c \frac{1}{S_a} \frac{\partial T}{\partial x_a} \right) + \frac{\partial}{\partial x_b} \left(S_a S_c \frac{1}{S_b} \frac{\partial T}{\partial x_b} \right) \right. \\ \left. + \frac{\partial}{\partial x_c} \left(\frac{S_a S_b}{S_c} \frac{\partial T}{\partial x_c} \right) \right]$$

$$= \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \\ \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2}$$

Kinematics:

q_f = Energy (area \times time)

$$\int ds q_f \cdot n = \int dV \operatorname{div} \underline{q}_f$$

Amount of fluid in

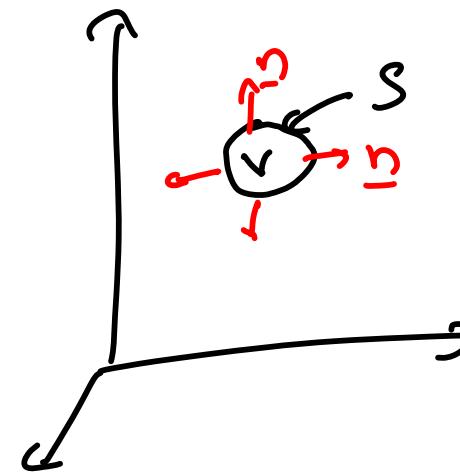
$$\text{volume } \Delta V = S \Delta V$$

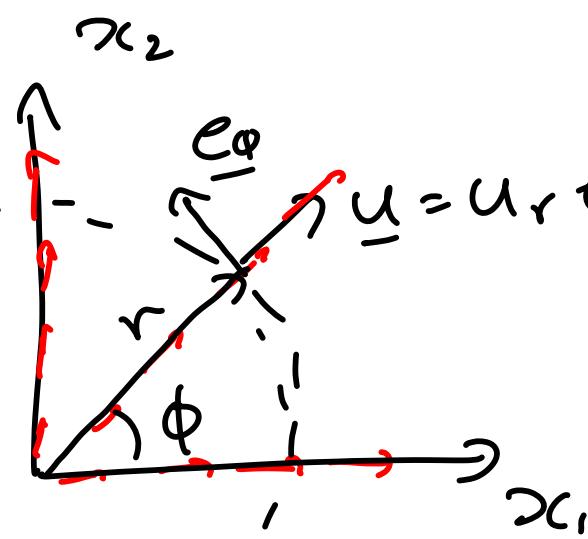
\dot{S}_U = Mass / (Area \times Time)

$$\int ds (\dot{S}_U) n = \int dV \operatorname{div} (\dot{S}_U)$$

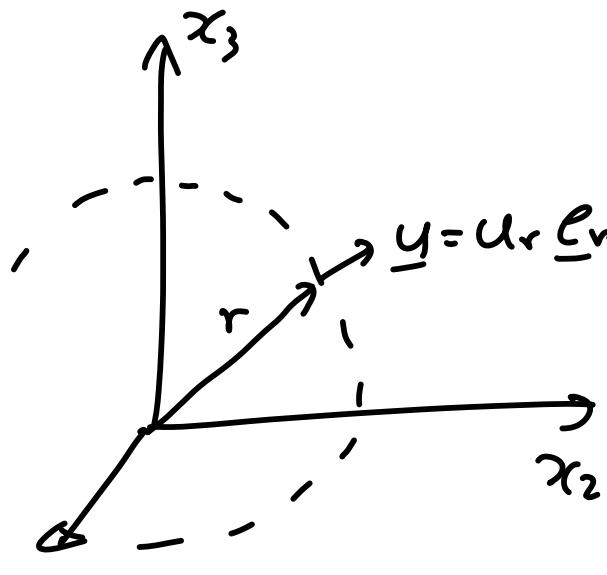
'Incompressible' constant density

$$\operatorname{div} \underline{u} = 0 \text{ or } \nabla \cdot \underline{u} = 0$$




 x_2
 e_ϕ

$$\underline{u} = u_r \underline{e}_r = C r \underline{e}_r$$


 x_3
 x_2

$$u_1 = \frac{u_r x_1}{r} \quad u_2 = \frac{u_r x_2}{r}$$

$$u_1 = C x_1$$

$$u_2 = C x_2$$

$$d\omega \underline{u} = 2C$$

$$\underline{e}_r = \underline{e}_1 \cos \phi + \underline{e}_2 \sin \phi$$

$$\underline{e}_\phi = -\underline{e}_1 \sin \phi + \underline{e}_2 \cos \phi$$

$$r = \sqrt{x_1^2 + x_2^2}; \quad x_1 = r \cos \phi, \quad x_2 = r \sin \phi$$

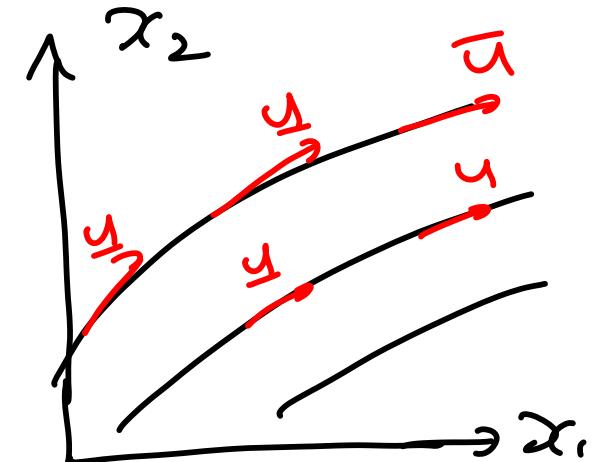
$$u_r = u_r \underline{e}_r = u_r [\underline{e}_1 \cos \phi + \underline{e}_2 \sin \phi]$$

$$u_1 = u_r \cos \phi \quad u_2 = u_r \sin \phi$$

Incompressible fluids

$$\nabla \cdot \underline{u} = 0 \Rightarrow \underline{u} = \nabla \times \Psi$$

$$\begin{aligned}\nabla \Psi \cdot \underline{u} &= \frac{\partial \Psi}{\partial x_1} u_1 + \frac{\partial \Psi}{\partial x_2} u_2 \\ &= \frac{\partial \Psi}{\partial x_1} \left(\frac{\partial \Psi}{\partial x_2} \right) + \frac{\partial \Psi}{\partial x_2} \left(-\frac{\partial \Psi}{\partial x_1} \right) \\ &= 0\end{aligned}$$



Stream function Ψ

$$\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} = 0$$

$$\begin{aligned}u_1 &= e_1 \frac{\partial \Psi}{\partial x_2} - e_2 \frac{\partial \Psi}{\partial x_1} \\ u_2 &= -e_1 \frac{\partial \Psi}{\partial x_2} - e_2 \frac{\partial \Psi}{\partial x_1}\end{aligned}$$

$$Q = \int_A^B ds \underline{u} \cdot \underline{n}$$

$$= \int_A^B ds (u_1 n_1 + u_2 n_2)$$

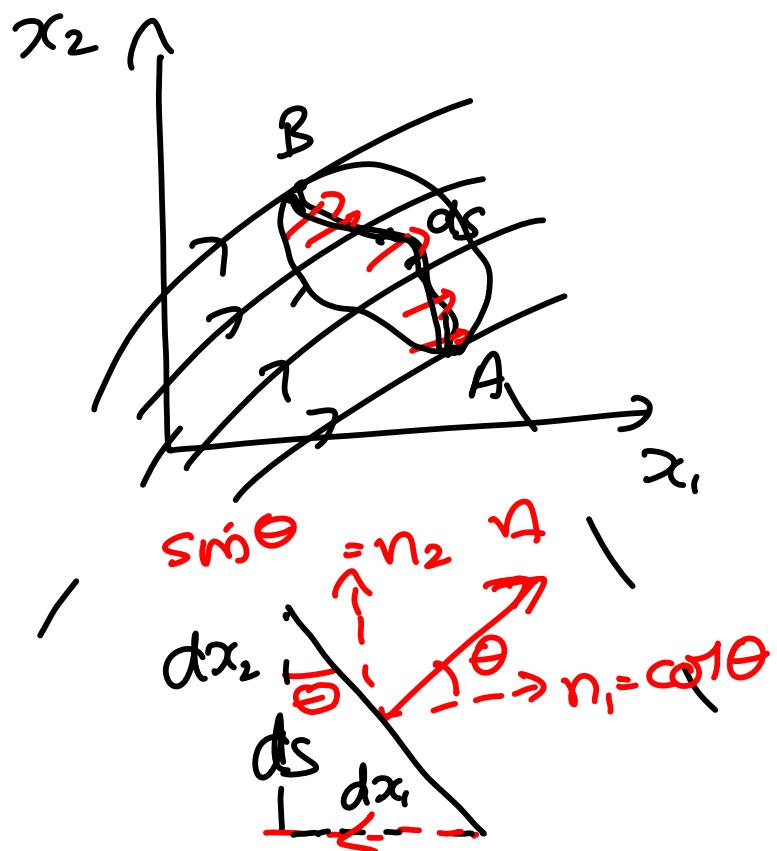
$$= \int_A^B ds \left(\frac{\partial \Psi}{\partial x_2} n_1 - \frac{\partial \Psi}{\partial x_1} n_2 \right)$$

$$n_1 ds = dx_2$$

$$n_2 ds = -dx_1$$

$$Q = \int_A^B \left[dx_2 \frac{\partial \Psi}{\partial x_2} + dx_1 \frac{\partial \Psi}{\partial x_1} \right]$$

$$= \int_A^B d\underline{x} \cdot \nabla \Psi = \Psi(\underline{x}_B) - \Psi(\underline{x}_A)$$



$$\nabla \times \underline{u} = \left(\frac{\partial u_2}{\partial x_1} - \frac{\partial u_1}{\partial x_2} \right) \underline{e}_3 = 2\Omega \underline{e}_3 = \underline{\omega}$$

$$\int ds \ \underline{v} \cdot (\nabla \times \underline{u}) = \oint dx \cdot \underline{u}$$

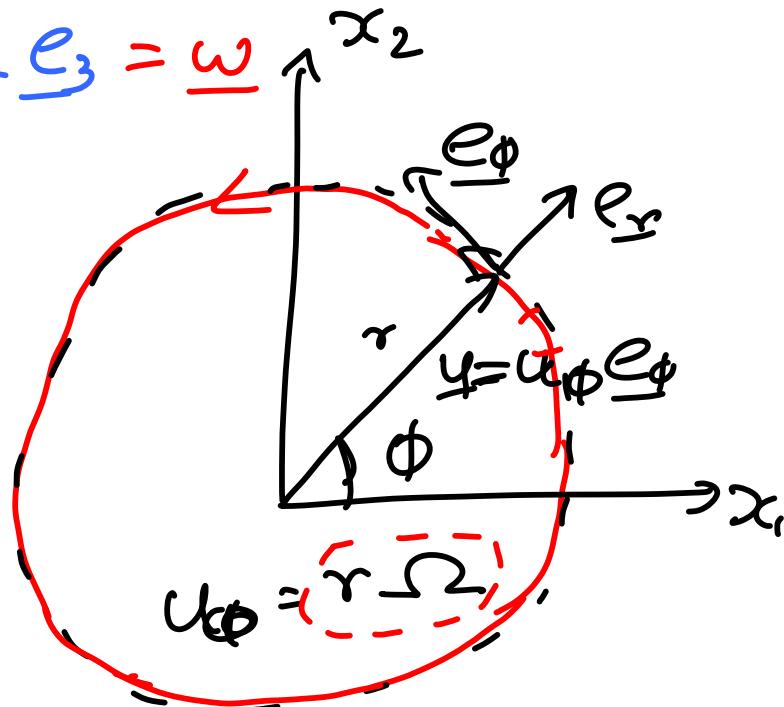
$$\int ds \ 2\Omega = 2\Omega \pi r^2$$

$$\begin{aligned} \oint dx \cdot \underline{u} &= \int_{2\pi}^{2\pi} r d\phi \ u_\phi \\ &= \int_0^{2\pi} r d\phi \ \Omega r \\ &= 2\pi r^2 \Omega \end{aligned}$$

If $\nabla \times \underline{u} = 0$; $\underline{u} = \nabla \phi$

Velocity potential

$$u = e_1 \frac{\partial \phi}{\partial x_1} + e_2 \frac{\partial \phi}{\partial x_2} + e_3 \frac{\partial \phi}{\partial x_3}$$



$$u_1 = \frac{\partial \phi}{\partial x_1} \quad u_2 = \frac{\partial \phi}{\partial x_2} \quad u_3 = \frac{\partial \phi}{\partial x_3}$$

$$u_1 = \frac{\partial \psi}{\partial x_1} \quad u_2 = -\frac{\partial \psi}{\partial x_2}$$

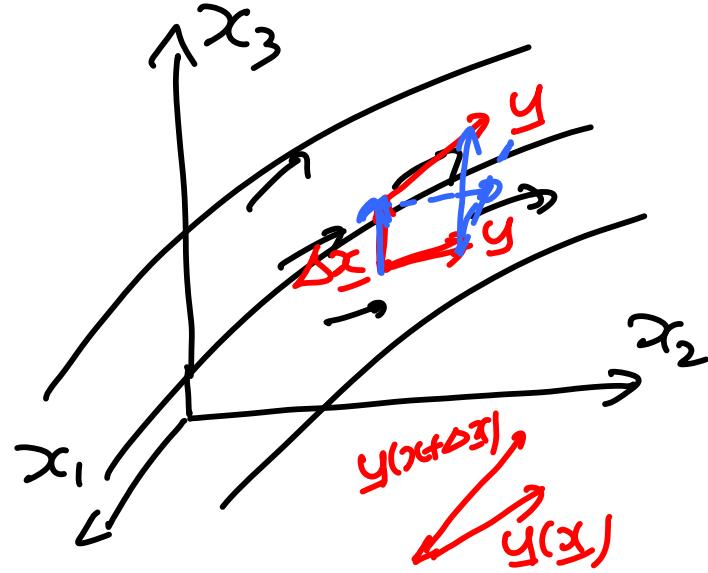
$$\begin{aligned} (\nabla \phi) \cdot (\nabla \psi) &= \left(\frac{\partial \phi}{\partial x_1} \right) \left(\frac{\partial \psi}{\partial x_1} \right) + \left(\frac{\partial \phi}{\partial x_2} \right) \left(\frac{\partial \psi}{\partial x_2} \right) \\ &= u_1 (-u_2) + (u_2)(u_1) \end{aligned}$$

$$= 0$$

Gradient of velocity Rate of deformation tensor:

$$\nabla \underline{u} = \sum_{i=1}^3 \sum_{j=1}^3 \frac{\partial u_i}{\partial x_j} \underline{e}_i \underline{e}_j$$

$$= \begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_1}{\partial x_2} & \frac{\partial u_1}{\partial x_3} \\ \frac{\partial u_2}{\partial x_1} & \frac{\partial u_2}{\partial x_2} & \frac{\partial u_2}{\partial x_3} \\ \frac{\partial u_3}{\partial x_1} & \frac{\partial u_3}{\partial x_2} & \frac{\partial u_3}{\partial x_3} \end{pmatrix}$$



$$\begin{aligned} u(x + \Delta x) - u(x) &= \Delta x \cdot \nabla u \\ &= \Delta x_j \left(\frac{\partial u_i}{\partial x_j} \right) \end{aligned}$$

$$\nabla u = \begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_1}{\partial x_2} & \frac{\partial u_1}{\partial x_3} \\ \frac{\partial u_2}{\partial x_1} & \frac{\partial u_2}{\partial x_2} & \frac{\partial u_2}{\partial x_3} \\ \frac{\partial u_3}{\partial x_1} & \frac{\partial u_3}{\partial x_2} & \frac{\partial u_3}{\partial x_3} \end{pmatrix} \quad | \quad (\nabla u^T) = \begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_2}{\partial x_1} & \frac{\partial u_3}{\partial x_1} \\ \frac{\partial u_1}{\partial x_2} & \frac{\partial u_2}{\partial x_2} & \frac{\partial u_3}{\partial x_2} \\ \frac{\partial u_1}{\partial x_3} & \frac{\partial u_2}{\partial x_3} & \frac{\partial u_3}{\partial x_3} \end{pmatrix}$$

$$\frac{\partial u_i}{\partial x_j} = S_{ij} + A_{ij}$$

$$S_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \quad | \quad A_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} - \frac{\partial u_j}{\partial x_i} \right)$$

$$S_{ij} = \begin{pmatrix} \frac{\partial u_1}{\partial x_1}, & \frac{1}{2} \left(\frac{\partial u_1}{\partial x_2} + \frac{\partial u_2}{\partial x_1} \right), & \frac{1}{2} \left(\frac{\partial u_1}{\partial x_3} + \frac{\partial u_3}{\partial x_1} \right) \\ \frac{1}{2} \left(\frac{\partial u_1}{\partial x_2} + \frac{\partial u_2}{\partial x_1} \right), & \frac{\partial u_2}{\partial x_2}, & \frac{1}{2} \left(\frac{\partial u_2}{\partial x_3} + \frac{\partial u_3}{\partial x_2} \right) \\ \frac{1}{2} \left(\frac{\partial u_1}{\partial x_3} + \frac{\partial u_3}{\partial x_1} \right), & \frac{1}{2} \left(\frac{\partial u_2}{\partial x_3} + \frac{\partial u_3}{\partial x_2} \right), & \frac{\partial u_3}{\partial x_3} \end{pmatrix}$$

$$= \begin{pmatrix} \frac{1}{3} \left(\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} + \frac{\partial u_3}{\partial x_3} \right), & 0, & 0 \\ 0, & \frac{1}{3} \left(\frac{\partial u_1}{\partial x_2} + \frac{\partial u_2}{\partial x_1} + \frac{\partial u_3}{\partial x_3} \right), & 0 \\ 0, & 0, & \frac{1}{3} \left(\frac{\partial u_1}{\partial x_3} + \frac{\partial u_2}{\partial x_2} + \frac{\partial u_3}{\partial x_1} \right) \end{pmatrix} + \boxed{E_{ij}}$$

KINEMATICS



$$\boxed{\underline{A} \cdot \underline{B}} = A_1 B_1 + A_2 B_2 + A_3 B_3$$

$$\boxed{\underline{A} \times \underline{B}} = \epsilon_{ijk} A_j B_k$$

$$\nabla \underline{u} = \frac{\partial \underline{u}_j}{\partial x_i}$$

$$\nabla \cdot \underline{u} = \text{div } \underline{u} = \frac{\partial u_i}{\partial x_i}$$

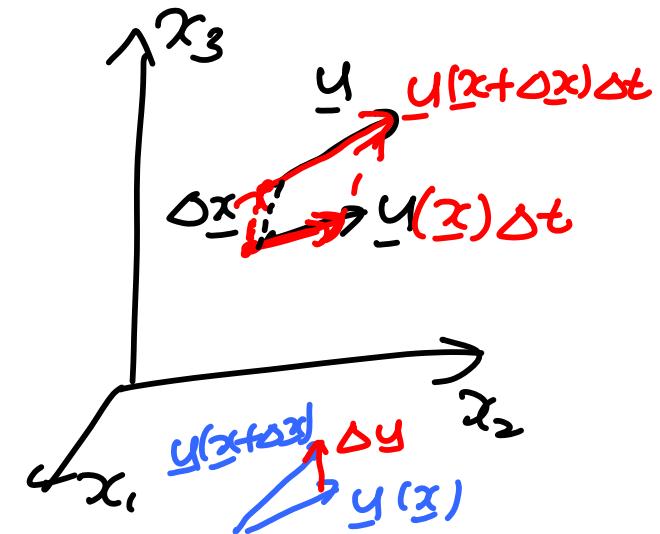
$$\int ds \underline{n} \cdot \underline{u} = \int dV (\text{div } \underline{u})$$

$$\underline{\omega} = \nabla \times \underline{u} = \epsilon_{ijk} \frac{\partial}{\partial x_j} u_k$$

$$\int ds \underline{n} \cdot \nabla \times \underline{u} = \oint d\underline{x} \cdot \underline{u}$$

Rate of deformation tensor:

$$\nabla \underline{u} = \frac{\partial u_i}{\partial x_j} = \begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_1}{\partial x_2} & \frac{\partial u_1}{\partial x_3} \\ \frac{\partial u_2}{\partial x_1} & \frac{\partial u_2}{\partial x_2} & \frac{\partial u_2}{\partial x_3} \\ \frac{\partial u_3}{\partial x_1} & \frac{\partial u_3}{\partial x_2} & \frac{\partial u_3}{\partial x_3} \end{pmatrix}$$

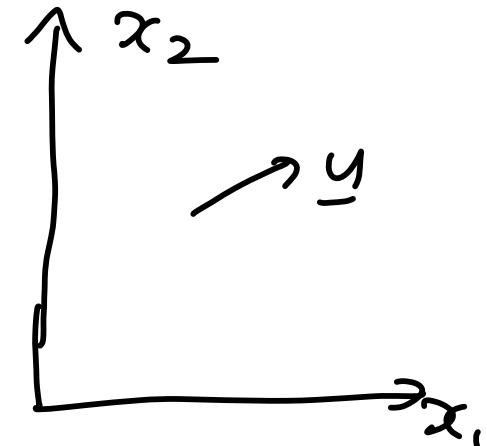


$$\frac{[u(x+\Delta x) - u(x)]}{\Delta x} = \Delta x \cdot \nabla \underline{u}$$

$$\Delta u_i = \Delta x_j \left[\frac{\partial u_i}{\partial x_j} \right]$$

$$[u(x+\Delta x) - u(x)] \Delta t = \left[\Delta x_j \frac{\partial u_i}{\partial x_j} \Delta t \right]$$

$$\nabla u = \frac{\partial u_i}{\partial x_j} = \begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_1}{\partial x_2} \\ \frac{\partial u_2}{\partial x_1} & \frac{\partial u_2}{\partial x_2} \end{pmatrix}$$



$$= S_{ij} + A_{ij}$$

$$S_{ij} = \frac{1}{2} \left[\frac{\partial u_i}{\partial x_j} + \left(\frac{\partial u_i}{\partial x_j} \right)^T \right] = \frac{1}{2} \left[\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right]$$

$$A_{ij} = \frac{1}{2} \left[\frac{\partial u_i}{\partial x_j} - \left(\frac{\partial u_i}{\partial x_j} \right)^T \right] = \frac{1}{2} \left[\frac{\partial u_i}{\partial x_j} - \frac{\partial u_j}{\partial x_i} \right]$$

$$S_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) = \begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{1}{2} \left(\frac{\partial u_1}{\partial x_2} + \frac{\partial u_2}{\partial x_1} \right) \\ \frac{1}{2} \left(\frac{\partial u_1}{\partial x_2} + \frac{\partial u_2}{\partial x_1} \right) & \frac{\partial u_2}{\partial x_2} \end{pmatrix}$$

$$= \begin{pmatrix} \frac{1}{2} \left(\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} \right) & 0 \\ 0 & \frac{1}{2} \left(\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} \right) \end{pmatrix} + \underbrace{\begin{pmatrix} \frac{\partial u_1}{\partial x_1} - \frac{1}{2} \left(\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} \right) & \frac{1}{2} \left(\frac{\partial u_1}{\partial x_2} + \frac{\partial u_2}{\partial x_1} \right) \\ \frac{1}{2} \left(\frac{\partial u_1}{\partial x_2} + \frac{\partial u_2}{\partial x_1} \right) & \frac{\partial u_2}{\partial x_2} - \frac{1}{2} \left(\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} \right) \end{pmatrix}}_{E_{ij}}$$

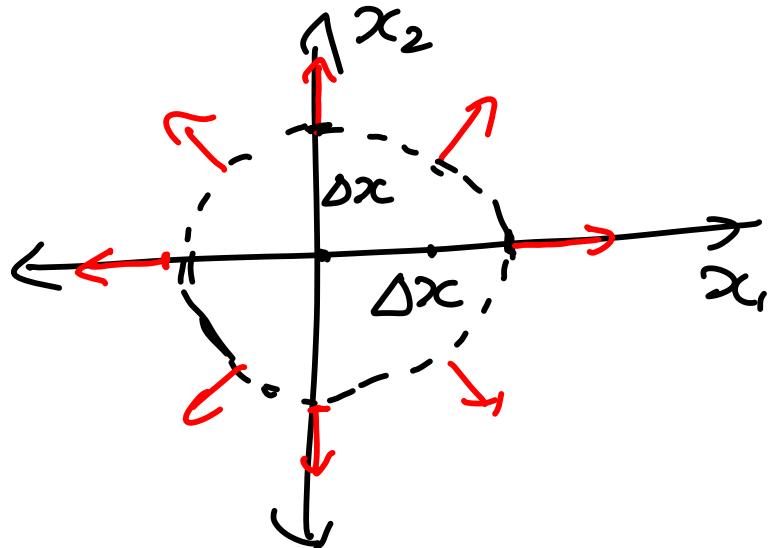
$$= \frac{1}{2} \left(\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} \right) \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} + E_{ij}$$

$$= \frac{1}{2} (\nabla \cdot \underline{u}) \delta_{ij} + E_{ij}$$

$$\frac{\partial u_i}{\partial x_j} = A_{ij} + E_{ij} + \frac{1}{2}(\nabla \cdot \underline{y}) \delta_{ij}$$

Isotropic

$$\begin{pmatrix} \Delta u_1 \\ \Delta u_2 \end{pmatrix} = \begin{pmatrix} S & 0 \\ 0 & S \end{pmatrix} \begin{pmatrix} \Delta x_1 \\ \Delta x_2 \end{pmatrix}$$



$$\Delta u_1 = S \Delta x_1$$

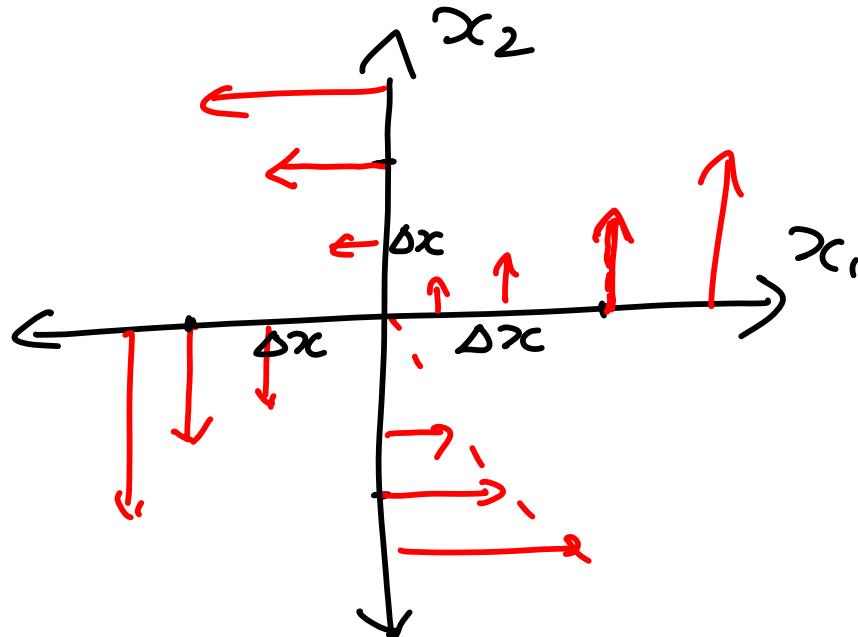
$$\Delta u_2 = S \Delta x_2$$

$$u_r = C r$$

$$\begin{pmatrix} \Delta u_1 \\ \Delta u_2 \end{pmatrix} = \begin{pmatrix} 0 & -a \\ a & 0 \end{pmatrix} \begin{pmatrix} \Delta x_1 \\ \Delta x_2 \end{pmatrix}$$

$$\Delta u_1 = -a \underline{\Delta x_2}$$

$$\Delta u_2 = a \underline{\Delta x_1}$$



$$w_i = \epsilon_{ijk} \frac{\partial (u_k)}{\partial x_j} = \nabla \times \underline{u}$$

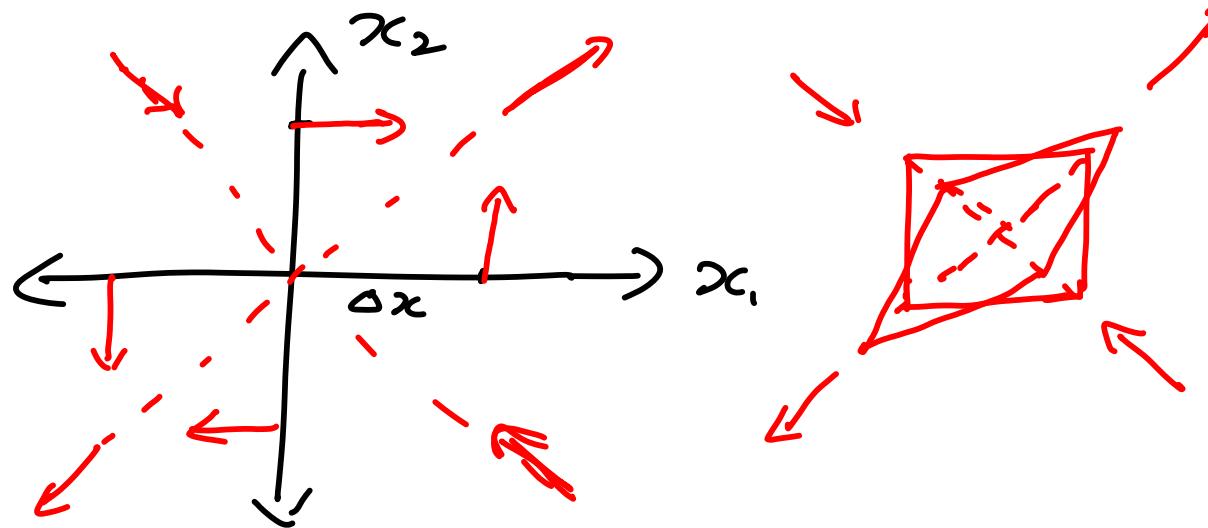
$$= \epsilon_{ikj} \frac{\partial u_i}{\partial x_k}$$

$$w_i = \frac{1}{2} \left(\epsilon_{ijk} \frac{\partial u_k}{\partial x_j} + \epsilon_{ikj} \frac{\partial u_j}{\partial x_k} \right)$$

$$= \frac{1}{2} \epsilon_{ijk} \left(\frac{\partial u_k}{\partial x_j} - \frac{\partial u_j}{\partial x_k} \right) = \epsilon_{ijk} A_{kj}$$

Symmetric traceless

$$\begin{pmatrix} \Delta u_1 \\ \Delta u_2 \end{pmatrix} = \begin{pmatrix} 0 & s \\ s & 0 \end{pmatrix} \begin{pmatrix} \Delta x_1 \\ \Delta x_2 \end{pmatrix} \quad \left| \begin{array}{l} \Delta u_1 = s \Delta x_2 \\ \Delta u_2 = s \Delta x_1 \end{array} \right.$$

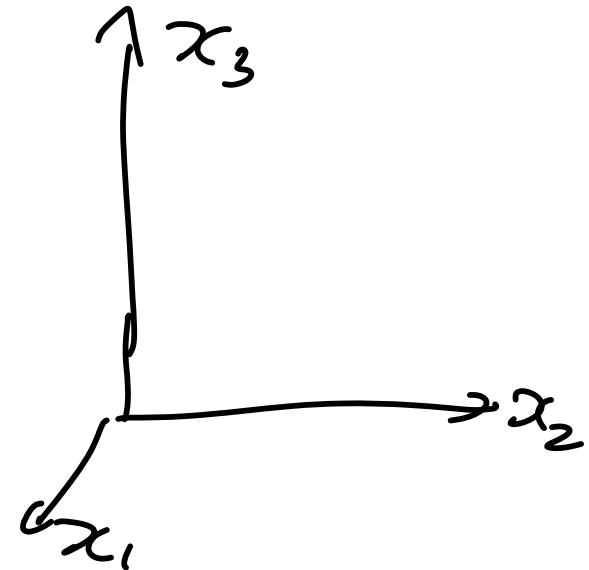


Pure extensional strain

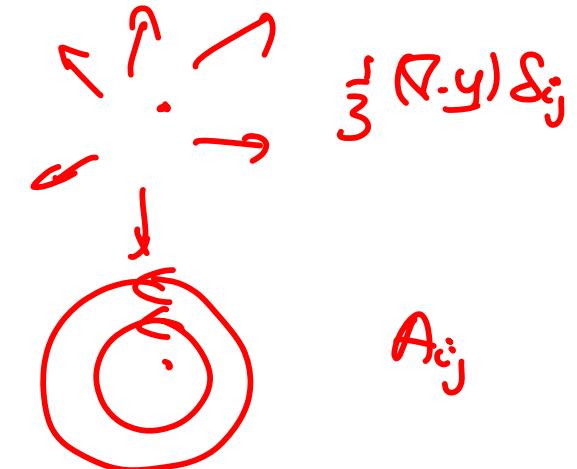
$$\frac{\partial u_i}{\partial x_j} = A_{ij} + \frac{1}{3} (\nabla \cdot \underline{y}) \delta_{ij} + E_{ij}$$

$$\left(\begin{array}{ccc} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_1}{\partial x_2} & \frac{\partial u_1}{\partial x_3} \\ \frac{\partial u_2}{\partial x_1} & \frac{\partial u_2}{\partial x_2} & \frac{\partial u_2}{\partial x_3} \\ \frac{\partial u_3}{\partial x_1} & \frac{\partial u_3}{\partial x_2} & \frac{\partial u_3}{\partial x_3} \end{array} \right)$$

$$\text{Trace}(\nabla \underline{y}) = \frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} + \frac{\partial u_3}{\partial x_3} = \nabla \cdot \underline{y}$$



$$\frac{\underline{\partial u_i}}{\underline{\partial x_j}} = \underline{A_{ij}} + \underline{E_{ij}} + \underline{\frac{1}{3}(\nabla \cdot \underline{y})\delta_{ij}}$$



$$\frac{\underline{\partial u_1}}{\underline{\partial x_1}} + \frac{\underline{\partial u_2}}{\underline{\partial x_2}} + \frac{\underline{\partial u_3}}{\underline{\partial x_3}} = \frac{\underline{\partial u_i}}{\underline{\partial x_i}} = \delta_{ij} \frac{\underline{\partial u_i}}{\underline{\partial x_j}}$$

$$\delta_{ij} \frac{\underline{\partial u_i}}{\underline{\partial x_j}} = \delta_{ij} A_{ij} + \delta_{ij} E_{ij} + \frac{1}{3}(\nabla \cdot \underline{y}) \delta_{ij} \delta_{ij}$$

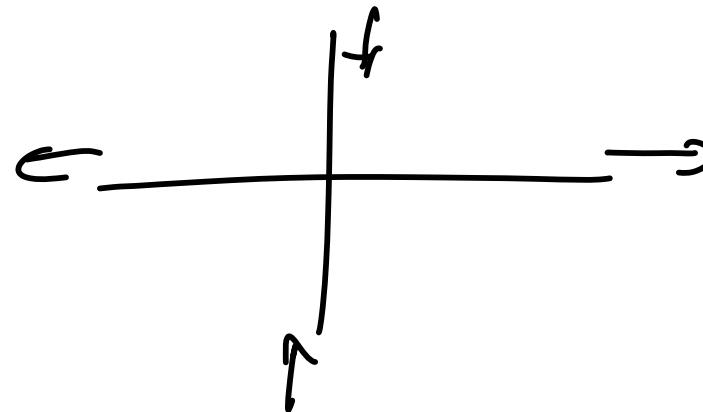
$$= 0 + E_{ii} + \frac{1}{3}(\nabla \cdot \underline{y}) \delta_{ii}$$

$$\cancel{\frac{\underline{\partial u_i}}{\underline{\partial x_i}}} = 0 + E_{ii} + (\cancel{\nabla \cdot \underline{y}})$$

$$E_{ii} = 0$$

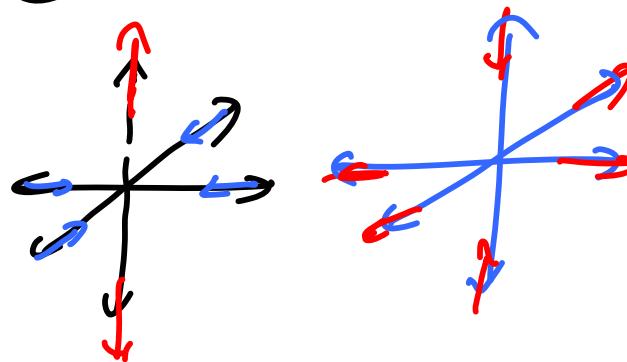
Symmetric traceless: ① One +ve & one -ve & one 0

$$E_{ij} = \begin{pmatrix} e_{11} & e_{12} & e_{13} \\ e_{12} & e_{22} & e_{23} \\ e_{13} & e_{23} & e_{33} \end{pmatrix}$$



- ① Three eigenvalues
- ② Three orthogonal eigenvectors.
- ③ Sum of eigenvalues = zero

② One +ve & two -ve



Rate of deformation tensor:

$$\nabla \underline{y} = \sum_{i=1}^3 \sum_{j=1}^3 \frac{\partial u_i}{\partial x_j} e_i e_j$$

$$\Delta \underline{y} = \nabla \underline{x} \cdot \nabla \underline{y}$$

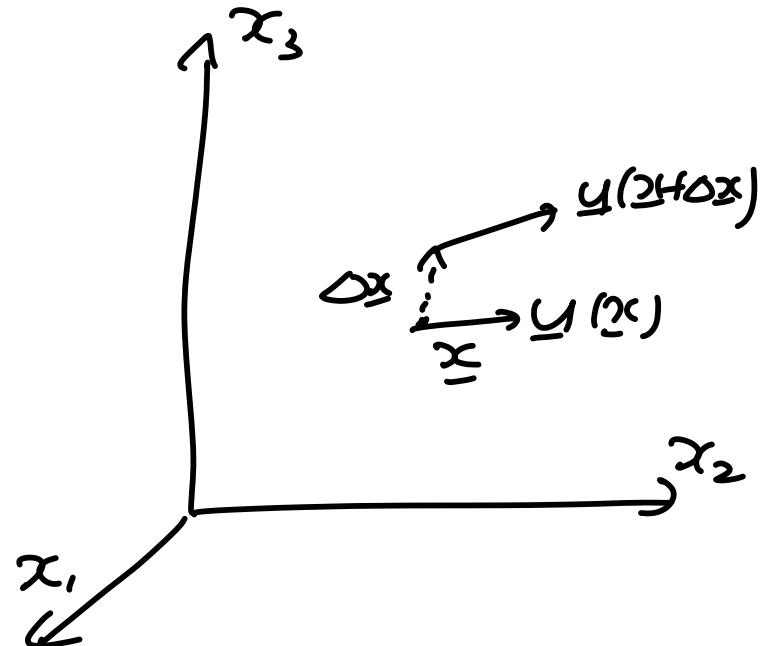
$$\nabla \underline{y} = S_{ij} + A_{ij}$$

$$S_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

$$A_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} - \frac{\partial u_j}{\partial x_i} \right)$$

$$S_{ij} = E_{ij} + \frac{1}{3} S_{ij} \left(\frac{\partial u_k}{\partial x_k} \right)$$

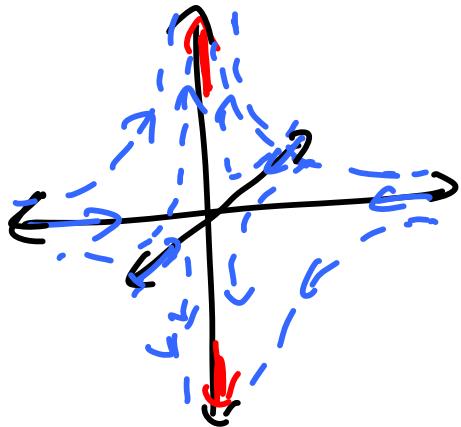
$$\text{Sum of diagonal elements} = E_{ii} = \sum_{i=1}^3 E_{ii}$$



$$\frac{\partial u_i}{\partial x_j} = A_{ij} + \frac{1}{3} \delta_{ij} \left(\frac{\partial u_k}{\partial x_k} \right) + E_{ij}$$

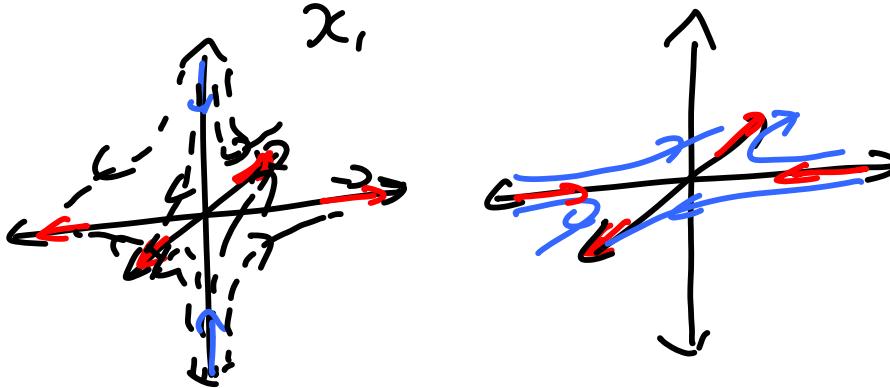
$$w_i = \epsilon_{ijk} \frac{\partial u_k}{\partial x_j} = \epsilon_{ijk} A_{kj}$$

$$E_{ij} = \begin{pmatrix} E_{11} & E_{12} & E_{13} \\ E_{12} & E_{22} & E_{23} \\ E_{13} & E_{23} & E_{33} \end{pmatrix}$$

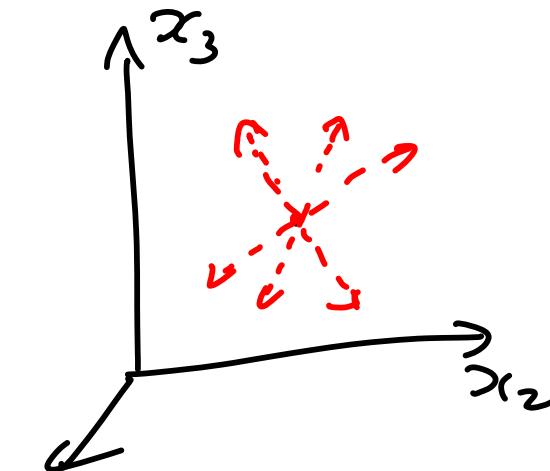


Uniaxial extension

Biaxial extension



Planar extension



Substantial derivative.

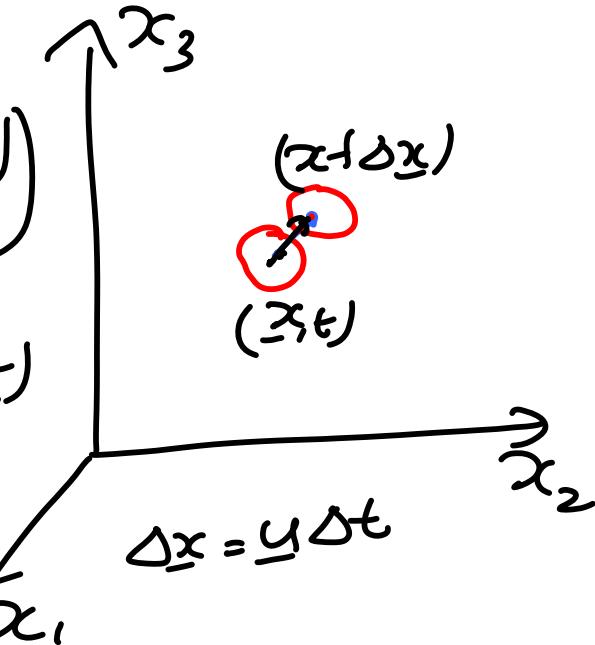
$$\frac{\partial T}{\partial t} = \lim_{\Delta t \rightarrow 0} \left(\frac{T(x_1, x_2, x_3, t + \Delta t) - T(x_1, x_2, x_3, t)}{\Delta t} \right)$$

'Eulerian reference frame' $T(\underline{x}, t)$

'Lagrangian reference frame'

$T(\underline{x}(t), t)$

$$\begin{aligned}\frac{DT}{Dt} &= \lim_{\Delta t \rightarrow 0} \left[\frac{T(\underline{x} + \underline{u} \Delta t, t + \Delta t) - T(\underline{x}, t)}{\Delta t} \right] \\ &= \left[\frac{\partial T}{\partial t} + u_1 \frac{\partial T}{\partial x_1} + u_2 \frac{\partial T}{\partial x_2} + u_3 \frac{\partial T}{\partial x_3} \right] = \frac{\partial T}{\partial t} + \underline{u} \cdot \nabla T\end{aligned}$$

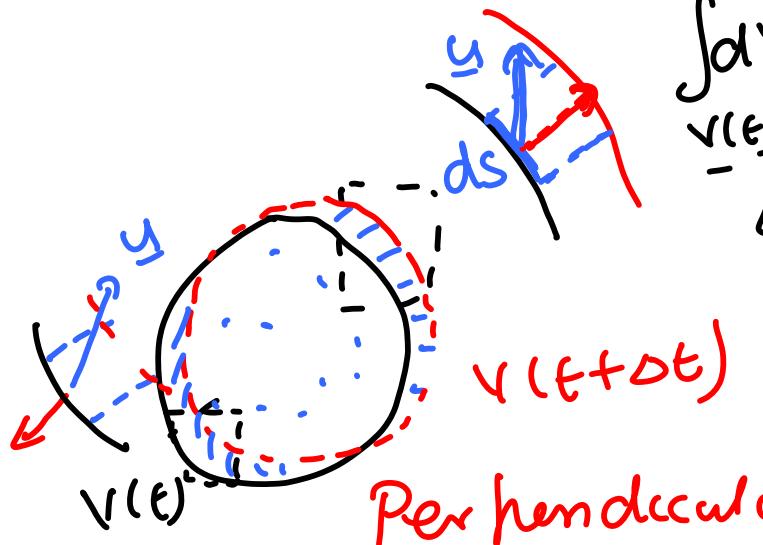


Mass in

$$= \int ds \underline{y} \cdot \underline{n} \Delta t$$

Rate of mass in

$$= \boxed{\int ds \underline{y} \cdot \underline{n}}$$



$$\text{Mass} = \int dV \underline{S}$$

$\underline{v}(t)$

Rate of change of mass = 0

$$= \frac{d}{dt} \left[\int dV \underline{S} \right] = 0$$

$$\int dV \underline{S} = \int dV \frac{\partial \underline{S}}{\partial t} + \boxed{\int dA \underline{S} \underline{y} \cdot \underline{n}}$$

Liebniz rule

Perpendicular distance varied

$$= \underline{y} \cdot \underline{n} \Delta t dA$$

$$\frac{d}{dt} \int_{V(t)} dV \rho = \int dV \frac{\partial \rho}{\partial t} + \int dS \rho \underline{u} \cdot \underline{n} = 0$$

$$\int dV \frac{\partial \rho}{\partial t} + \int dV \nabla \cdot (\rho \underline{u}) = 0$$

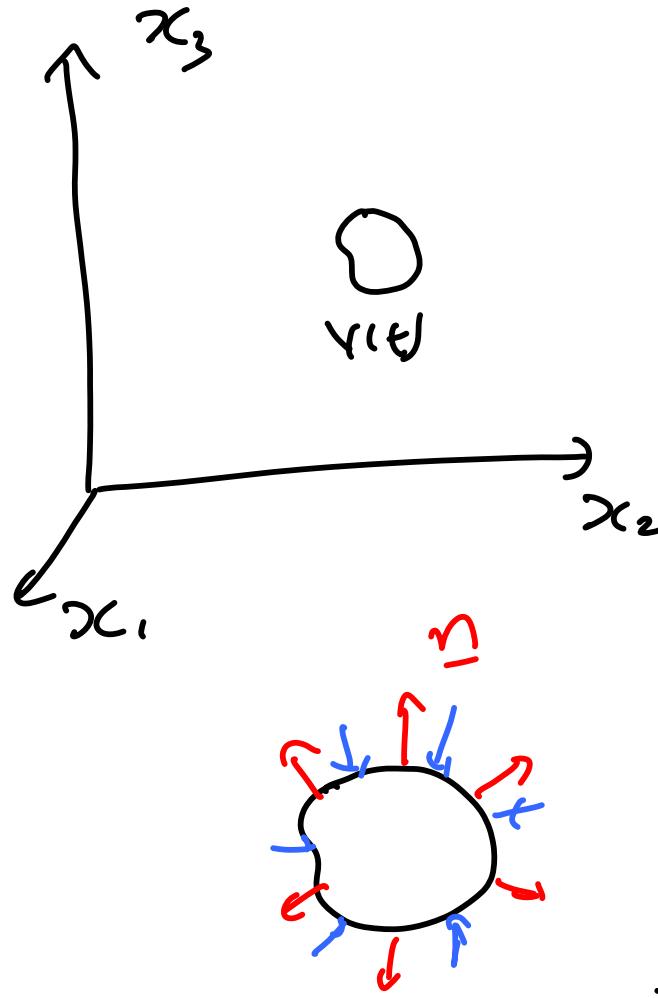
Mass conservation equation; Incompressible
 $\frac{\partial u_i}{\partial x_i} = 0 \quad \nabla \cdot \underline{u} = 0$

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{u}) = 0$$

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_i} (\rho u_i) = 0$$

$$\frac{\partial \rho}{\partial t} + u_i \frac{\partial \rho}{\partial x_i} + \rho \frac{\partial u_i}{\partial x_i} = 0$$

$$\frac{D\rho}{Dt} + \rho \frac{\partial u_i}{\partial x_i} = 0$$



$$\frac{d}{dt} \int dV c = - \int ds j \cdot n$$

$$\int dV \left[\frac{\partial c}{\partial t} \right] + \int dS c \underline{n} \cdot \underline{n} = - \int ds j \cdot n$$

$$\int dV \left(\frac{\partial c}{\partial t} \right) + \int dV \frac{\partial}{\partial x_i} (c u_i) = - \int dV \frac{\partial (j_i)}{\partial x_i}$$

$$\frac{\partial c}{\partial t} + \frac{\partial}{\partial x_i} (c u_i) = - \frac{\partial j_i}{\partial x_i}$$

$$\frac{\partial c}{\partial t} + \nabla \cdot (u c) = - \nabla \cdot j$$

$$j = - D \nabla c$$

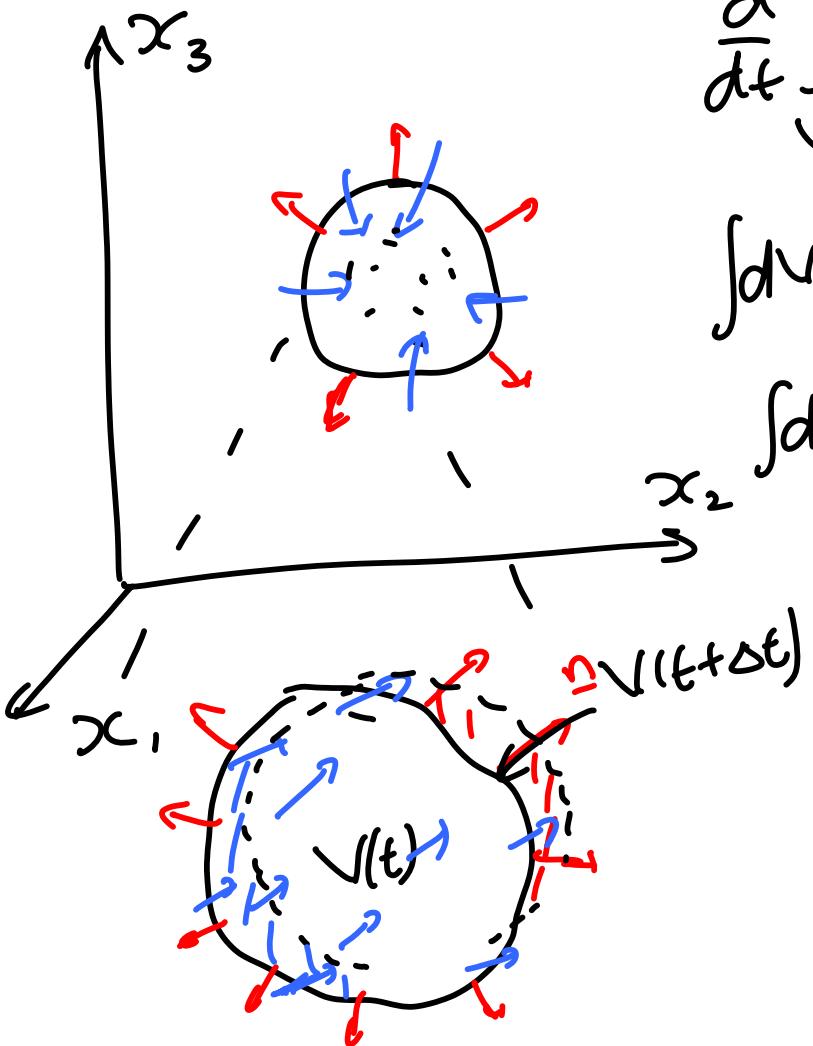
$$\frac{\partial c}{\partial t} + \nabla \cdot (u c) = \nabla \cdot (D \nabla c) \\ = D \nabla^2 c$$

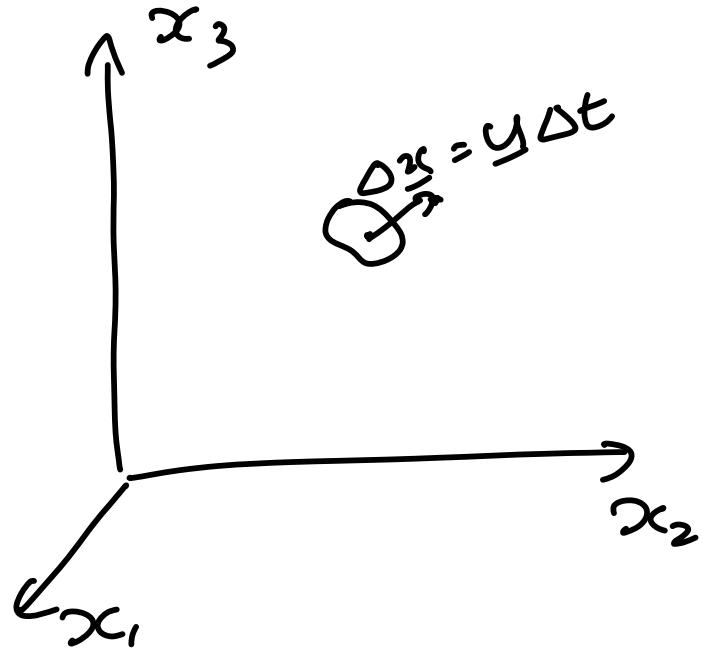
$$SC_v \left[\frac{\partial T}{\partial t} + \frac{\partial}{\partial x_i} (u_i T) \right] = \frac{\partial}{\partial x_i} \left(k \frac{\partial T}{\partial x_i} \right)$$

$$\begin{aligned} SC_v \left[\frac{\partial T}{\partial t} + \nabla \cdot (u T) \right] &= \nabla \cdot (k \nabla T) \\ &= k \nabla^2 T \end{aligned}$$

Mass conservation equations:

$$\frac{d}{dt} \int_{V(t)} dV c = \int dS (-\vec{j} \cdot \vec{n}) + \int dV S(x)$$
$$\int dV \left(\frac{\partial c}{\partial t} \right) + \int dS (c \vec{u} \cdot \vec{n}) = \int dS (-\vec{j} \cdot \vec{n}) + \int dV S(x)$$
$$\int dV \left[\frac{\partial c}{\partial t} + \nabla \cdot (c \vec{u}) \right] = \int dV (-\nabla \cdot \vec{j}) + \int dV S$$
$$\frac{\partial c}{\partial t} + \nabla \cdot (c \vec{u}) = -\nabla \cdot \vec{j} + S$$
$$\vec{j} = -D \nabla c$$





$$\frac{\partial S}{\partial t} + \nabla \cdot (S \mathbf{u}) = 0$$

$$\frac{\partial S}{\partial t} + \mathbf{u} \cdot \nabla S + S \nabla \cdot \mathbf{u} = 0$$

$$\boxed{\frac{DS}{Dt}} + S \nabla \cdot \mathbf{u} = 0$$

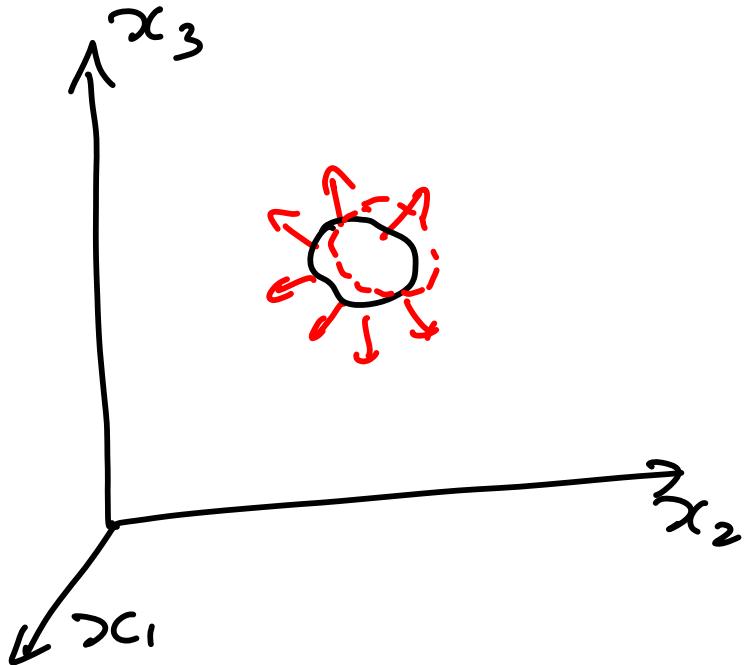
$$\frac{\partial S}{\partial t} + \frac{\partial}{\partial x_i} (S u_i) = 0$$

Incompressible fluid

$$\nabla \cdot \mathbf{u} = 0$$

$$\frac{\partial u_i}{\partial x_i} = 0$$

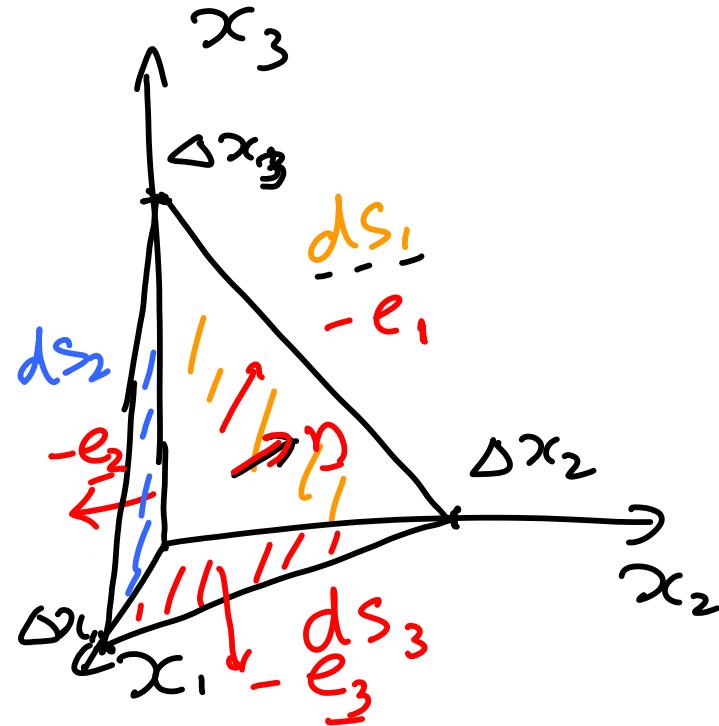
Momentum conservation:



Rate of change of momentum = Sum of applied forces

$$\frac{d}{dt} \int_{V(t)} dV \rho u_i = \int_{V(t)} dV \rho a_i + \int_S dS R_i$$

$$\begin{aligned} \frac{d}{dt} \int_{V(t)} dV \rho u_i &= \int_{V(t)} dV \frac{\partial}{\partial t} (\rho u_i) + \int_S dS (u_j n_j) (\rho u_i) \\ &= \int_{V(t)} dV \frac{\partial}{\partial t} (\rho u_i) + \int_V \frac{\partial}{\partial x_j} (\rho u_i u_j) \end{aligned}$$



$$R_i(\underline{n}) = -R_i(-\underline{n}_i)$$

$$R_i(\underline{n}) = T_{ij} \underline{n}_j$$

Cauchy construction.

Total surface force

$$\begin{aligned} &= dS R_i(\underline{n}) + dS_1 R_i(-\underline{e}_1) + dS_2 R_i(-\underline{e}_2) \\ &\quad + dS_3 R_i(-\underline{e}_3) \end{aligned}$$

Total surface force

$$= dS R_i(\underline{n}) - dS_1 R_i(\underline{e}_1) - dS_2 R_i(\underline{e}_2) - dS_3 R_i(\underline{e}_3) = 0$$

$$\underline{n} = n_1 \underline{e}_1 + n_2 \underline{e}_2 + n_3 \underline{e}_3$$

$$dS_1 = n_1 dS; dS_2 = n_2 dS; dS_3 = n_3 dS$$

Total surface force

$$= dS (R_i(\underline{n}) - n_1 R_i(\underline{e}_1) - n_2 R_i(\underline{e}_2) - n_3 R_i(\underline{e}_3)) = 0$$

$$R_i(\underline{m}) = n_1 R_i(\underline{e}_1) + n_2 R_i(\underline{e}_2) + n_3 R_i(\underline{e}_3)$$

$$= T_{i1} n_1 + T_{i2} n_2 + T_{i3} n_3$$

$$= T_{ij} n_j$$

T_{ij} = Force/Area in i direction acting at
a surface with **outward** unit
normal in j direction

$$\int dS R_i = \int dS T_{ij} n_j = \int dV \left(\frac{\partial}{\partial x_j} T_{ij} \right)$$

$$\frac{d}{dt} \int_{V(t)} dV (\delta u_i) = \int_{V(t)} \delta q_i + \int_{\partial V(t)} ds R_i$$

$$\int_{V(t)} dV \left(\frac{\partial}{\partial t} (\delta u_i) \right) + \int_{\partial V(t)} (n_j \delta u_i u_j) = \int_{V(t)} \delta q_i + \int_{\partial V(t)} T_{ij} n_j$$

$$\int_{V(t)} \frac{\partial}{\partial t} (\delta u_i) + \int_{V(t)} \frac{\partial}{\partial x_j} (\delta u_i u_j) = \int_{V(t)} \delta q_i + \int_{V(t)} \frac{\partial}{\partial x_j} (T_{ij})$$

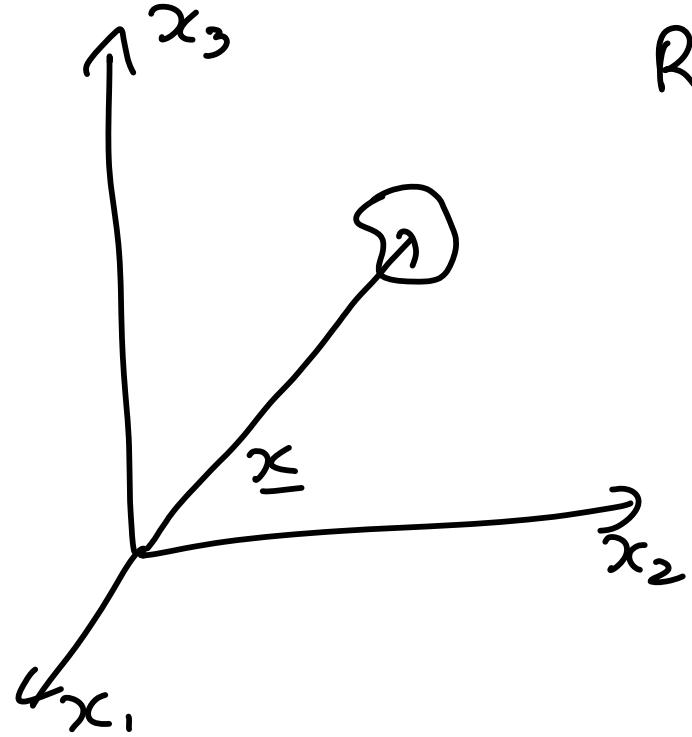
$$\frac{\partial}{\partial t} (\delta u_i) + \frac{\partial}{\partial x_j} (\delta u_i u_j) = \delta q_i + \frac{\partial}{\partial x_j} (T_{ij})$$

$$u_i \left(\frac{\partial S}{\partial t} + \frac{\partial}{\partial x_j} (\delta u_j) \right) + S \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right)$$

$$= \delta q_i + \frac{\partial}{\partial x_j} (T_{ij})$$

$$S \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = Sa_i + \frac{\partial}{\partial x_j} (T_{ij})$$

$$\text{Angular momentum} = \underline{x} \times S \underline{u} = \epsilon_{ijk} x_j S u_k$$



Rate of change
of angular momentum

Sum of applied
torques

$$\frac{d}{dt} \int_V dV (\epsilon_{ijk} x_j \delta u_k) = \int_V dV \epsilon_{ijk} x_j \delta a_k + \int_S dS \epsilon_{ijk} x_j R_k$$

$$= \int_V dV \epsilon_{ijk} x_j \delta a_k + \int_S dS \epsilon_{ijk} x_j \bar{T}_{kc} n_c$$

$$\int_V dV \frac{\partial}{\partial t} (\epsilon_{ijk} x_j \delta u_k) + \int_S dS (u_c n_c) (\epsilon_{ijk} x_j \delta u_k)$$

$$= \int_V dV \epsilon_{ijk} x_j \delta a_k + \int_S dS \epsilon_{ijk} x_j \bar{T}_{kc} n_c$$

$$\int_V dV \epsilon_{ijk} x_j \frac{\partial}{\partial t} (\delta u_k) + \int_V dV \frac{\partial}{\partial x_c} (\epsilon_{ijk} x_j \underline{\delta u}_k \underline{u}_c)$$

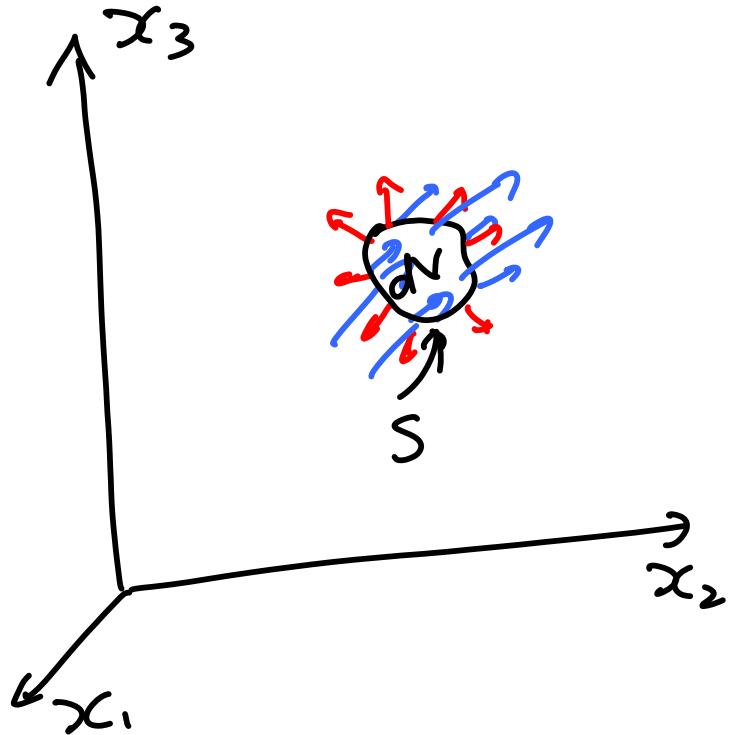
$$= \int_V dV (\epsilon_{ijk} x_j \delta u_k) + \int_V dV \frac{\partial}{\partial x_c} (\epsilon_{ijk} x_j \bar{T}_{kc} n_c)$$

$$\int_V dV \epsilon_{ijk} x_j \frac{\partial}{\partial t} (\delta u_k) + \int_V dV \epsilon_{ijk} \left[x_j \frac{\partial}{\partial x_c} (\delta u_k u_c) + \delta u_k u_c \color{red}{\delta_{jl}} \right]$$

$$= \int_V dV (\epsilon_{ijk} x_j \delta u_k) + \int_V dV \epsilon_{ijk} \left(x_j \frac{\partial}{\partial x_c} T_{kl} + T_{lc} \color{red}{\delta_{jl}} \right)$$

$$\int dV G_{ijkl} x_j \left[\frac{\partial}{\partial t} (\delta u_k) + \frac{\partial}{\partial x_i} (\delta u_k u_i) \right] + \int dV \epsilon_{ijkl} x_j \delta u_k u_j \\ = \int dV \epsilon_{ijkl} x_j \delta u_k + \int dV \left[\epsilon_{ijk} x_j \frac{\partial}{\partial x_i} (\bar{T}_{kj}) + \epsilon_{ijk} \bar{T}_{kj} \right]$$

Mass conservation:



$$\frac{d}{dt} \int_{V(t)} dV \rho = 0$$

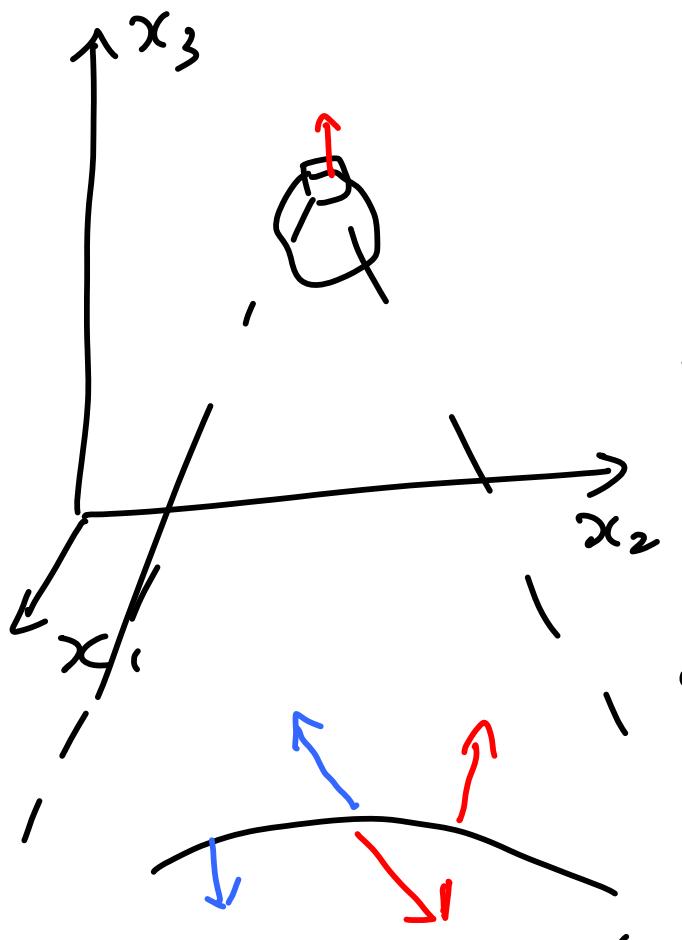
$$\int_{\partial V} dS \frac{\partial \rho}{\partial t} + \int_{\partial V} dS \rho \underline{u} \cdot \underline{n} = 0$$

$$\int_{\partial V} \left[\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{u}) \right] dS = 0$$

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{u}) = 0$$

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_i} (\rho u_i) = 0$$

Momentum conservation:



$$\frac{d}{dt} \int_{\Gamma(t)} dV (\delta u_i) = \int_V \delta a_i + \int_S R_i$$

$$\int dV \frac{\partial}{\partial t} (\delta u_i) + \int dS (\delta u_i) (u_j n_j) = \int_V \delta a_i + \int_S R_i$$

$$\int dV \frac{\partial}{\partial t} (\delta u_i) + \int dV \frac{\partial}{\partial x_j} (\delta u_i u_j) = \int_V \delta a_i + \int_S R_i$$

$$\int dV \left(\frac{\partial (\delta u_i)}{\partial t} + \frac{\partial}{\partial x_j} (\delta u_i u_j) \right) = \int_V \delta a_i + \int_S T_{ij} n_j$$

$$\int dV \frac{\partial}{\partial x_j} (T_{ij})$$

$$R_i(\nu) = -R_i(-\nu) = T_{ij} n_j$$

Momentum conservation eqn:

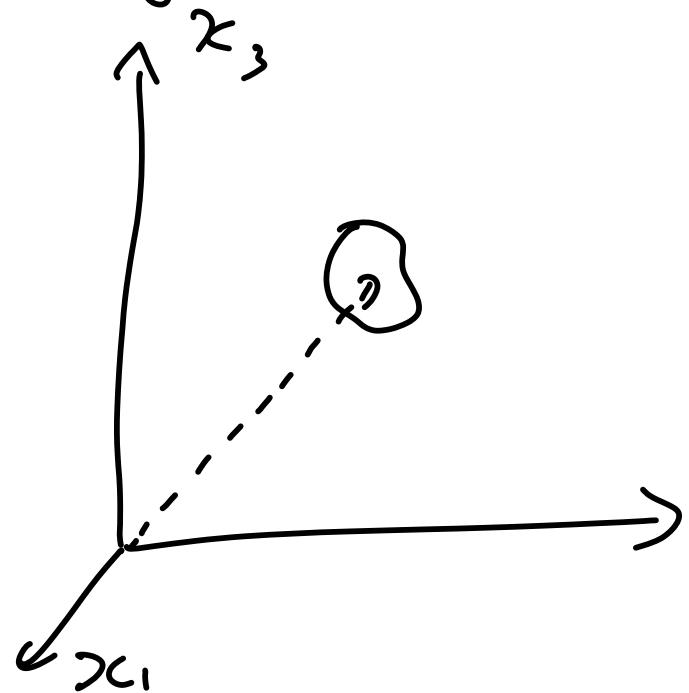
$$\frac{\partial}{\partial t} (\bar{S} u_i) + \frac{\partial}{\partial x_j} (\bar{S} u_i u_j) = \bar{S} a_i + \frac{\partial}{\partial x_j} \bar{T}_{ij}$$

$$\bar{S} \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = \bar{S} a_i + \frac{\partial}{\partial x_j} \bar{T}_{ij}$$

Angular momentum conservation:

$$L = \int dV \underline{\underline{\underline{x}}} \times (\underline{S} \underline{U}) = \int_{V(t)} dV \epsilon_{ijk} x_j S_{ik}$$

$$L_i = \epsilon_{ijk} \int dV x_j S_{ik}$$



$$\frac{d}{dt} \int dV \epsilon_{ijk} x_j S_{ik} = \int dV \epsilon_{ijk} x_j S_{ik} + \int dS \epsilon_{ijk} x_j T_{kc} n_c$$

$$\int dV \epsilon_{ijk} \frac{\partial}{\partial t} (x_j S_{ik}) + \int dS \epsilon_{ijk} x_j S_{ik} n_c \\ = \int dV \epsilon_{ijk} x_j S_{ik} + \int dV \frac{\partial}{\partial x_c} (\epsilon_{ijk} x_j T_{kc})$$

$$\int dV \epsilon_{ijk} x_j \frac{\partial}{\partial t} (S_{ik}) + \int dV \frac{\partial}{\partial x_c} (\underline{\underline{\underline{x}}}_j \underline{\underline{S}}_{ik} \underline{\underline{U}}_c) \\ = \int dV \epsilon_{ijk} x_j S_{ik} + \int dV \epsilon_{ijk} \frac{\partial}{\partial x_c} (\underline{\underline{\underline{x}}}_j \underline{\underline{T}}_{kc})$$

$$\int dV \epsilon_{ijk} x_j \left[\frac{\partial}{\partial t} (8u_k) \right] + \int dV \epsilon_{ijk} \left[x_j \frac{\partial}{\partial x_i} (8u_k u_i) + 8u_k u_j \right]$$

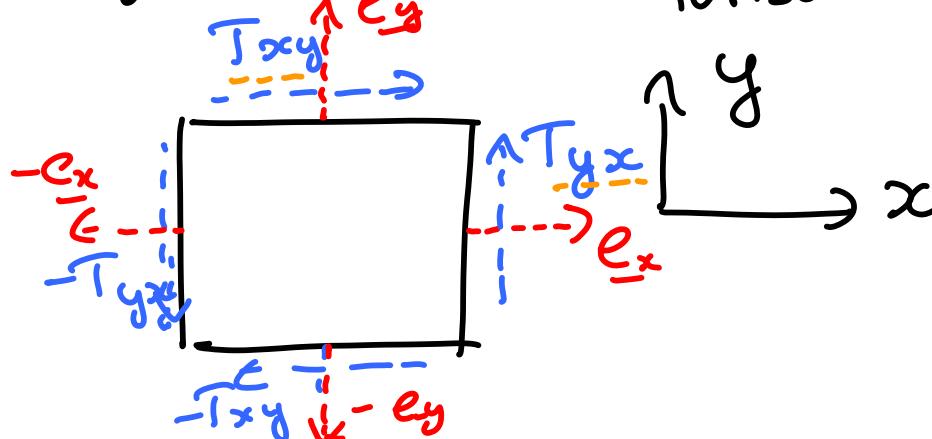
$$= \int dV \epsilon_{ijk} x_j (8a_k) + \int dV \epsilon_{ijk} \left[x_j \frac{\partial}{\partial x_i} T_{kj} + T_{kj} \right]$$

$$\epsilon_{ijk} x_j \left[\frac{\partial}{\partial t} (8u_k) + \frac{\partial}{\partial x_i} (8u_k u_i) \right] + \epsilon_{ijk} S a_k u_j$$

$$= \epsilon_{ijk} x_j S a_k + \epsilon_{ijk} x_j \frac{\partial}{\partial x_i} T_{kj} + \epsilon_{ijk} T_{kj}$$

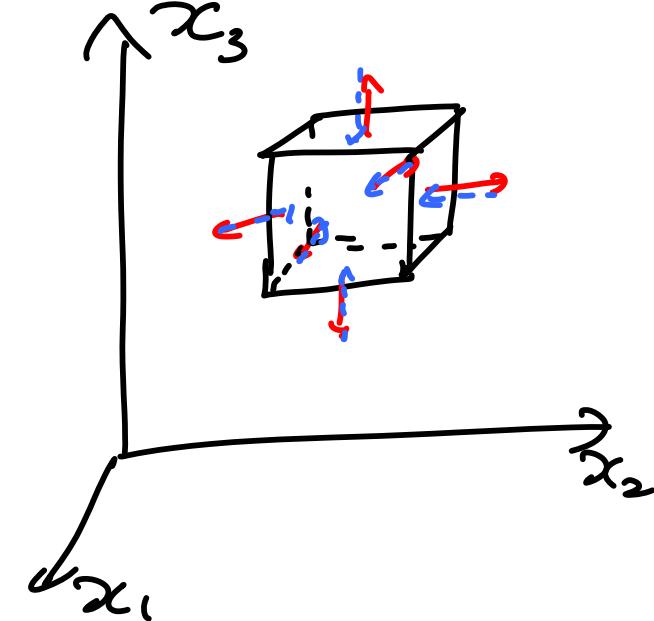
$$\epsilon_{ijk} T_{kj} = 0$$

$T_{ij} = T_{ji} \Rightarrow$ Symmetric tensor



Stress tensor:

$$\underline{\underline{T}} = \begin{pmatrix} T_{11} & T_{12} & T_{13} \\ T_{21} & T_{22} & T_{23} \\ T_{31} & T_{32} & T_{33} \end{pmatrix}$$



$$= \begin{pmatrix} \frac{T_{11} + T_{22} + T_{33}}{3} & 0 & 0 \\ 0 & \frac{T_{11} + T_{22} + T_{33}}{3} & 0 \\ 0 & 0 & \frac{T_{11} + T_{22} + T_{33}}{3} \end{pmatrix} + \underline{\underline{T}}$$

$$T_{ij} = \underline{\underline{T}_{ij}} + \delta_{ij} (-p) ; T_{ii} = 0$$

$$T_{ij} = -p \delta_{ij} + T_{ij} + \mu_b \delta_{ij} \left(\frac{\partial u_k}{\partial x_k} \right)$$

$$\frac{\partial u_i}{\partial x_j} = A_{ij} + E_{ij} + \frac{1}{2} \delta_{ij} \left(\frac{\partial u_k}{\partial x_k} \right)$$

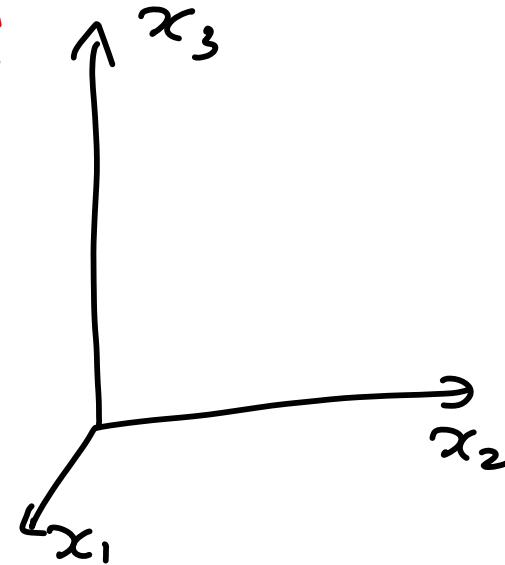
Additional postulate:

Stress tensor is linear function
of rate of deformation tensor

$$T_{ij} = 2 \mu E_{ij}$$
 Newton's law

μ = Coefficient of viscosity

$$\tau_{xy} = \mu \frac{\partial u_x}{\partial y}$$



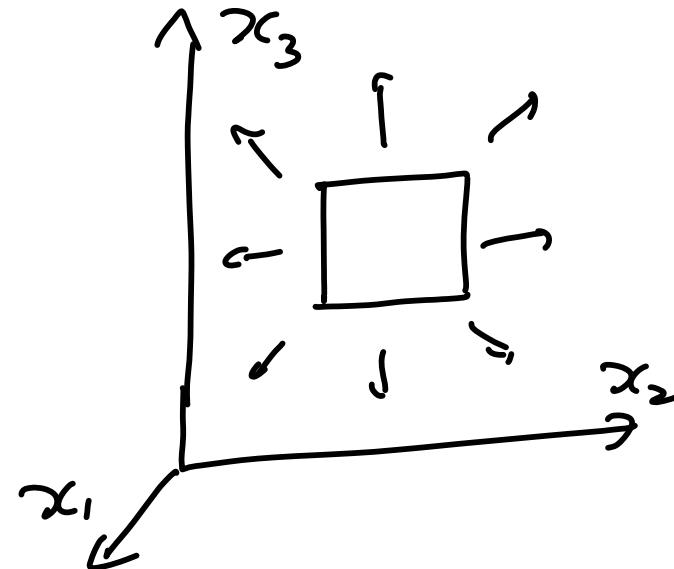
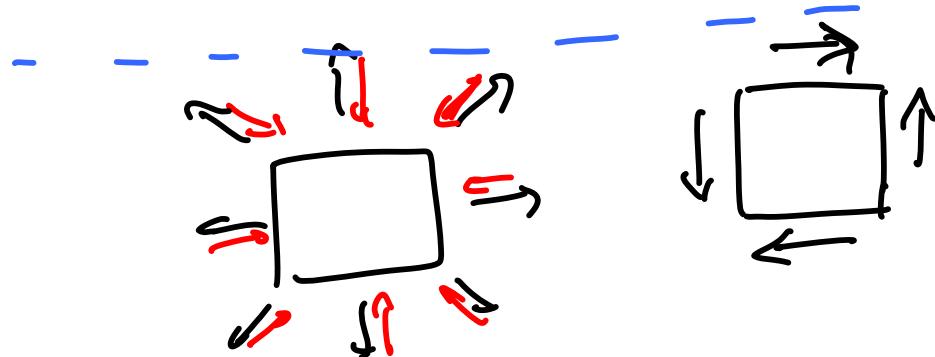
$$\frac{\partial S}{\partial t} + \frac{\partial}{\partial x_j} (S u_j) = 0$$

$$S \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = S a_i + \frac{\partial}{\partial x_j} \left(-\rho \delta_{ij} + 2\mu E_{ij} + \lambda_b \delta_{ij} \frac{\partial u_k}{\partial x_k} \right)$$

$$S \frac{D u_i}{D t} = S a_i - \frac{\partial p}{\partial x_i} + \frac{\partial}{\partial x_j} \left(2\mu E_{ij} \right) + \frac{\partial}{\partial x_i} \left(\lambda_b \frac{\partial u_k}{\partial x_k} \right)$$

Stress Tensor:

$$\bar{\tau}_{ij} = -p \delta_{ij} + \bar{\tau}_{kk}$$



$$\bar{\tau}_{ij} = -p \delta_{ij} + \bar{\tau}_{ij}$$

$$\frac{\partial u_i}{\partial x_j} = A_{ij} + E_{ij} + \frac{1}{3} \delta_{ij} \left(\frac{\partial u_k}{\partial x_k} \right)$$

$$A_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} - \frac{\partial u_j}{\partial x_i} \right); E_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) - \frac{1}{3} \delta_{ij} \frac{\partial u_k}{\partial x_k}$$

$$\underline{\underline{T}}_{ij} = \underline{\underline{2\mu E}}_{ij}$$

$$T_{ij} = -p \delta_{ij} + 2\mu E_{ij} + \mu_b \left(\frac{\partial u_k}{\partial x_k} \right) \delta_{ij}$$

Newtonian fluid

$$= -p \delta_{ij} + 2\mu \left[\frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) - \frac{1}{3} \delta_{ij} \frac{\partial u_k}{\partial x_k} \right] + \mu_b \left(\frac{\partial u_k}{\partial x_k} \right) \delta_{ij}$$

$$= -p \delta_{ij} + \underline{\underline{\mu}} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) + \underline{\underline{\left(\mu_b - \frac{2}{3}\mu \right) \delta_{ij} \left(\frac{\partial u_k}{\partial x_k} \right)}}$$

$$T_{ij} = \underline{\underline{\mu^{(g)}}} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) - p \delta_{ij}$$

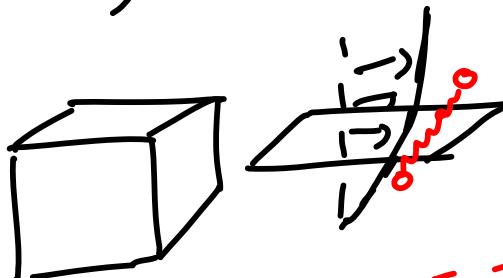
$$\underline{\underline{\mu^{(g)}}} = \text{fn. (rate of deformation tensor)}$$

$$\underline{\underline{E}} = \begin{pmatrix} E_{11} & E_{12} & E_{13} \\ E_{21} & E_{22} & E_{23} \\ E_{31} & E_{32} & E_{33} \end{pmatrix}$$

$$\underline{\underline{I}}_1 = \text{Trace}(\underline{\underline{E}}); \quad \underline{\underline{I}}_2 = \underline{\underline{E}} : \underline{\underline{E}}; \quad \underline{\underline{I}}_3 = \text{Det}(\underline{\underline{E}})$$

$$\mu^{(g)} = \mu^{(g)}(\underline{\underline{I}}_1, \underline{\underline{I}}_2, \underline{\underline{I}}_3)$$

Polymer solution:



$$\underline{\underline{q}} = \underline{\underline{x}} \underline{\underline{x}}$$

$$q_{ij} = x_i x_j$$

$$\underline{\underline{I}}^P = \frac{\eta_p k_n}{T \ln T} \left(\underline{\underline{q}} - \underline{\underline{q}}^{\text{ear}} \right)$$

Mass conservation:

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_j} (\rho u_j) = 0$$

$$\rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = \rho a_i + \frac{\partial}{\partial x_j} (T_{ij})$$

$$\begin{aligned} \frac{\partial}{\partial x_j} (T_{ij}) &= \frac{\partial}{\partial x_j} \left(-p \delta_{ij} + 2\mu E_{ij} + \mu_b \delta_{ij} \frac{\partial u_k}{\partial x_k} \right) \\ &= -\frac{\partial p}{\partial x_i} + 2\mu \frac{\partial}{\partial x_j} \left(\frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) - \frac{1}{3} \delta_{ij} \frac{\partial u_k}{\partial x_k} \right) \\ &\quad + \mu_b \frac{\partial}{\partial x_j} \left(\frac{\partial u_k}{\partial x_k} \right) \delta_{ij} \\ &= -\frac{\partial p}{\partial x_i} + \mu \frac{\partial}{\partial x_j} \left(\frac{\partial u_i}{\partial x_j} \right) + \mu \frac{\partial}{\partial x_j} \left(\frac{\partial u_i}{\partial x_i} \right) \\ &\quad - \frac{2}{3} \mu \frac{\partial}{\partial x_i} \left(\frac{\partial u_k}{\partial x_k} \right) + \mu_b \frac{\partial}{\partial x_i} \left(\frac{\partial u_k}{\partial x_k} \right) \end{aligned}$$

$$\frac{\partial T_{ij}}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} + \left(\mu_b + \frac{1}{3} \mu \right) \frac{\partial}{\partial x_i} \left(\frac{\partial u_k}{\partial x_k} \right)$$

$$\rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = - \frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} + \left(\mu_b + \frac{1}{3} \mu \right) \frac{\partial}{\partial x_i} \left(\frac{\partial u_k}{\partial x_k} \right)$$

$$\rho \left(\frac{\partial u}{\partial t} + u \cdot \nabla u \right) = - \nabla p + \mu \nabla^2 u + \left(\mu_b + \frac{1}{3} \mu \right) \nabla (\nabla \cdot u)$$

$$\frac{\partial S}{\partial t} + \frac{\partial}{\partial x_i} (S u_i) = 0 \quad \frac{\partial S}{\partial t} + u_i \frac{\partial S}{\partial x_i} + S \frac{\partial u_i}{\partial x_i} = 0$$

Equation of state

$$p = n k T = \frac{S}{m} k T$$

Incompressible: $S = \text{constant}$

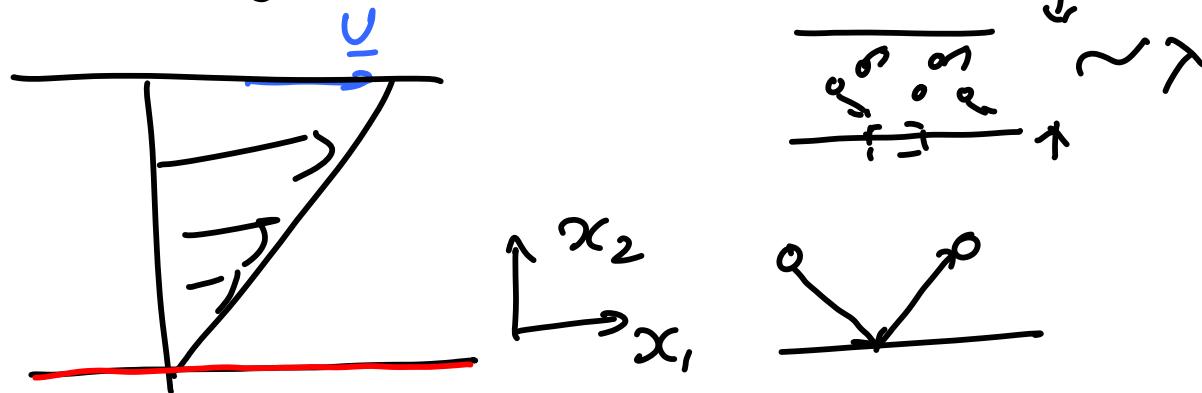
$$\nabla \cdot u = 0 \quad \text{Mass conservation}$$

$$\left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = - \frac{1}{S} \frac{\partial p}{\partial x_i} + \left(\frac{\mu}{S} \frac{\partial^2 u_i}{\partial x_j^2} \right)$$

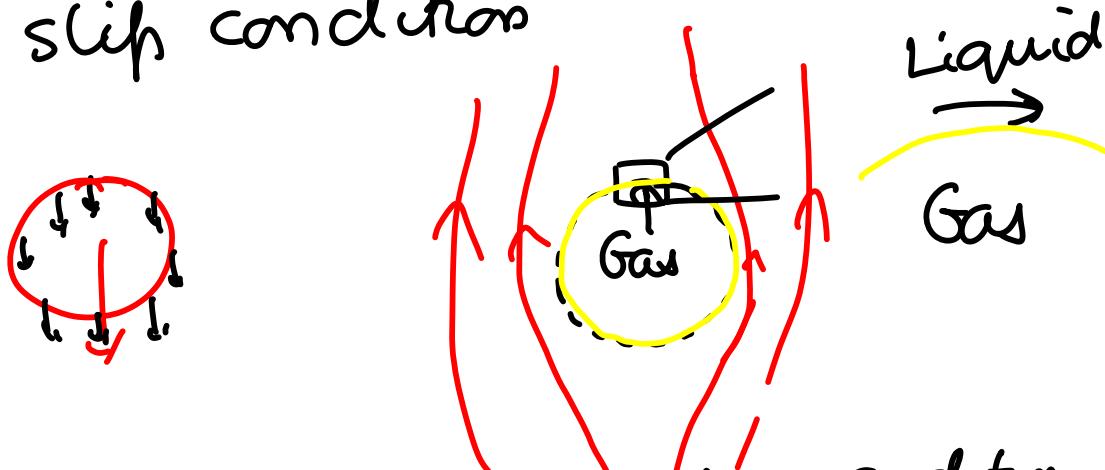
|| Navier
Stokes
eqns.

$$\frac{\partial c}{\partial t} + \nabla \cdot (u c) = D \nabla^2 c$$

Boundary conditions:



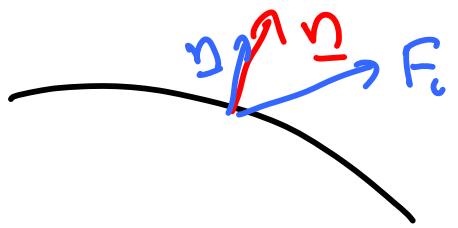
'No-slip condition'



Zero tangential stress boundary condition

$$(\text{Normal stress outside}) - (\text{Normal stress inside}) = \gamma \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$$

$$F_i = T_{ij} n_j$$



$$n_i F_i = n_i \bar{T}_{ij} n_j$$

$$n_i \bar{T}_{ij} n_j - n_i \bar{T}_{ij} n_j \Big|_{\text{gas}} = \gamma \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$$

liquido

$$\begin{array}{c} n_i F_i \\ \nearrow \\ F_i \\ \searrow \\ (\delta_{ij} - n_i n_j) F_j \end{array}$$

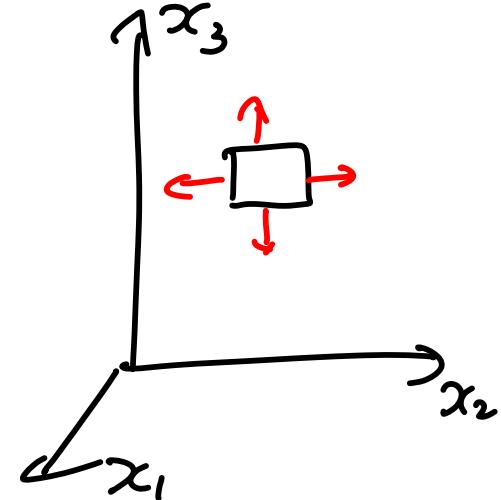
$$(\delta_{ij} - n_i n_j) F_j = (\delta_{ij} - n_i n_j) \bar{T}_{ik} n_k = 0$$

$$n_i (\delta_{ij} - n_i n_j) = n_i - n_i n_j^2$$

Mass conservation eqn:

$$\frac{\partial S}{\partial t} + \frac{\partial}{\partial x_i} (S u_i) = 0$$

$$\frac{DS}{Dt} + S \frac{\partial u_i}{\partial x_i} = 0 \quad \frac{\partial u_i}{\partial x_i} = \nabla \cdot u = 0$$



$$\frac{\partial (S u_i)}{\partial t} + \frac{\partial}{\partial x_j} (S u_i u_j) = \frac{\partial T_{ij}}{\partial x_j} + S a_i$$

$$T_{ij} = T_{ji} = -p \delta_{ij} + \bar{T}_{ij} + \mu_b S_{ij} \frac{\partial u_k}{\partial x_k}$$

$$\bar{T}_{ij} = 2\mu E_{ij} = 2\mu \left[\frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) - \frac{1}{3} \delta_{ij} \frac{\partial u_k}{\partial x_k} \right]$$

$$\frac{\partial u_i}{\partial x_i} = 0$$

$$\nabla \cdot \underline{u} = 0$$

$$\frac{\partial (\rho u_i)}{\partial t} + \frac{\partial}{\partial x_j} (u_i u_j) = \frac{\partial}{\partial x_j} \left(-\frac{p}{\rho} \delta_{ij} + 2\mu E_{ij} \right) + \rho a_i$$

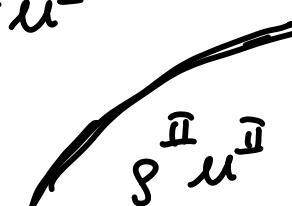
$$\begin{aligned} & \rho \frac{\partial u_i}{\partial t} + \rho u_j \frac{\partial u_i}{\partial x_j} + u_i \left(\frac{\partial p}{\partial t} + \frac{\partial (\rho u_j)}{\partial x_j} \right) \\ &= - \frac{\partial p}{\partial x_i} + 2\mu \frac{\partial}{\partial x_j} \left(\frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right) + \rho a_i \\ &= - \frac{\partial p}{\partial x_i} + \mu \frac{\partial}{\partial x_j} \left(\frac{\partial u_i}{\partial x_j} \right) + \mu \frac{\partial}{\partial x_j} \left(\frac{\partial u_j}{\partial x_i} \right) + \rho a_i \\ &= - \frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} \end{aligned}$$

Navier - Stokes mass & momentum eqns
for an incompressible fluid:

$$\nabla \cdot \underline{u} = 0 \quad \frac{\partial u_i}{\partial x_i} = 0$$

$$\rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = - \frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2}$$

$$\rho \left(\frac{\partial u}{\partial t} + \underline{u} \cdot \nabla \underline{u} \right) = - \nabla p + \mu \nabla^2 \underline{u}$$

$$\rho^2 u^2$$


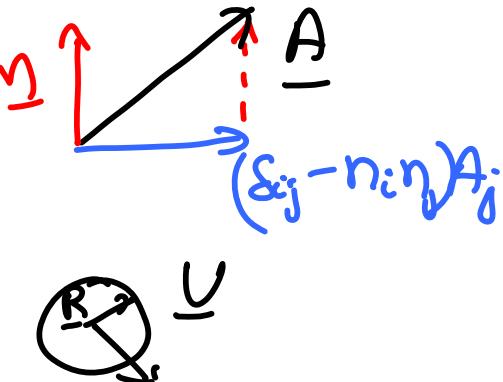
Boundary conditions:

Continuity of velocity
& stress

$$u_i^I n_i = u_i^{\bar{I}} n_i \quad \left| \begin{array}{l} (\delta_{ij} - n_i n_j) u_j^I = (\delta_{ij} - n_i n_j) u_j^{\bar{I}} \\ (\underline{E} - \underline{n} \underline{n}) \cdot \underline{u}^I = (\underline{E} - \underline{n} \underline{n}) \cdot \underline{u}^{\bar{I}} \end{array} \right.$$

$$(\delta_{ij} - n_i n_j) T_{j,k}^I n_k = (\delta_{ij} - n_i n_j) T_{j,k}^{\bar{I}} n_k$$

$$(\delta_{ij} - n_i n_j) T_{j,k}^I n_k = (\delta_{ij} - n_i n_j) T_{j,k}^{\bar{I}} n_k$$



$$n_j T_{j,k}^I n_k = n_j T_{j,k}^{\bar{I}} n_k + \gamma \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$$

Solid-Fluid interface $\bar{y} = \bar{U} + \bar{B} \times \bar{S}$

Gas-Liquid interface: $(\delta_{ij} - n_i n_j) T_{j,k} n_k = 0$

$$n_j T_{j,k}^I n_k - n_j T_{j,k}^{\bar{I}} n_k = \gamma \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$$

$$n_j T_{j,k}^I n_k - (-b^{\bar{I}}) = \gamma \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$$

$$u_i \times S \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = - \frac{\partial p}{\partial x_i} + \frac{\partial}{\partial x_j} T_{ij} + S a_i$$

$$S \left(\frac{\partial}{\partial t} \left(\frac{1}{2} u_i^2 \right) + u_j \frac{\partial}{\partial x_j} \left(\frac{1}{2} u_i^2 \right) \right) = - u_i \frac{\partial p}{\partial x_i} + u_i \frac{\partial}{\partial x_j} (T_{ij}) + S a_i u_i$$

$$\frac{1}{2} u_i^2 \left(\frac{\partial S}{\partial t} + \frac{\partial}{\partial x_j} (S u_j) \right) = 0$$

$$\frac{\partial}{\partial t} \left(\frac{1}{2} S u_i^2 \right) + \frac{\partial}{\partial x_j} \left(\frac{1}{2} S u_i^2 u_j \right) = - \frac{\partial}{\partial x_i} (p u_i) + p \frac{\partial u_i}{\partial x_i} + \frac{\partial}{\partial x_j} (T_{ij} u_i) \\ - T_{ij} \frac{\partial u_i}{\partial x_j} + S a_i u_i$$

$$\frac{\partial}{\partial t} (e_k) + \frac{\partial}{\partial x_j} (u_j e_k) = - \frac{\partial}{\partial x_i} (p u_i) + \frac{\partial}{\partial x_j} (T_{ij} u_i) \\ + p \frac{\partial u_i}{\partial x_i} - T_{ij} \frac{\partial u_i}{\partial x_j} + S a_i u_i$$

$$\frac{D S}{D t} + S \nabla \cdot u = 0 \quad - \frac{p}{S} \frac{D S}{D t}$$

$$D = T_{ij} \frac{\partial u_i}{\partial x_j} = 2\mu E_{ij} \left(\frac{\partial u_i}{\partial x_j} \right)$$

$$\underline{\underline{\dots}} = 2\mu E_{ij} (S_{ij} + A_{ij})$$

$$= 2\mu E_{ij} S_{ij}$$

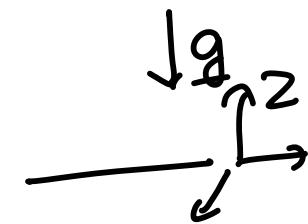
$$= 2\mu \left[S_{ij} - \frac{1}{3} \delta_{ij} \sum_k S_{kk} \right] S_{ij}$$

$$\geq 0$$

Navier- Stokes equations.

$$\nabla \cdot \underline{u} = 0$$

$$3\left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j}\right) = -\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} + g a_i$$



Hydrostatics:

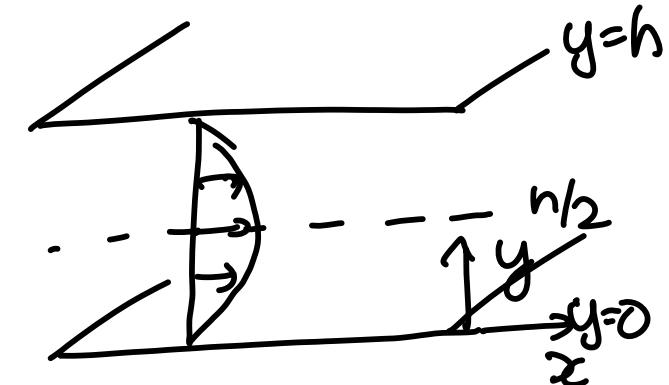
$$-\frac{\partial p}{\partial x_i} + g a_i = 0 \Rightarrow \frac{\partial p}{\partial x_i} = g a_i$$

$$p = p_0 + g a_j x_j \Rightarrow \frac{\partial p}{\partial x_i} = \frac{\partial}{\partial x_i} (g a_j x_j) = g a_j \delta_{ij}$$

$$= p_0 - g g^2$$

Unidirectional flows:

$$\nabla \cdot \underline{u} = 0 \Rightarrow \frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} = 0$$



$$\rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = - \frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2}$$

Independent
of y

$$\rho \left(\frac{\partial u_x}{\partial t} + u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} \right) = - \frac{\partial p}{\partial x} + \mu \left(\frac{\partial^2 u_x}{\partial x^2} + \frac{\partial^2 u_x}{\partial y^2} \right)$$

$$\rho \left(\frac{\partial u_y}{\partial t} + u_x \frac{\partial u_y}{\partial x} + u_y \frac{\partial u_y}{\partial y} \right) = - \frac{\partial p}{\partial y} + \mu \left(\frac{\partial^2 u_y}{\partial x^2} + \frac{\partial^2 u_y}{\partial y^2} \right)$$

$$\frac{\partial u_x}{\partial x} = 0 \quad \circ = - \frac{\partial p}{\partial y}$$

'Fully developed'

$$\left\{ \begin{array}{l} \rho \frac{\partial u_x}{\partial t} = - \frac{\partial p}{\partial x} + \mu \frac{\partial^2 u_x}{\partial y^2} \end{array} \right.$$

Fully developed steady

$$\left. - \frac{\partial p}{\partial x} + \mu \frac{\partial^2 u_x}{\partial y^2} \right) = 0$$

$$U_x = -\frac{h^2}{2u} \frac{\partial f}{\partial x} \left(\frac{y}{h}\right) \left(1 - \frac{y}{h}\right)$$

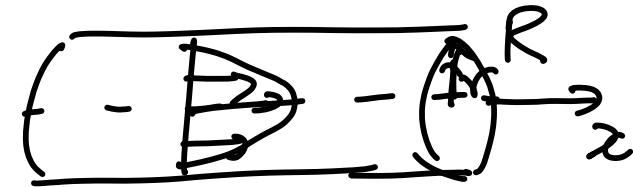
$$U_x^{\max} = -\frac{\partial f}{\partial x} \frac{h^2}{8u}$$

$$U_x = L U_x^{\max} \left(\frac{y}{h}\right) \left(1 - \frac{y}{h}\right)$$

$$U_x^{av} = \frac{2}{3} U_x^{\max}$$

$$f = \left(-\frac{\partial f}{\partial x}\right) \left(\frac{8U_x^{av}}{2h}\right) = \frac{24}{Re}$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_r}{\partial r} \right) + \frac{\partial u_x}{\partial x} = 0 \quad \frac{\partial u_x}{\partial x} = 0$$



Unidirectional \Rightarrow Fully developed

$$\rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = -\frac{\partial p}{\partial x_i} + \mu \nabla^2 u_i$$

$$\rho \left(\frac{\partial u_x}{\partial t} + u_x \frac{\partial u_x}{\partial x} + u_r \frac{\partial u_x}{\partial r} \right) = -\frac{\partial p}{\partial x} + \mu \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_x}{\partial r} \right) \right) + \frac{\partial^2 u_x}{\partial x^2}$$

$$\rho \left(\frac{\partial u_r}{\partial t} + u_r \frac{\partial u_r}{\partial r} + u_x \frac{\partial u_r}{\partial x} \right) = -\frac{\partial p}{\partial r} + \mu \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_r}{\partial r} \right) + \frac{\partial^2 u_r}{\partial x^2} \right)$$

$$-\frac{\partial p}{\partial x} = 0$$

$$\rho \left(\frac{\partial u_x}{\partial t} \right) = -\frac{\partial p}{\partial x} + \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_x}{\partial r} \right) \right]$$

$$0 = -\frac{\partial p}{\partial x} + \mu \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_x}{\partial r} \right) \right)$$

$$U_x = -\frac{R^2}{4\mu} \left(\frac{\partial p}{\partial x} \right) \left(1 - \frac{r^2}{R^2} \right)$$

$$U_x^{\max} = -\frac{R^2}{4\mu} \frac{\partial p}{\partial x}$$

$$U_x^{av} = \frac{U_x^{\max}}{2}$$

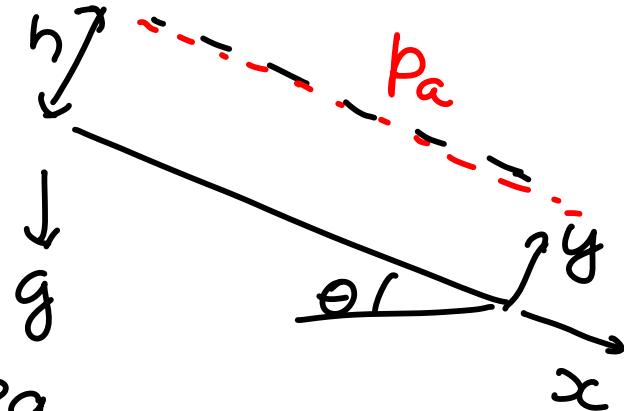
$$f = \left(-\frac{\partial p}{\partial x} \right) / \left(8U_{av}^2 / (2D) \right) = \frac{64}{Re}$$

$$= f \frac{\partial p}{\partial x} / \left(28U_{av}^2 / D \right) = \frac{16}{Re}$$

Flow down inclined plane

$$\frac{\partial u_x}{\partial x} + \cancel{\frac{\partial u_y}{\partial y}} = 0$$

$$\rho \left(\frac{\partial u_x}{\partial t} + u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} \right) = -\frac{\partial p}{\partial x} + \mu \left(\frac{\partial^2 u_x}{\partial x^2} + \frac{\partial^2 u_x}{\partial y^2} \right) + \rho g_x$$



$$\rho \left(\frac{\partial u_y}{\partial t} + u_x \frac{\partial u_y}{\partial x} + u_y \frac{\partial u_y}{\partial y} \right) = -\frac{\partial p}{\partial y} + \mu \left(\frac{\partial^2 u_y}{\partial x^2} + \frac{\partial^2 u_y}{\partial y^2} \right) + \rho g_y$$

$$-\frac{\partial p}{\partial y} + \rho g_y = 0 \Rightarrow p = b_0(x) + \rho g_y y$$

$$b = b_0 + \rho g_y y$$

Normal stress: At $y=h$, $p = p_a \Rightarrow \frac{\partial p_0}{\partial x} = 0$

$$p_0(x) = [p_a - \rho g_y h]$$

$$\delta \frac{\partial u_x}{\partial t} = \mu \frac{\partial^2 u_x}{\partial y^2} + \delta g_x$$

Steady $\mu \frac{\partial^2 u_x}{\partial y^2} + \delta g_x = 0$

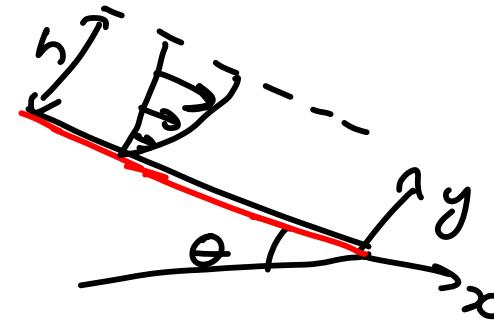
$$u_x = -\frac{\delta g_x}{\mu} \frac{y^2}{2} + C_0 + C_1 y$$

At $y=0$, $u_x = 0$

At $y=h$, $\mu \frac{\partial u_x}{\partial y} = 0$

$$u_x = \left(\frac{\delta g_x h^2}{\mu} \right) \left(\frac{y}{h} - \frac{y^2}{2h^2} \right)$$

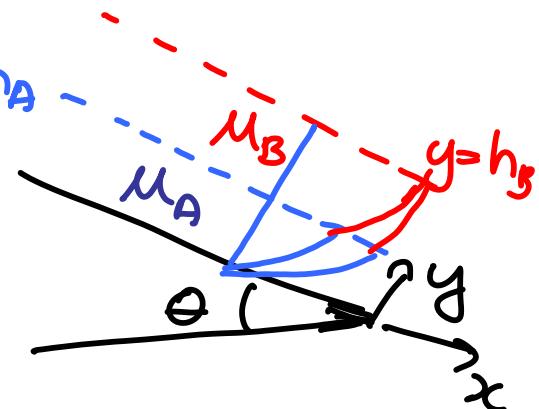
$$u_x^{\max} = \frac{\delta g_x h^2}{2\mu}$$



Flow down inclined plane:

$$M_A \frac{\partial^2 u_x^A}{\partial y^2} = -g g_x \quad u_x^A = \frac{-g g_x y^2 + A_A y + B_A}{2 M_A}$$

$$M_B \frac{\partial^2 u_x^B}{\partial y^2} = -g g_x \quad u_x^B = \frac{-g g_x y^2 + A_B y + B_B}{2 M_B}$$



$$\text{At } y=0, u_x^A = 0 \implies B_A = 0$$

$$\text{At } y=h_B, M_B \frac{\partial u_x^B}{\partial y} = 0 \implies -\frac{g g_x h_B + A_B}{M_B} = 0$$

$$\text{At } y=h_A, M_A \left(\frac{\partial u_x^A}{\partial y} \right) = M_B \left(\frac{\partial u_x^B}{\partial y} \right)$$

$$\therefore u_x^A = u_x^B$$

$$A_A = g g_x \left(h_A \left(\frac{1}{M_A} - \frac{1}{M_B} \right) + \frac{h_B}{M_B} \right)$$

$$B_B = \frac{g g_x h_A^2}{2} \left(\frac{1}{M_A} - \frac{1}{M_B} \right)$$

$$\frac{\partial u_i}{\partial x_i} = 0$$



$$\overline{D \not\rightarrow U}$$

$$g \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = - \frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2}$$

$$Re = \frac{\text{Inertia}}{\text{Viscosity}} = \frac{gUL}{\mu} = \frac{UL}{N}$$

Characteristic length L $x_i^* = x_i/L$
 Characteristic velocity U $u_i^* = u_i/U$

$$t^* = \left(\frac{tU}{L} \right)$$

$$p^* = \left(\frac{p(\mu UL)}{\rho U^2} \right)$$

$$p^{**} = \left(\frac{p}{\rho g U^2} \right)$$

$$\frac{U}{L} \frac{\partial u_i^*}{\partial x_i^*} = 0 \quad \frac{\partial u_i^*}{\partial x_i^*} = 0$$

$$\frac{gU^2}{L} \left(\frac{\partial u_i^*}{\partial t^*} + u_j^* \frac{\partial u_i^*}{\partial x_j^*} \right) = - \frac{1}{L} \frac{\partial p^*}{\partial x_i^*} + \frac{\mu}{L^2} \frac{\partial^2 u_i^*}{\partial x_j^*}$$

$$Re \left(\frac{gUL}{\mu} \right) \left(\frac{\partial u_i^*}{\partial t^*} + u_j^* \frac{\partial u_i^*}{\partial x_j^*} \right) = - \frac{\partial p^*}{\partial x_i^*} + \frac{\partial^2 u_i^*}{\partial x_j^*} //$$

$$\frac{\partial u_i^*}{\partial t^*} + u_j^* \frac{\partial u_i^*}{\partial x_j^*} = - \frac{\partial p^{**}}{\partial x_i^*} + \frac{1}{Re} \frac{\partial^2 u_i^*}{\partial x_j^*} //$$

① Low Reynolds number:

Neglect inertia

$$0 = - \frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 \bar{u}_i}{\partial x_j^2}$$

$$\frac{\partial \bar{u}_i}{\partial x_i} = 0$$

② High Reynolds number Potential flow

$$\delta \left(\frac{\partial \bar{u}_i}{\partial t} + u_j \frac{\partial \bar{u}_i}{\partial x_j} \right) = - \frac{\partial p}{\partial x_i}$$

$$\frac{\partial \bar{u}_i}{\partial x_i} = 0$$

③ Boundary layer theory.

Navier-Stokes equations:

$$\nabla \cdot \mathbf{u} = 0 \quad \frac{\partial u_i}{\partial x_i} = 0$$

$$\rho \left(\frac{\partial u_i}{\partial t} + \underbrace{\left[u_j \frac{\partial u_i}{\partial x_j} \right]}_{\text{viscous term}} \right) = - \frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2}$$

$$u_i^* = (u_i / U); \quad x_i^* = (x_i / L); \quad t^* = t / (U/L)$$

$$\text{Re} \left(\frac{\partial u_i^*}{\partial t^*} + u_j^* \frac{\partial u_i^*}{\partial x_j^*} \right) = - \frac{\partial p^*}{\partial x_i^*} + \frac{\partial^2 u_i^*}{\partial x_j^* \partial x_j^*}$$

$$p^* = P / (\mu U L); \quad \text{Re} = \frac{\rho U L}{\mu} = \frac{UL}{\nu}$$

Small Reynolds number $\text{Re} \ll 1$

Stokes equations:

$$\underline{\nabla} \cdot \underline{u} = 0 \quad \frac{\partial u_i}{\partial x_i} = 0$$

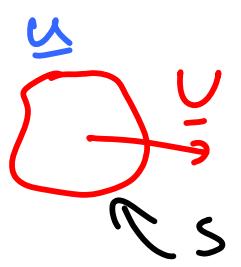
$$-\nabla p + \mu \nabla^2 \underline{u} = 0 \quad -\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j \partial x_i} = 0$$

$$T_{ij} = -p \delta_{ij} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

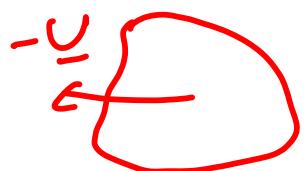
Linear Quasi-steady.

$$D \nabla^2 C = 0$$

$$\alpha \nabla^2 T = 0$$



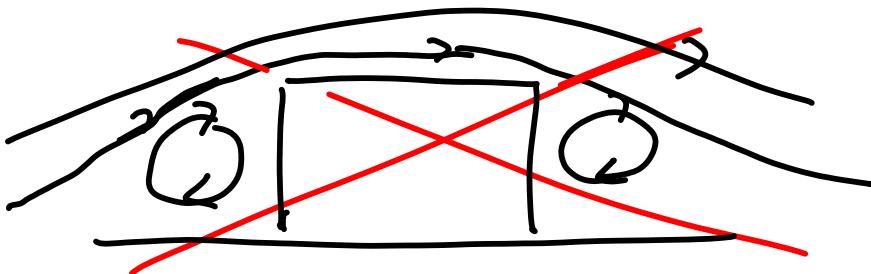
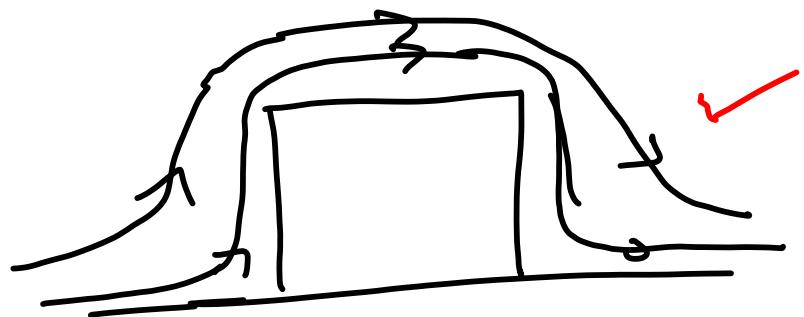
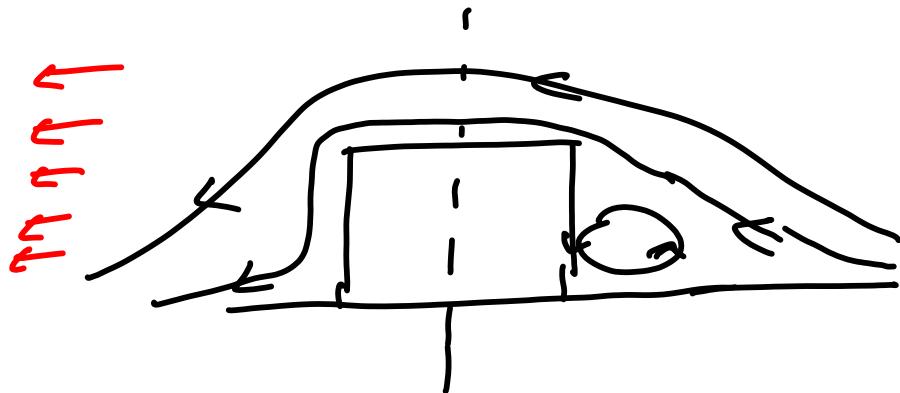
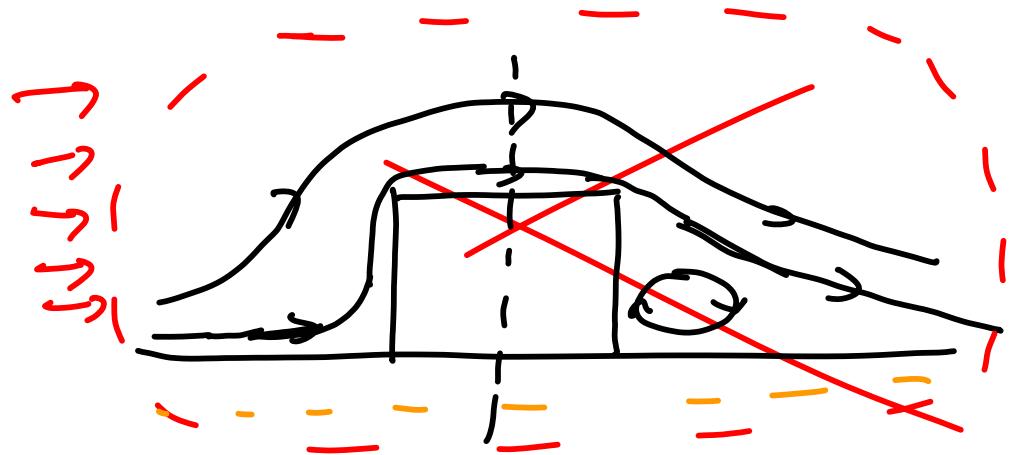
$$\begin{aligned} & [\nabla \cdot \underline{u} = 0] \\ & [-\nabla p + \mu \nabla^2 \underline{u} = 0] \\ & \underline{u} = \underline{v} \text{ on the surface } S \end{aligned}$$

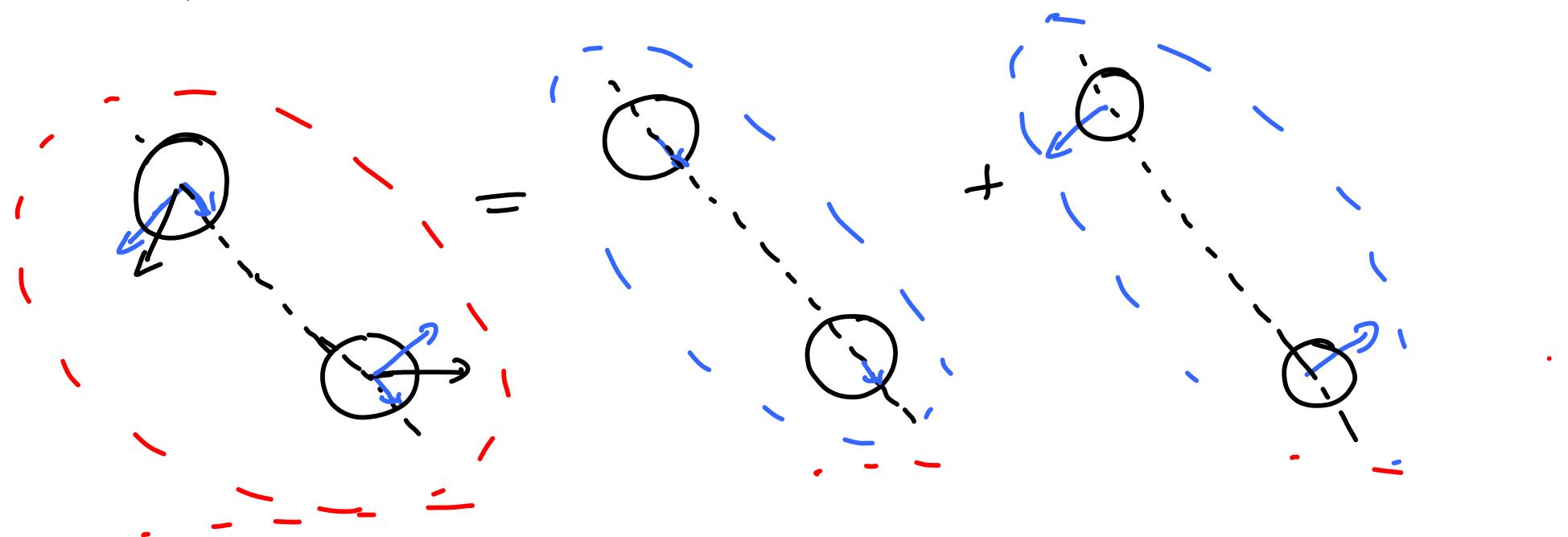
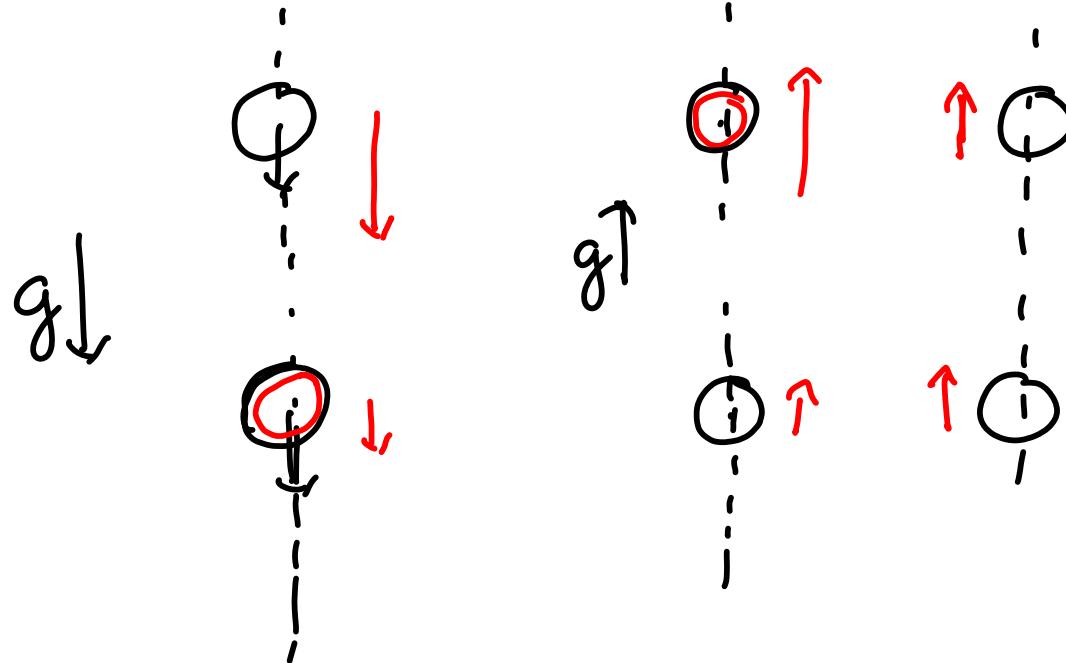


$$\begin{aligned} & \nabla \cdot \underline{u}' = 0 \\ & -\nabla p' + \mu \nabla^2 \underline{u}' = 0 \end{aligned}$$

$$\underline{u}' = -\underline{v} \text{ on the surface } S$$

$$\begin{aligned} \underline{u}' &= -\underline{u} \\ p' &= -p \quad \alpha = -1 \end{aligned}$$





Linearity \Rightarrow Superposition

$$\nabla \cdot u = 0$$

$$\frac{\partial u_i}{\partial x_i} = 0$$

$$-\nabla p + \mu \nabla^2 u = 0$$
$$\frac{\partial}{\partial x_i} \left[-\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} \right] = 0$$
$$\boxed{\nabla^2 u = 0}$$

$$-\frac{\partial^2 p}{\partial x_i^2} + \mu \frac{\partial}{\partial x_i} \left(\frac{\partial^2 u_i}{\partial x_j^2} \right) = 0$$

$$-\frac{\partial p}{\partial x_i^2} + \mu \frac{\partial^2}{\partial x_j^2} \left(\frac{\partial u_i}{\partial x_i} \right) = 0$$

$$\frac{\partial^2 p}{\partial x_i^2} = 0 \Rightarrow \boxed{\nabla^2 p = 0}$$

$$-\nabla p + \mu \nabla^2 u = 0$$
$$\frac{\partial u_i}{\partial x_j} = C \frac{\partial p}{\partial x_j}$$
$$\frac{\partial}{\partial x_j} \left[x_i \frac{\partial p}{\partial x_j} + p \delta_{ij} \right] = 0$$
$$\nabla^2 u_i = 0$$
$$-\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} = 0$$
$$\frac{\partial}{\partial x_j} \left[x_i \frac{\partial^2 p}{\partial x_j^2} + \frac{2 \partial p \delta_{ij}}{\partial x_j} \right] = 0$$

$$\frac{\partial}{\partial x_j} \left[\frac{\partial u_i}{\partial x_j} \right] = 2c \frac{\partial^2 f}{\partial x_i^2} = \frac{1}{u} \frac{\partial^2 f}{\partial x_i^2}$$

$$u_i = \frac{1}{2u} p x_i \quad u_i = u_i^{8+1} \frac{p x_i}{2u}$$

Low Reynolds number viscous flows:

$$\nabla \cdot \underline{u} = 0$$

$$\frac{\partial u_i}{\partial x_i} = 0$$

$$-\nabla p + \mu \nabla^2 \underline{u} = 0$$

$$-\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} = 0$$

$$\underline{T} = -\nabla p + \mu (\nabla \underline{u} + \nabla \underline{u}^\top) \quad T_{ij} = -p \delta_{ij} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

'Quasi-steady' 'Linear'

$$\frac{\partial}{\partial x_i} \left[-\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} \right] = 0$$

$$\frac{\partial^2 p}{\partial x_i^2} = 0 \quad \text{or} \quad \boxed{\nabla^2 p = 0}$$

$$-\nabla p + \mu \nabla^2 \underline{u} = 0$$

$$\boxed{\mu \nabla^2 \underline{u}^p = 0} \quad \leftarrow \quad -\nabla p + \mu \nabla^2 \underline{u}^p = 0$$
$$u_i^p = \frac{1}{2\mu} p x_i$$

$$u_i = u_i^{(g)} + \frac{1}{2\mu} \rho x_i$$

$$\nabla^2 T = 0$$

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} = 0$$

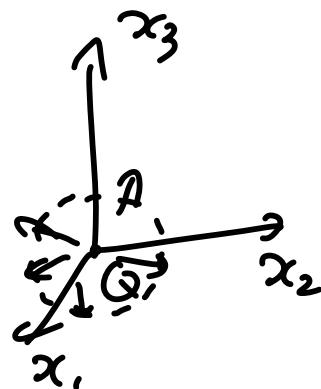
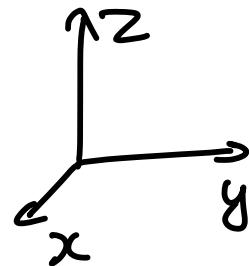
$$T = X(x) Y(y) Z(z)$$

Point source:

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) = 0$$

$$T = \frac{C_1}{r} + C_2 = \frac{Q}{4\pi k r} + T_\infty$$

$$Q = \int ds q_r = \int ds \left(-k \frac{\partial T}{\partial r} \right)$$

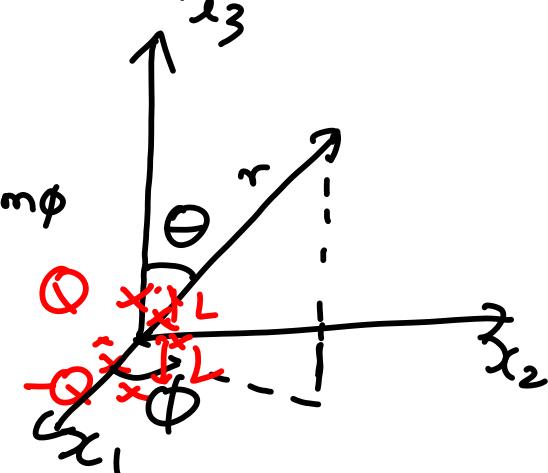


$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} = 0$$

$$T = R(r) F(\theta) H(\phi)$$

$$= \sum_{n=0}^{\infty} \sum_{m=-n}^{n} \left[\frac{A_{nm}}{r^{n+1}} + B_{nm} r^n \right] P_n^m(\cos \theta) e^{im\phi}$$

$P_n^m(\cos \theta) \Rightarrow$ Legendre polynomials

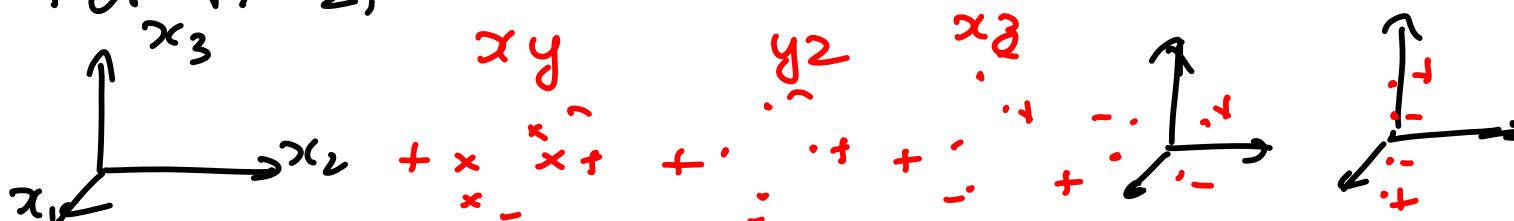


$$\text{For } n=0 \Rightarrow T = \frac{A}{r} + B$$

$$\text{For } n=1 \ m=0 \Rightarrow T = \frac{A_{10}}{r^2} \cos \theta + B_{10} r \cos \theta$$

In the Limit $L \rightarrow 0$ & QL \rightarrow Finite

For $n=2, m=-2, -1, 0, +1, +2$



$$\nabla^2 \underline{\hat{\Phi}}^{(0)} = 0$$

$$\underline{\hat{\Phi}}^{(0)} \leq \frac{C}{r}$$

Fundamental solution

$$\nabla(\nabla^2 \underline{\hat{\Phi}}^{(0)}) = 0$$

$$\nabla^2(\nabla \underline{\hat{\Phi}}^{(0)}) = 0$$

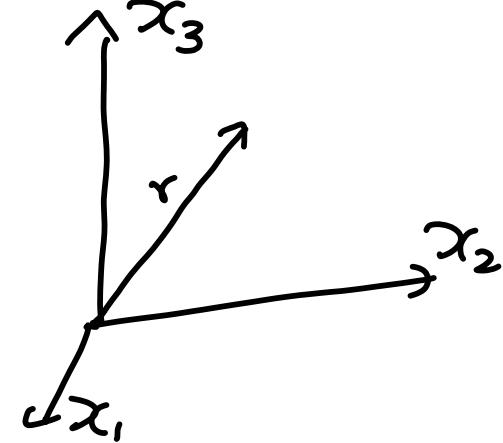
$$\nabla^2(\underline{\hat{\Phi}}^{(0)}) = 0 \quad \underline{\hat{\Phi}}_i^{(0)} = \text{Vector solution of Laplace equation}$$

$$\nabla^2(\underline{\hat{\Phi}}_i^{(0)}) = 0$$

$$r = \sqrt{x_1^2 + x_2^2 + x_3^2}$$

$$\underline{\hat{\Phi}}^{(0)} = \frac{C}{r} = \frac{C}{\sqrt{x_1^2 + x_2^2 + x_3^2}}$$

$$\nabla(\underline{\hat{\Phi}}^{(0)}) = \left(e_1 \frac{\partial}{\partial x_1} + e_2 \frac{\partial}{\partial x_2} + e_3 \frac{\partial}{\partial x_3} \right) \left(\frac{C}{r} \right)$$



$$\nabla r = \left(\frac{e_1}{\partial x_1} \frac{\partial}{\partial x_1} + \frac{e_2}{\partial x_2} \frac{\partial}{\partial x_2} + \frac{e_3}{\partial x_3} \frac{\partial}{\partial x_3} \right) \left(\sqrt{x_1^2 + x_2^2 + x_3^2} \right)$$

$$= \frac{e_1 x_1}{\sqrt{x_1^2 + x_2^2 + x_3^2}} + \frac{e_2 x_2}{\sqrt{x_1^2 + x_2^2 + x_3^2}} + \frac{e_3 x_3}{\sqrt{x_1^2 + x_2^2 + x_3^2}}$$

$$\frac{\partial r}{\partial x_i} = \sum_{i=1}^3 \frac{e_i x_i}{r} = \frac{x_i}{r}$$

$$\frac{\partial}{\partial x_i} (\Phi^{(0)}) = \frac{\partial}{\partial x_i} \left(\frac{c}{r} \right) = -\frac{c}{r^2} \frac{\partial r}{\partial x_i} = -\frac{c x_i}{r^3}$$

$$\hat{\Phi}_i^{(1)} = -\frac{c x_i}{r^3}$$

$$\nabla^2 \hat{\Phi}_i^{(1)} = 0 \Rightarrow \frac{\partial}{\partial x_j} \left(\nabla^2 \hat{\Phi}_i^{(1)} \right) = 0$$

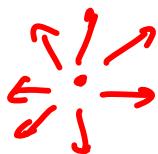
$$\nabla^2 \left(\frac{\partial}{\partial x_j} \hat{\Phi}_i^{(1)} \right) = 0 \Rightarrow \nabla^2 \left(\hat{\Phi}_{ij}^{(2)} \right) = 0$$

$$\begin{aligned}
 \bar{\Phi}_{ij}^{(2)} &= \frac{\partial}{\partial x_j} \left(-\frac{c x_i}{r^3} \right) = -\frac{c}{r^3} \frac{\partial x_i}{\partial x_j} - c x_i \frac{\partial}{\partial x_j} \left(\frac{1}{r^3} \right) \\
 &= -\frac{c \delta_{ij}}{r^3} - c x_i \left[-\frac{3}{r^4} \right] \left[\frac{\partial r}{\partial x_j} \right] \\
 &= -\frac{c \delta_{ij}}{r^3} + \frac{3 c x_i x_j}{r^5} \\
 &= c \left[-\frac{\delta_{ij}}{r^3} + \frac{3 x_i x_j}{r^5} \right]
 \end{aligned}$$

$$\bar{\Phi}_{ijk}^{(3)} = \frac{\partial}{\partial x_k} \left(\bar{\Phi}_{ij}^{(2)} \right) = c \left[-\frac{3 \delta_{ij} x_k}{r^5} - \frac{3 \delta_{ik} x_j}{r^5} - \frac{3 \delta_{jk} x_i}{r^5} \right. \\
 \left. + \frac{15 x_i x_j x_k}{r^7} \right]$$

Physical interpretation:

$$\underline{\Phi}^{(0)} = \frac{1}{r}$$



$$T = \sum \frac{A_{nm}}{r^{n+1}} P_n^m(\cos\theta) e^{im\phi}$$

$$n=0; m=0$$

$$\underline{\Phi}^{(1)} = - \frac{x_i}{r^3} \underline{e}_i$$

$$= - \frac{x_1}{r^3} \underline{e}_1 - \frac{x_2}{r^3} \underline{e}_2 - \frac{x_3}{r^3} \underline{e}_3$$

$$+ \begin{cases} n=1 \\ m=0 \end{cases} \frac{A_{10} \cos\theta}{r^2}$$

$$= - \frac{rs \sin\theta \cos\phi}{r^3} \underline{e}_1 - \frac{rs \sin\theta \sin\phi}{r^3} \underline{e}_2 - \frac{rc \sin\theta}{r^3} \underline{e}_3$$

$$+ \begin{cases} n=1 \\ m=1 \end{cases} \frac{A_{11} \sin\theta \cos\phi}{r^2}$$

$$+ \begin{cases} n=1 \\ m=-1 \end{cases} \frac{A_{1-1} \sin\theta \sin\phi}{r^2}$$

$$\bar{\Phi}_{ij}^{(2)} = \left(-\frac{\delta_{ij}}{r^3} + \frac{3\vec{x}_i \cdot \vec{x}_j}{r^5} \right)$$

$$= \frac{\partial}{\partial x_j} \left(\frac{\partial}{\partial x_i} (\bar{\Phi}^{(0)}) \right) = \frac{\partial}{\partial x_i} \left(\frac{\partial}{\partial x_j} \bar{\Phi}^{(0)} \right) = \bar{\Phi}_{ji}^{(2)}$$

$$\begin{pmatrix} \bar{\Phi}_{11}^{(2)} & \bar{\Phi}_{12}^{(2)} & \bar{\Phi}_{13}^{(2)} \\ \bar{\Phi}_{21}^{(2)} & \bar{\Phi}_{22}^{(2)} & \bar{\Phi}_{23}^{(2)} \\ \bar{\Phi}_{31}^{(2)} & \bar{\Phi}_{32}^{(2)} & \bar{\Phi}_{33}^{(2)} \end{pmatrix}$$

$$\delta_{ij} \bar{\Phi}_{ij}^{(2)} = \bar{\Phi}_{ii}^{(2)} = \delta_{ij} \left[-\frac{\delta_{ij}}{r^3} + \frac{3\vec{x}_i \cdot \vec{x}_j}{r^5} \right]$$

$$= \left[-\frac{\delta_{ii}}{r^3} + \frac{3\vec{x}_i \cdot \vec{x}_i}{r^5} \right]$$

$$= \left[-\frac{3}{r^3} + \frac{3}{r^3} \right] = 0$$

$$\delta_{ij} \bar{\Phi}_{ij}^{(2)} = \delta_{ij} \left[\frac{\partial}{\partial x_j} \left(\frac{\partial \bar{\Phi}^{(0)}}{\partial x_i} \right) \right] = \frac{\partial}{\partial x_i} \left(\frac{\partial \bar{\Phi}^{(0)}}{\partial x_i} \right) = 0$$

$$\frac{A_{nm}}{r^{n+r'}} P_n^m(\cos\theta) e^{im\phi}$$

$$n=2 \Rightarrow \frac{A_{2m}}{r^3} P_2^m(\cos\theta) e^{im\phi}$$

$$T = \sum \left[\frac{A_{nm}}{r^{n+1}} + \frac{B_{nm}}{r^{n+1}} \right] P_n^m(\cos \theta) e^{im\phi}$$

$$\Phi^{(0)} = \frac{1}{r} \quad | \quad T = \frac{Q}{4\pi r} + T_\infty$$

$$\Phi_i^{(0)} = \frac{x_i}{r^3} \quad n=1 \quad \partial x_i$$

$$\Phi_{ij}^{(2)} = \left[-\frac{\delta_{ij}}{r^3} + \frac{3x_i x_j}{r^5} \right] \quad n=2 \quad \left[-r^2 \delta_{ij} + 3x_i x_j \right]$$

Viscous flows:

$$\nabla \cdot \underline{u} = 0 \quad \frac{\partial u_i}{\partial x_i} = 0$$

$$-\nabla p + \mu \nabla^2 \underline{u} = 0 \quad -\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} = 0$$

$$T_{ij} = -p \delta_{ij} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

$$\boxed{\nabla^2 p = 0} \quad \boxed{\nabla^2 \underline{u}^{(0)} = 0}$$

$$u_i^{(p)} = \frac{1}{2\mu} p x_i$$

$$u_i = u_i^{(0)} + u_i^{(p)}$$

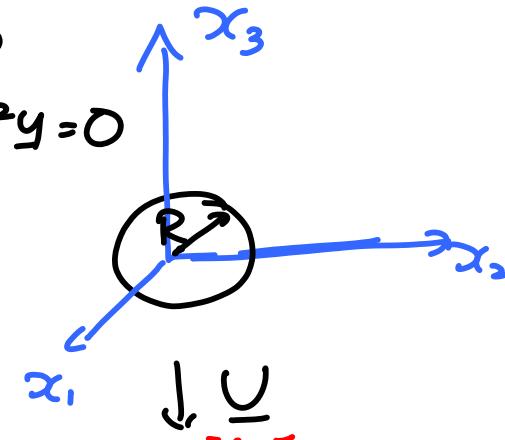
$$\nabla^2 p = 0 \quad \nabla^2 u_i^{(g)} = 0$$

$$T = \sum_{n=0}^{\infty} \sum_{m=-n}^n \left(\frac{A_{nm}}{r^{n+1}} + B_{nm} r^n \right) P_n^m(\cos\theta) e^{im\phi}$$

At $r=R$,
 $u_i = U_i$

$$\nabla \cdot \mathbf{y} = 0$$

$$-\nabla p + \mu \nabla^2 \mathbf{y} = 0$$



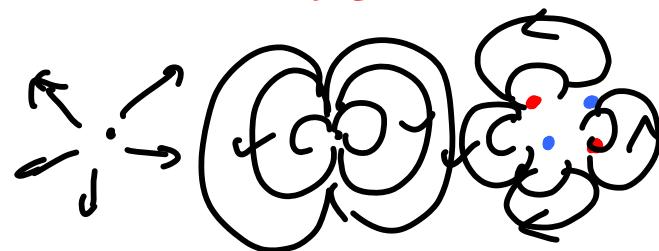
$$T = \frac{Q}{4\pi k r} + T_\infty$$

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \tilde{\Phi}^{(0)}}{\partial r} \right) = 0$$

$$\tilde{\Phi}^{(0)} = \frac{1}{r} \frac{\partial}{\partial x_i} \left(\nabla^2 \tilde{\Phi}^{(0)} \right) = 0 \quad n=0 \quad \tilde{\Phi}^{(0)} = 1$$

$$\tilde{\Phi}_i^{(1)} = \frac{x_i}{r^3} \quad \nabla^2 \left(\frac{\partial \tilde{\Phi}^{(0)}}{\partial x_i} \right) = 0 \quad n=1 \quad \tilde{\Phi}_i^{(1)} = x_i$$

$$\tilde{\Phi}_{ij}^{(2)} = \frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \quad n=2 \quad \tilde{\Phi}_{ij}^{(2)} = \delta_{ij} r^2 - 3x_i x_j$$



$$\nabla^2 p = 0 \quad \nabla^2 u_i^{(0)} = 0$$

$$p = A_3 \underline{v}_j \tilde{\Phi}_j^{(1)} = A_3 \frac{\underline{v}_j x_j}{r^3}$$

$$u_i^{(0)} = A_1 \underline{v}_i \tilde{\Phi}_i^{(0)} + A_2 \underline{v}_j \tilde{\Phi}_{ij}^{(2)}$$

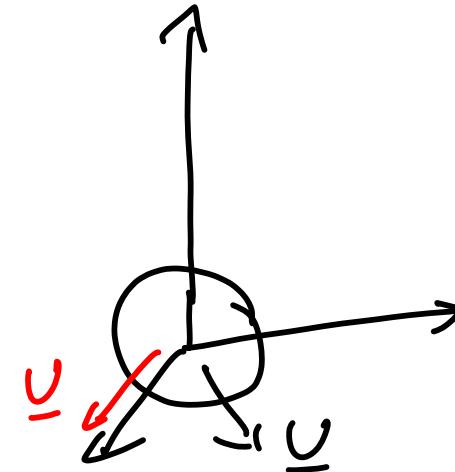
$$= A_1 \frac{\underline{v}_i}{r} + A_2 \underline{v}_j \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right)$$

$$u_i = u_i^{(0)} + \frac{1}{2\mu} p x_i$$

$$= A_1 \frac{\underline{v}_i}{r} + A_2 \underline{v}_j \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right) + \frac{A_3}{2\mu} \frac{x_i \underline{v}_j x_j}{r^3}$$

$$\frac{\partial u_i}{\partial x_i} = 0$$

$$u_i = A_1 \underline{v}_i \tilde{\Phi}_i^{(0)} + A_2 \underline{v}_j \tilde{\Phi}_{ij}^{(2)} + \frac{A_3}{2\mu} \underline{x}_i \underline{v}_j \tilde{\Phi}_j^{(1)}$$



$$\frac{\partial U_i}{\partial x_i} = A_1 V_i \frac{\partial \hat{\Phi}^{(0)}}{\partial x_i} + A_2 V_j \left[\frac{\partial}{\partial x_i} \left(\hat{\Phi}_{ij}^{(2)} \right) \right] + \frac{A_3}{2\mu} \left[\delta_{ii} V_j \hat{\Phi}_j^{(0)} + \underline{x}_i V_j \frac{\partial \hat{\Phi}_i^{(0)}}{\partial x_i} \right]$$

$$= A_1 V_i \left(-\frac{x_i}{r^3} \right) + \frac{A_3}{2\mu} \left[3V_j \hat{\Phi}_j^{(0)} + \underline{x}_i V_j \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right) \right]$$

$$= -\frac{A_1 V_i x_i}{r^3} + \frac{A_3}{2\mu} \left[\frac{3V_j x_j}{r^3} + \frac{V_j x_j}{r^3} - \frac{3x_i^2 x_j}{r^5} \right] = 0$$

$$\Rightarrow A_1 = \frac{A_3}{2\mu}$$

$$U_i = A_1 \left[\frac{V_i}{r} + \underline{x}_i \frac{x_j V_j}{r^3} \right] + A_2 V_j \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right]$$

$$= V_i \left[\frac{A_1}{r} + \frac{A_2}{r^3} \right] + V_j x_i x_j \left[\frac{A_1}{r^3} - \frac{3A_2}{r^5} \right]$$

$$Y = \underline{V} \left[\frac{A_1}{r} + \frac{A_2}{r^3} \right] + \underline{x} (\underline{V} \cdot \underline{x}) \left[\frac{A_1}{r^3} - \frac{3A_2}{r^5} \right]$$

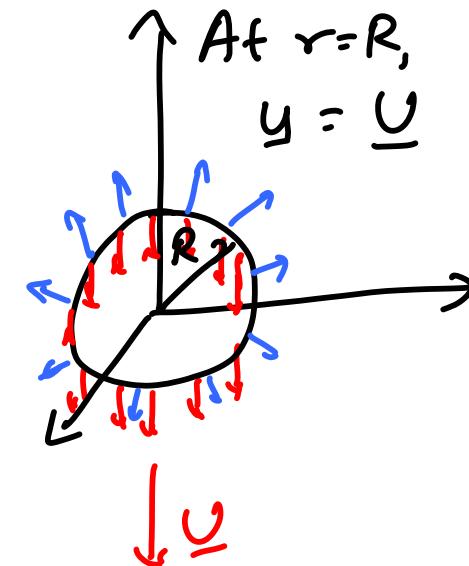
$$At \quad r=R, \quad \frac{A_1}{R} + \frac{A_2}{R^3} = 1$$

$$\frac{A_1}{R^3} - \frac{3A_2}{R^5} = 0$$

$$A_1 = \frac{3R}{4}; \quad A_2 = \frac{R^3}{4}$$

$$y = \frac{3R}{4} \left[\frac{U_i}{r} + \frac{U_j x_i x_j}{r^3} \right] + \frac{R^3}{4} U_j \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right]$$

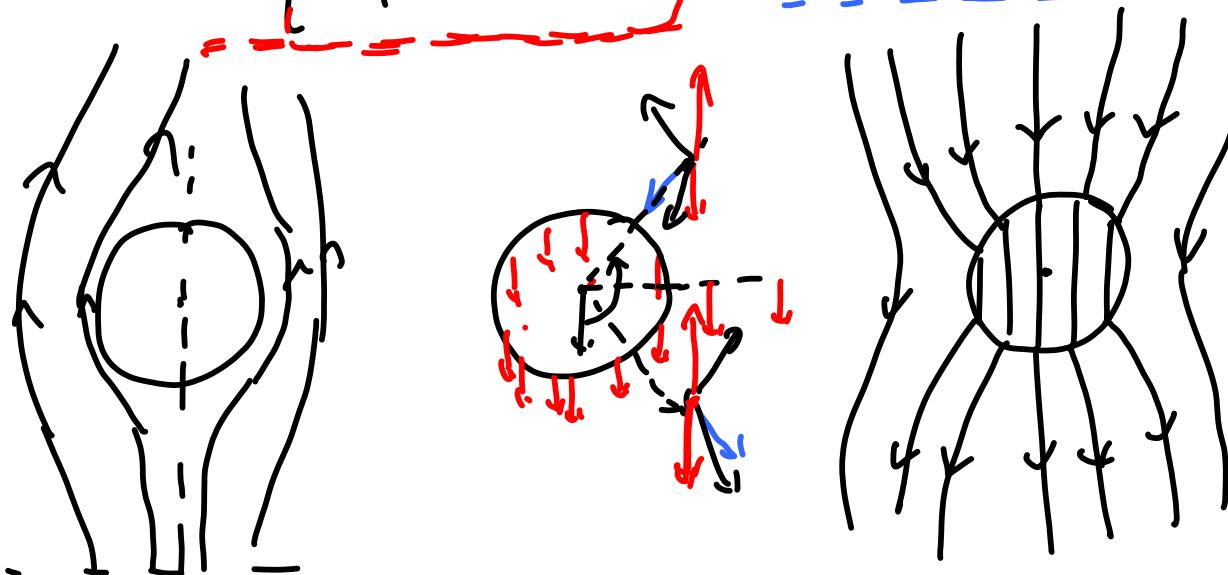
$$b = A_3 \frac{U_j x_j}{r^3} = \frac{3}{2} \frac{U R U_j x_j}{r^3}$$



$$U_i = \frac{3R}{4} \left[\frac{U_i}{r} + \frac{U_j x_i x_j}{r^3} \right] + \frac{R^3}{4} U_j \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right]$$

$$= U_i \left[\frac{3R}{4r} + \frac{R^3}{4r^3} \right] + U_j x_i x_j \left[\frac{3R}{4r^3} - \frac{3R^3}{4r^5} \right]$$

$$U = U \left[\frac{3R}{4r} + \frac{R^3}{4r^3} \right] + \underline{x} (\underline{U} \cdot \underline{x}) \left[\frac{3R}{4r^3} - \frac{3R^3}{4r^5} \right]$$



Stokes equations:

$$\nabla \cdot \underline{u} = 0$$

$$\frac{\partial u_i}{\partial x_i} = 0$$

$$-\nabla p + \mu \nabla^2 \underline{u} = 0 \quad -\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} = 0$$

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$$\frac{\partial}{\partial x_i} \left(-\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} \right) = 0$$

$$\nabla^2 p = 0 \quad \nabla^2 u_i^{(g)} = 0$$

----- -----

$$u_i^{(b)} = \frac{1}{2\mu} p x_i$$

$$u_i = u_i^{(g)} + \frac{1}{2\mu} p x_i$$

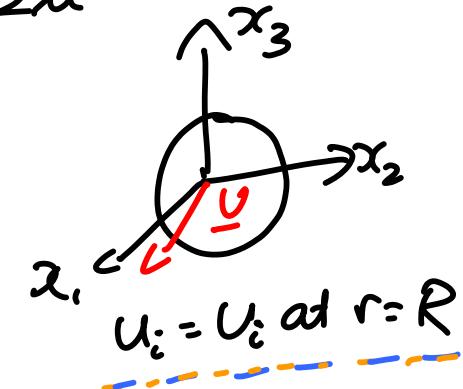
$$\nabla \cdot \underline{u} = 0$$

$$-\nabla p + \mu \nabla^2 \underline{u} = 0$$

$$\begin{cases} \nabla^2 p = 0 \\ \nabla^2 \underline{u}^{(g)} = 0 \end{cases}$$

$$u_i^{(p)} = \frac{1}{2\mu} p x_i$$

$$u_i = u_i^{(g)} + \frac{1}{2\mu} p x_i$$



$$\hat{\Phi}^{(0)} = \frac{1}{r}$$

$$\hat{\Phi}_i^{(1)} = \frac{x_i}{r^3}$$

$$\hat{\Phi}_{ij}^{(2)} = \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right]$$

$$\hat{\Phi}^{(0)} = 1$$

$$\hat{\Phi}^{(1)} = x_i$$

$$\hat{\Phi}_{ij}^{(2)} = r^2 \delta_{ij} - 3x_i x_j$$

$$p = A_3 \frac{U_i x_i}{r^3}$$

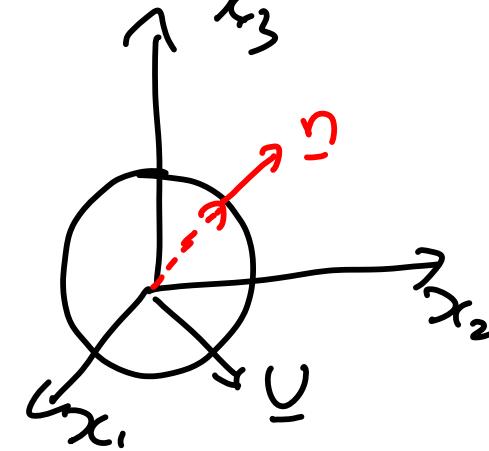
$$u_i = \frac{A_1 U_i}{r} + A_2 U_j \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right) + \frac{A_3}{2\mu} x_i \frac{U_i x_j}{r^3}$$

$$u_i = \frac{3U_j R}{4} \left[\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right] + \frac{U_j R^3}{4} \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right]$$

$$b = \frac{3\mu U_j R}{2} \left(\frac{x_i}{r^3} \right)$$

$$F_i = \int dS T_{ik} n_k = \int dS T_{ik} \left(\frac{x_k}{r} \right)$$

$$T_{ik} = -b \delta_{ik} + \mu \left(\frac{\partial u_i}{\partial x_k} + \frac{\partial u_k}{\partial x_i} \right)$$



$$n_k = \frac{x_k}{r}$$

$$U_i = \frac{3}{4} U_j R \left(\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right) + \frac{U_j R^3}{4} \hat{\Phi}_{ij}^{(2)}$$

$$\mu \frac{\partial U_i}{\partial x_k} = \frac{3\mu}{4} U_j R \left[-\frac{\delta_{ij} x_k}{r^3} + \frac{\delta_{ik} x_j}{r^3} + \frac{\delta_{jk} x_i}{r^3} - \frac{3x_i x_j x_k}{r^5} \right] + \frac{\mu U_j R^3}{4} \hat{\Phi}_{ijk}^{(3)}$$

$$\mu \frac{\partial U_k}{\partial x_i} = \frac{3\mu}{4} U_j R \left[-\frac{\delta_{ik} x_i}{r^3} + \frac{\delta_{ik} x_j}{r^3} + \frac{\delta_{ij} x_k}{r^3} - \frac{3x_i x_j x_k}{r^5} \right] + \frac{\mu U_j R^3}{4} \hat{\Phi}_{ijk}^{(3)}$$

$$-\beta \delta_{ik} = -\frac{3}{2} \frac{\mu U_j x_j}{r^3} \delta_{ik}$$

$$\begin{aligned} T_{ik} &= \frac{3}{4} \mu U_j R \left[-\frac{6x_i x_j x_k}{r^5} \right] + \frac{\mu U_j R^3}{4} \left[2 \hat{\Phi}_{ijk}^{(3)} \right] \\ &= -\frac{9}{2} \frac{\mu U_j R x_i x_j x_k}{r^5} + \frac{\mu U_j R^3}{2} \hat{\Phi}_{ijk}^{(3)} \end{aligned}$$

$$T_{ik} = -\frac{9}{2} \frac{\mu U_j R x_i x_j x_k}{r^5} + \frac{\mu U_i R^3}{2} \hat{\Phi}_{ijk}^{(3)}$$

$$\begin{aligned}\hat{\Phi}_{ijk}^{(3)} &= \frac{\partial}{\partial x_k} \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right] \\ &= \left[-\frac{3\delta_{ij} x_k}{r^5} - \frac{3\delta_{ik} x_j}{r^5} - \frac{3\delta_{jk} x_i}{r^5} + \frac{15x_i x_j x_k}{r^7} \right] \\ T_{ik} \frac{x_k}{r} &= -\frac{9}{2} \frac{\mu U_j R x_i x_j x_k^2}{r^6} + \frac{\mu U_i R^3}{2} \left[-\frac{3\delta_{ij} x_k^2}{r^6} - \frac{3x_i x_j}{r^6} - \frac{3x_i x_j}{r^6} \right. \\ &\quad \left. + \frac{15x_i x_j x_k^2}{r^8} \right] \\ &= -\frac{9}{2} \frac{\mu U_j R x_i x_j}{r^4} + \frac{\mu U_i R^3}{2} \left[-\frac{3\delta_{ij}}{r^4} - \frac{6x_i x_j}{r^6} + \frac{15x_i x_j}{r^6} \right] \\ &= -\frac{9}{2} \frac{\mu U_j R \cancel{x_i} \cancel{x_j}}{r^4} - \frac{3}{2} \frac{\mu U_i R^3 \delta_{ij}}{r^4} + \frac{9}{2} \frac{\mu U_i R^3 x_i x_j}{r^6}\end{aligned}$$

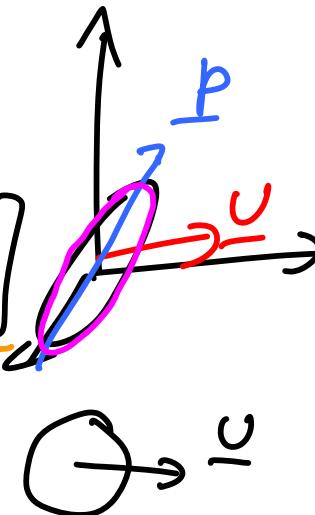
$$T_{ik} \frac{x_k}{r} \Big|_{r=R} = -\frac{3}{2} \frac{\mu U_i \delta_{ij}}{R} = -\frac{3}{2} \frac{\mu U_i}{R}$$

$$F_i = \int dS T_{ik} n_k = \left(-\frac{3}{2} \frac{\mu U_i}{R} \right) (4\pi R^2) = -6\pi \mu R U_i$$

$$\underline{\underline{F}} = -6\pi \mu R \underline{\underline{U}} \quad \text{Stokes law}$$

$$U_i = \frac{3U_j R}{4} \left[\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right] + \frac{U_j R^3}{4} \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right]$$

$$\rho = \frac{3\mu U_j x_j R}{2 r^3}$$



$$F_i = 6\pi \mu R U_i \Rightarrow U_i = \frac{F_i}{6\pi \mu R}$$

$$U_i = \frac{F_i}{8\pi \mu} \left[\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right] \quad \rho = \frac{F_i x_i}{4\pi \mu r^3} \\ = J_{ij} F_j \quad = K_i F_i$$

$$\text{Oseen tensor } J_{ij} = \frac{1}{8\pi \mu} \left(\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right) \quad K_i = \frac{x_i}{4\pi \mu r^3}$$

$$k \nabla^2 T + Q \delta(\underline{x}) = 0$$

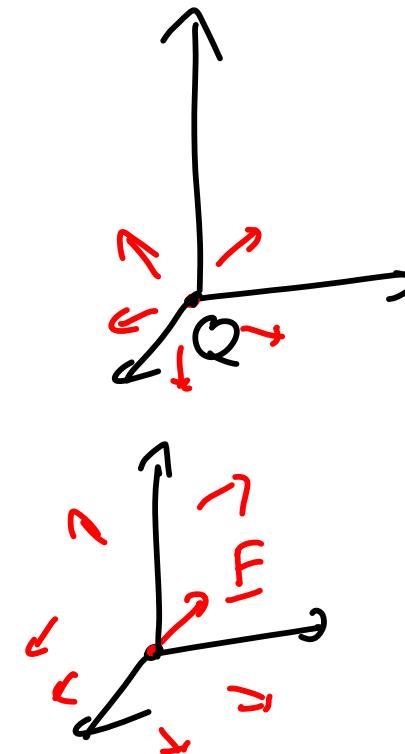
$$T = \frac{Q}{4\pi k r}$$

$$u_i = J_{ij} F_j \quad p = K_i F_i$$

$$\nabla \cdot u = 0$$

$$-\nabla p + \mu \nabla^2 u + F \delta(\underline{x}) = 0$$

$$J_{ij} = \frac{1}{8\pi\mu} \left[\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right]$$



Low Reynolds number Stokes flow:

$$\nabla \cdot \underline{u} = 0$$

$$\nabla^2 p = 0 \quad \underline{u} = \underline{u}^{(g)} + \frac{1}{2\mu} \underline{p} \times$$

$$-\nabla p + \mu \nabla^2 \underline{u} = 0 \quad \nabla^2 \underline{u}^{(g)} = 0$$

$$\hat{\Phi}^{(0)} = \frac{1}{r}$$

$$\hat{\Phi}^{(1)} = \frac{x_i}{r^3}$$

$$\hat{\Phi}^{(2)} = \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right)$$

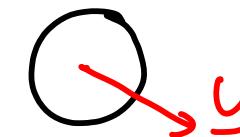
$$\hat{\Phi}^{(0)} = 1$$

$$\hat{\Phi}^{(1)} = x_i$$

$$\hat{\Phi}^{(2)} = (r^2 \delta_{ij} - 3x_i x_j)$$

$$u_i = \frac{3R}{4} u_j \left(\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right) + \frac{R^3}{4} u_j \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right)$$

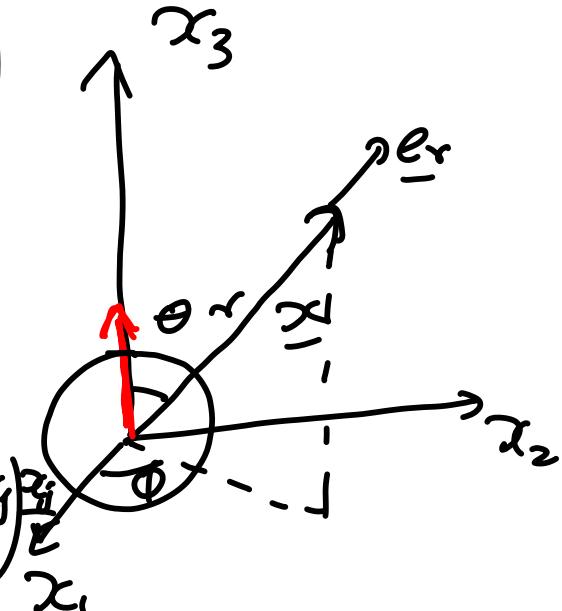
$$p = \frac{3R}{2} \mu \frac{u_j x_i}{r^3}$$



$$\underline{u} = \underline{u} \text{ at } r=R$$

$$F_i = 6\pi \mu R U_i$$

$$U_i = \frac{3U_j R}{4} \left(\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right) + \frac{R^3 U_j}{4} \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right)$$



$$U_i x_i = U \cdot \underline{x}$$

$$= U r \cos \theta$$

$$= \frac{3U_j R}{4} \left(\frac{x_i}{r^2} + \frac{x_i^2 x_j}{r^4} \right) + \frac{R^3 U_j}{4} \left[\frac{x_j}{r^4} - 3 \frac{x_i^2 x_j}{r^6} \right]$$

$$= \frac{3U_j R}{4} \left(\frac{2x_j}{r^2} \right) + \frac{R^3 U_j}{4} \left[- \frac{2x_j}{r^4} \right]$$

$$= \frac{3}{2} \frac{R U_j x_j}{r^2} - \frac{R^3 U_j x_j}{r^4}$$

$$= \frac{3}{2} \frac{R U \cos \theta}{r} - \frac{R^3 U \cos \theta}{r^3}$$

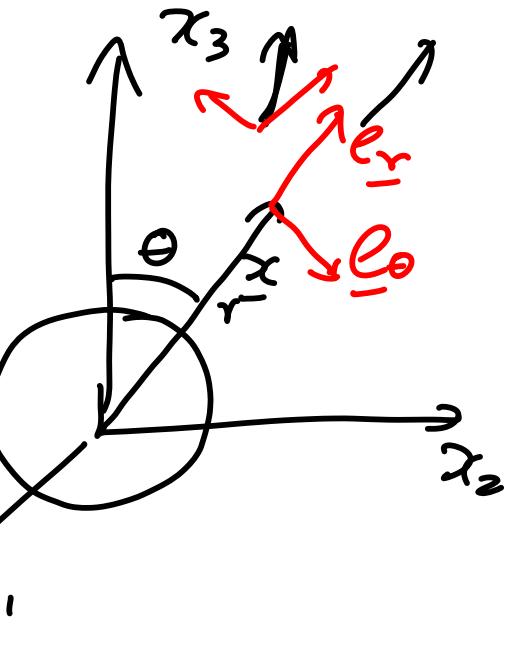
$$U_{ti} = \left(\delta_{ij} - \frac{x_i x_j}{r^2} \right) U_j$$

$$= \left[\delta_{ij} - \frac{x_i x_j}{r^2} \right] \left[\frac{3R U_k}{4} \left(\frac{\delta_{jk}}{r} + \frac{x_j x_k}{r^3} \right) + \frac{R^3 U_k}{4} \left(\frac{\delta_{jk}}{r^3} - \frac{3x_j x_k}{r^5} \right) \right]$$

$$= \left[\delta_{ik} - \frac{x_i x_k}{r^2} \right] U_k \left[\frac{3R}{4r} + \frac{R^3}{4r^3} \right]$$

$$(U_{ti} \cdot U_{ci}) = U^2 \sin^2 \theta \left[\frac{3R}{4r} + \frac{R^3}{4r^3} \right]^2$$

$$U_\theta = -U^2 \sin \theta \left[\frac{3R}{4r} + \frac{R^3}{4r^3} \right]$$

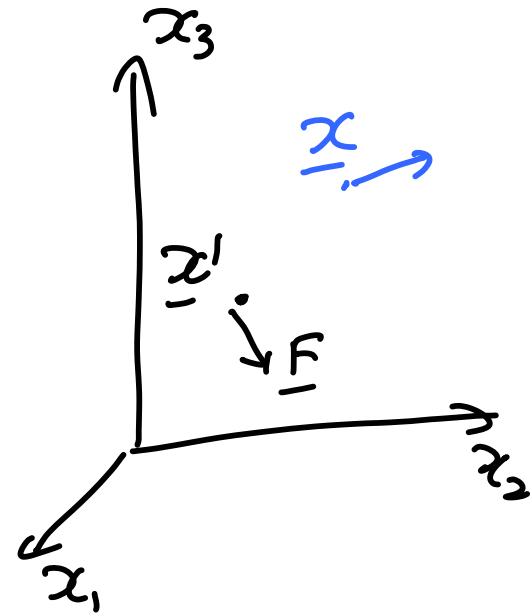


$$U_i(\underline{x}) = J_{ij} (\underline{x} - \underline{x}') F_j'(\underline{x}')$$

$$\rho(\underline{x}) = K_i (\underline{x} - \underline{x}') F_i(\underline{x}')$$

$$J_{ij} = \frac{1}{8\pi\mu} \left[\frac{\delta_{ij}}{r} + \frac{\underline{x}_i \underline{x}_j}{r^3} \right]$$

$$K_i = \frac{1}{4\pi} \frac{\underline{x}_i}{r^3}$$



Particle rotating in Stokes flow

$$\underline{u} = \boldsymbol{\Omega} \times \underline{x} \text{ at } r=R$$

$$u_i = \epsilon_{ijk} \omega_j x_k \text{ at } r=R$$

= = = = =

$$u_i^{(g)} = A_1 \epsilon_{ijk} \omega_j \bar{\phi}_k$$

- - - - -

$$+ A_2 \hat{\phi}_{ijk}^{(3)} \epsilon_{jkl} \omega_l$$

- - - - -

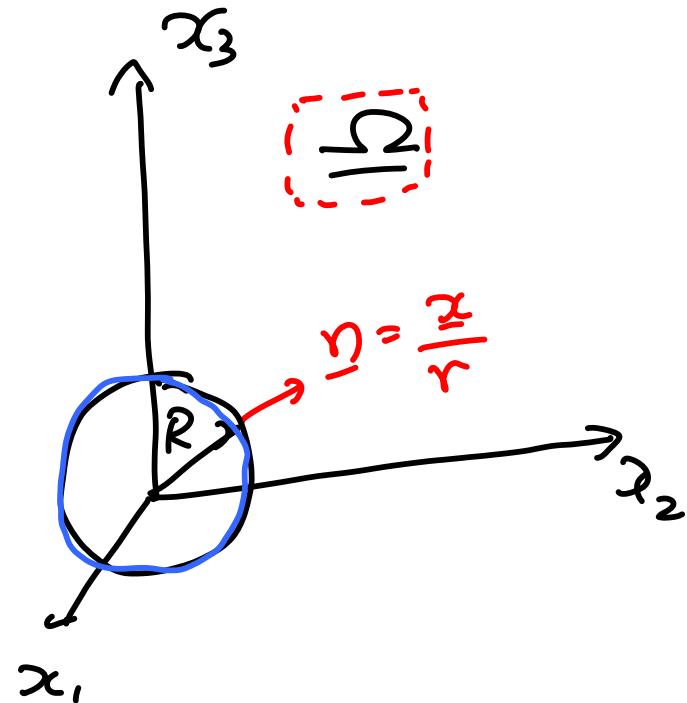
$$b = A_3 \epsilon_{ijk} \omega_k \bar{\phi}_{ij}^{(2)} = 0$$

- - - - -

$$u_i^{(g)} = R^3 \epsilon_{ijk} \omega_j \left(\frac{x_k}{r^3} \right) = u_i$$

- - - - -

$$u_i = \frac{\epsilon_{ijk} \omega_j x_k R^3}{r^3} \quad b = 0$$



$$\underline{L} = \int ds (\underline{x} \times \underline{F}) \quad L_i = \int ds \epsilon_{ijk} x_j F_k$$

$$= \int ds \epsilon_{ijk} x_j \overline{T}_{kl} n_l$$

$$\underline{T}_{kl} = \mu \left(\frac{\partial \underline{u}_k}{\partial x_l} + \frac{\partial \underline{u}_l}{\partial x_k} \right)$$

$$\underline{u}_k = \epsilon_{kmn} \frac{\underline{r}_m \underline{x}_n}{r^3} R^3$$

$$\frac{\partial \underline{u}_k}{\partial x_l} = R^3 \epsilon_{kmn} \underline{r}_m \left[\frac{\delta_{nl}}{r^3} - \frac{3x_n x_l}{r^5} \right]$$

$$\frac{\partial \underline{u}_l}{\partial x_k} = R^3 \epsilon_{lmn} \underline{r}_m \left[\frac{\delta_{lk}}{r^3} - \frac{3x_n x_k}{r^5} \right]$$

$$\begin{aligned} \overline{T}_{kl} n_l &= \mu R^3 \epsilon_{kmn} \underline{r}_m \left[\frac{\delta_{nl}}{r^3} - \frac{3x_n x_l}{r^5} \right] \frac{x_l}{r} \\ &+ \mu R^3 \epsilon_{lmn} \underline{r}_m \left[\frac{\delta_{nk}}{r^3} - \frac{3x_n x_k}{r^5} \right] \frac{x_k}{r} \end{aligned}$$

$$T_{kk} n_i = \mu R^3 \left[\epsilon_{kmn} \Omega_m \frac{x_n}{r^4} - \frac{3 \epsilon_{kmn} \Omega_m x_n x_c^2}{r^6} \right]$$

$$+ \mu R^3 \epsilon_{imk} \Omega_m \frac{x_c}{r^4}$$

$$= \mu R^3 \left[\underbrace{\epsilon_{kmn} \Omega_m \frac{x_c}{r^4}}_{\text{---}} + \underbrace{\epsilon_{imk} \Omega_m x_c}_{\text{---}} \right]$$

$$- 3 \mu R^3 \frac{\epsilon_{kmn} \Omega_m x_n}{r^4}$$

$$= \underbrace{-3 \mu R^3 \epsilon_{kmn} \Omega_m x_n}_{\text{---}} \frac{r^4}{\text{---}}$$

$$L_i = \int dS \underbrace{\epsilon_{ijk}}_{\text{---}} \underbrace{x_j}_{\text{---}} \left[\underbrace{-3 \mu R^3 \epsilon_{kmn} \Omega_m x_n}_{\text{---}} \frac{r^4}{\text{---}} \right]$$

$$\epsilon_{ijk} \epsilon_{kmn} = \delta_{im} \delta_{jn} - \delta_{in} \delta_{jm}$$

$$L_i = \underbrace{-3 \mu R^3}_{\text{---}} \int dS \underbrace{(\delta_{im} \delta_{jn} - \delta_{in} \delta_{jm})}_{\text{---}} \left[\Omega_m x_j x_n \right]$$

$$= \underbrace{-3 \mu R^3}_{\text{---}} \int dS \left(\Omega_i x_j^2 - x_i \cdot x_j \Omega_j \right)$$

$$= -\frac{3\mu R^3}{r^4} \left[\Omega_i \int ds x_j^2 - \Omega_j \int ds x_i x_j \right]$$

$$= -\frac{3\mu R^3}{r^4} \left[\Omega_i \int ds r^2 - \Omega_j \int ds x_i x_j \right]$$

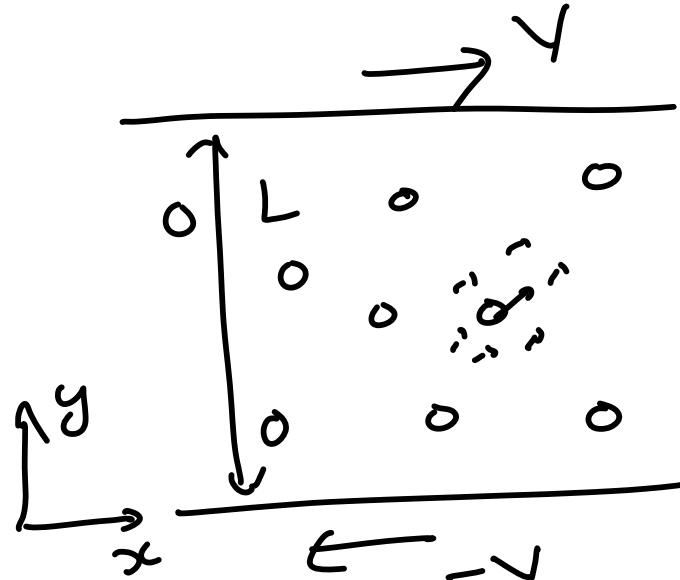
$$\underline{L}_i \Big|_{r=R} = -\frac{3\mu R^3}{R^4} \left[\Omega_i R^2 (4\pi R^2) - \Omega_j \frac{4}{3} \pi R^4 \delta_{ij} \right]$$

$$= -\frac{3\mu R^3}{R^4} \left[\frac{8}{3} \pi R^4 \Omega_i \right]$$

$$= -\frac{8\pi\mu R^3}{R^4} \underline{\underline{\Omega}}_i$$

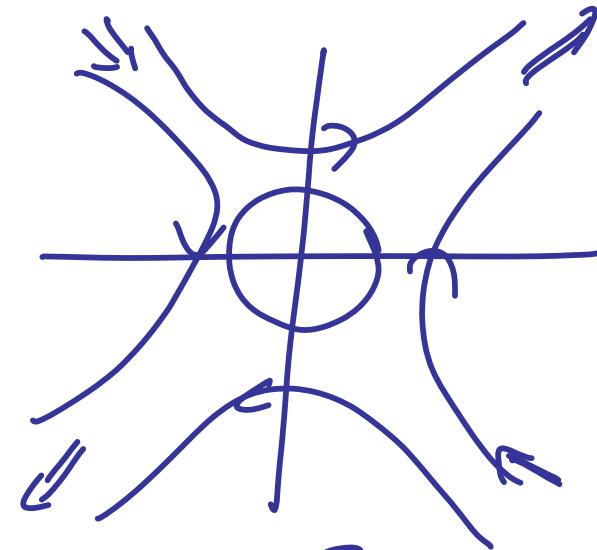
$$u_i = \frac{\epsilon_{ijk} \underline{\Omega}_j x_k R^3}{r^3} = \frac{\epsilon_{ijk} L_j x_k}{8\pi\mu r^3}$$

Effective viscosity of a suspension:



$$\bar{\tau}_{xy} = \mu_{\text{eff}} \left(\frac{2V}{L} \right)$$

Fluid viscosity μ



$$u_i = E_{ij} x_{ij}$$

'Dilute limit'

$$\langle T_{ij} \rangle = \frac{1}{V} \int dV T_{ij} = \frac{1}{V} \left[\int_{\text{Fluid}} dV T_{ij} + \int_{\text{Particle}} dV T_{ij} \right]$$

$$T_{ij} = [T_{ij} + \beta \delta_{ij} - 2\mu E_{ij}] - \beta \delta_{ij} + 2\mu E_{ij}$$

$$\langle T_{ij} \rangle = \frac{1}{V} \left[\int dV (\underbrace{T_{ij}}_{\text{---}} + \underbrace{\beta \delta_{ij}}_{\text{---}} - \underbrace{2\mu E_{ij}}_{\text{---}}) + \int dV (-\underbrace{\beta \delta_{ij}}_{\text{---}} + \underbrace{2\mu E_{ij}}_{\text{---}}) \right]$$

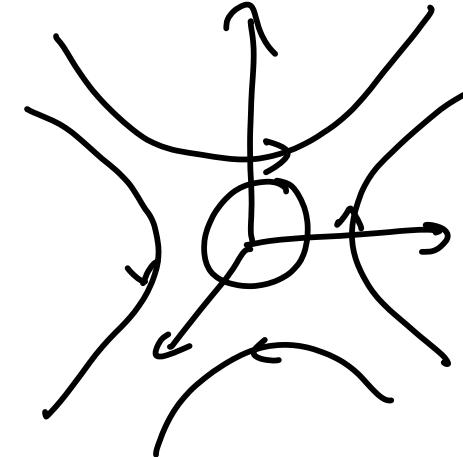
$$T_{ij} = -\beta \delta_{ij} + 2\mu E_{ij}$$

$$\begin{aligned} \langle T_{ij} \rangle &= \frac{1}{V} \int dV \left[\underbrace{T_{ij}}_{\text{particular}} + \underbrace{\beta \delta_{ij}}_{\text{---}} - \underbrace{2\mu E_{ij}}_{\text{---}} \right] \\ &\quad - \langle \beta \rangle \delta_{ij} + 2\mu \langle E_{ij} \rangle \\ &= \frac{1}{V} \int dV \underbrace{T_{ij}}_{\text{particular}} + \underbrace{(\langle \beta \rangle \delta_{ij} - \langle \beta \rangle \delta_{ij})}_{\text{---}} + \underbrace{2\mu \langle E_{ij} \rangle}_{\text{---}} \end{aligned}$$

$$\sqrt{\frac{1}{V}} \int dV T_{ij} = \frac{N}{\sqrt{V}} \int dV \underline{T}_{ij}$$

hamilton

1 particle



$$\frac{\partial}{\partial x_l} (T_{il} x_j) = \left[\frac{\partial}{\partial x_c} (T_{il}) \right] x_j + T_{il} \frac{\partial x_j}{\partial x_l}$$

$$= x_j \frac{\partial}{\partial x_c} (T_{il}) + T_{il} \delta_{jl}$$

$$= T_{ij}$$

$$\sqrt{\frac{1}{V}} \int dV T_{ij} = \sqrt{\frac{1}{V}} \int dV \frac{\partial}{\partial x_c} (T_{il} x_j)$$

hamilton

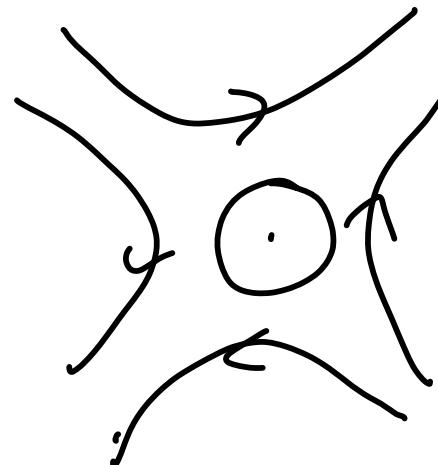
1 particle

$$= \sqrt{\frac{1}{V}} \int dV \underline{T}_{il} n_c x_j$$

hamilton

Particle in extensional flow

$$u_i^{(g)} = \underbrace{E_{ij} x_j}_{+ A_1 E_{ij} \hat{\Phi}_j^{(1)}} + A_2 E_{jk} \hat{\Phi}_{ijk}^{(3)}$$



$$p = A_3 E_{jk} \hat{\Phi}_{jk}^{(2)}$$

$$E_{ii} = E_{ij} \delta_{ij} = 0$$

$$u_i = E_{ij} x_j \left(1 - \frac{R^5}{r^5} \right) + \frac{5}{2} E_{jk} x_i x_j x_k \left(\frac{R^5}{r^7} - \frac{R^3}{r^5} \right)$$

$$p = -5 \mu R^3 x_j x_k E_{jk}$$

$$\int ds \underline{T}_{ij} \underline{n}_i x_j = \frac{20\pi R^3 \mu E_{ij}}{3}$$

$$u_i = \underbrace{E_{ij} x_j}_{+ \text{dashed line}} \text{ as } r \rightarrow \infty$$

$$u_i = 0 \text{ at } r = R$$

$$\langle T_{ij} \rangle = \frac{N}{V} \int ds \underbrace{T_{ii} n_i}_{\text{harmonic}} x_j - \langle p^i \rangle \delta_{ij} + \langle p \rangle \delta_{ij} + 2\mu \langle E_{ij} \rangle$$

$$= \frac{N}{V} \left(\frac{20 \pi R^3 \mu E_{ij}}{3} \right) - \langle p^i \rangle \delta_{ij} + \langle p \rangle \delta_{ij} + 2\mu \bar{E}_{ij}$$

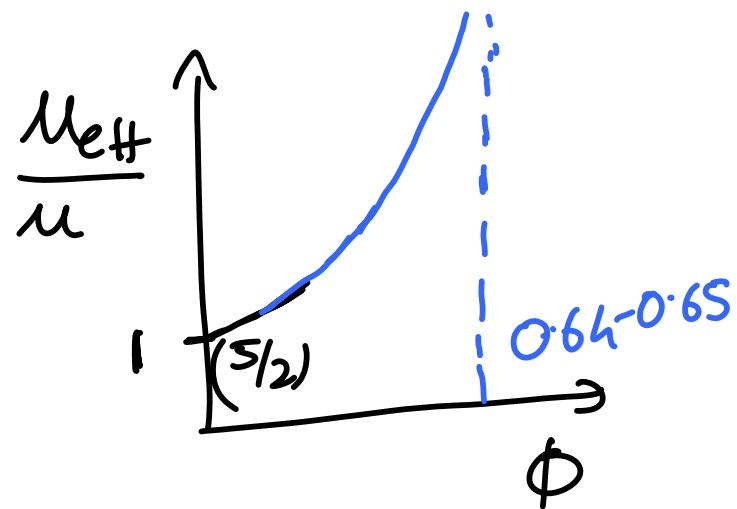
$$= 5\phi \mu E_{ij} + 2\mu E_{ij} + \delta_{ij} (\langle p \rangle - \langle p^i \rangle)$$

$$= 2\mu \left(1 + \frac{5\phi}{2} \right) E_{ij} + \delta_{ij} (\langle p \rangle - \langle p^i \rangle)$$

$$= 2\mu_{eff} E_{ij} + \delta_{ij} (\langle p \rangle - \langle p^i \rangle)$$

$$\mu_{eff} = \mu \left(1 + \frac{5\phi}{2} \right) \text{ 'Einstein viscosity'}$$

$$\mu_{\text{eff}} = \mu \left(1 + \frac{5}{2} \phi + 6.5 \phi^2 \right)$$



Low Reynolds number.

$$\nabla \cdot \mathbf{u} = 0$$

$$-\nabla p + \mu \nabla^2 \mathbf{u} = 0$$

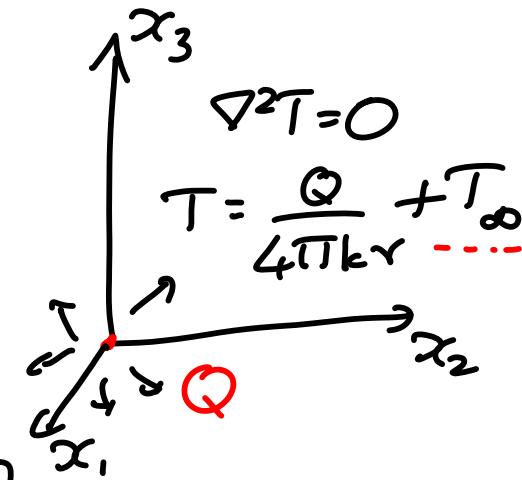
Stokes equations:

$$\nabla^2 p = 0$$

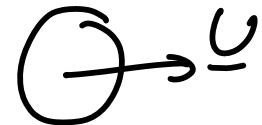
$$\nabla^2 \mathbf{u}^{(g)} = 0$$

$$\mathbf{u} = \mathbf{u}^{(g)} + \frac{1}{2\mu} \mathbf{p} \times \mathbf{x}$$

$$\left| \begin{array}{l} \Phi^{(0)} = \frac{1}{r} \\ \tilde{\Phi}_i^{(1)} = \frac{x_i}{r^3} \\ \tilde{\Phi}_{ij}^{(2)} = \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right] \\ \tilde{\Phi}^{(0)} = 1 \\ \tilde{\Phi}_i^{(1)} = x_i \\ \tilde{\Phi}_{ij}^{(2)} = (\delta_{ij} r^2 - 3x_i x_j) \end{array} \right.$$



Flow past a sphere:



$$u_i = \frac{3R}{4} u_j \left[\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right] + \frac{R^2 u_i}{4} \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right]$$

$u_i = U_i \text{ at } r=R$

$$p = \frac{3}{2} \mu R \frac{U_j x_i}{r^3} \quad F_i = 6\pi \mu R U_i$$

$$u_i = F_j \left[\frac{1}{8\pi\mu} \left(\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right) + \frac{R^2}{24\pi\mu} \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right) \right]$$

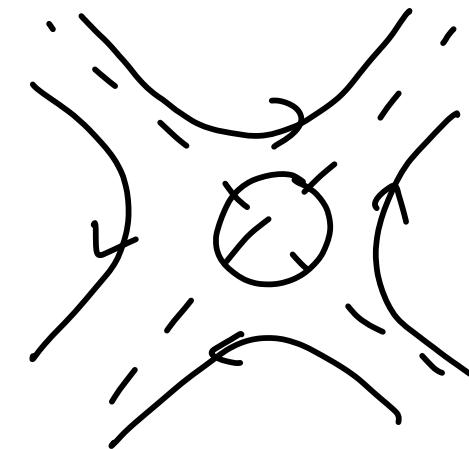
$$= J_{ij} F_j \quad \text{where } J_{ij} = \frac{1}{8\pi\mu} \left(\frac{\delta_{ij}}{r} + \frac{x_i x_j}{r^3} \right)$$

$$p = k_i F_i \quad \text{where } k_i = \frac{1}{4\pi} \left(\frac{x_i}{r^3} \right)$$

Particle in shear flow:

$$u_i = E_{ij} x_j \left[1 - \frac{R^5}{r^5} \right] +$$

$$2 E_{jkl} x_i x_j x_k \left[\frac{R^5}{r^7} - \frac{R^3}{r^5} \right]$$



As $r \rightarrow \infty$; $u_i = E_{ij} x_j$
 $r = R$; $u_i = 0$

$$F_{ij}^S = \frac{1}{2} \int_s ds (f_i x_j + f_j x_i)$$

$$= \frac{1}{2} \int_s ds [(\tau_{ic} n_c x_j + \tau_{jc} n_c x_i)]$$

$$\int_s ds [\tau_{ic} n_c x_j] = \frac{20\pi}{3} R^3 \mu (E_{ij}) = F_{ij}^S$$

$$u_i = E_{ij} x_j - \frac{3 F_{ij}^S x_i R^2}{20\pi \mu r^5} + \frac{3 x_i x_j x_k F_{jk}^S}{8\pi \mu R^3} \left[\frac{R^5}{r^7} - \frac{R^3}{r^5} \right]$$

$$= E_{ij} x_j - \frac{3 F_{jk}^S x_i x_j x_k}{8\pi \mu r^5}$$

$$u_i = \frac{\epsilon_{ijk} \omega_j x_k R^3}{r^3}$$



$$L_i = -\frac{8\pi\mu R^3 \omega_i}{}$$

$$= \epsilon_{ijk} \int ds x_j f_k$$

$$= \epsilon_{ijk} \left[\int_s^l \int ds (x_j f_k - x_k f_j) \right]$$

$$= \epsilon_{ijk} F_{jik}^A$$

$$\underline{u}_i = \epsilon_{ijk} \omega_j x_k$$

at $r=R$

$$u_i = \frac{\epsilon_{ijk} x_k R^3}{r^3} \quad \frac{L_j}{8\pi\mu R^3} = \frac{\epsilon_{ijk} L_j x_k}{8\pi\mu r^3}$$

Internal flows:

Two-dimensional internal flows:

$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} = 0$$

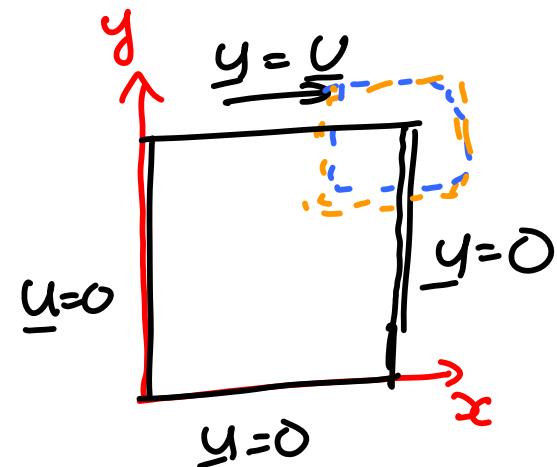
$$u_x = \frac{\partial \psi}{\partial y} \quad u_y = -\frac{\partial \psi}{\partial x}$$

$$\begin{aligned} \frac{\partial}{\partial y} \left[-\frac{\partial p}{\partial x} + \mu \nabla^2 u_x \right] &= 0 \quad \left| \begin{array}{l} -\frac{\partial p}{\partial x} + \mu \nabla^2 \left(\frac{\partial \psi}{\partial y} \right) = 0 \\ -\frac{\partial p}{\partial y} + \mu \nabla^2 \left(-\frac{\partial \psi}{\partial x} \right) = 0 \end{array} \right. \\ \frac{\partial}{\partial x} \left[-\frac{\partial p}{\partial y} + \mu \nabla^2 u_y \right] &= 0 \end{aligned}$$

$$\mu \frac{\partial}{\partial y} \left[\nabla^2 \frac{\partial \psi}{\partial y} \right] + \mu \frac{\partial}{\partial x} \left[\nabla^2 \frac{\partial \psi}{\partial x} \right] = 0$$

$$\nabla^2 [\nabla^2 \psi] = 0 \quad \text{'Biharmonic equation'}$$

$$\nabla^4 \psi = 0$$



$$u_x = \frac{\partial \psi}{\partial y}$$

$$u_y = -\frac{\partial \psi}{\partial x}$$

$$\frac{1}{r} \frac{\partial}{\partial r} (r u_r) + \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} = 0$$

$$u_r = \frac{1}{r} \frac{\partial \Psi}{\partial \theta} \quad u_\theta = -\frac{\partial \Psi}{\partial r}$$

$$\nabla^2 (\nabla^2 \Psi) = 0$$

$$\nabla^2 = \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} \right]$$

$$\Psi = r f(\theta)$$

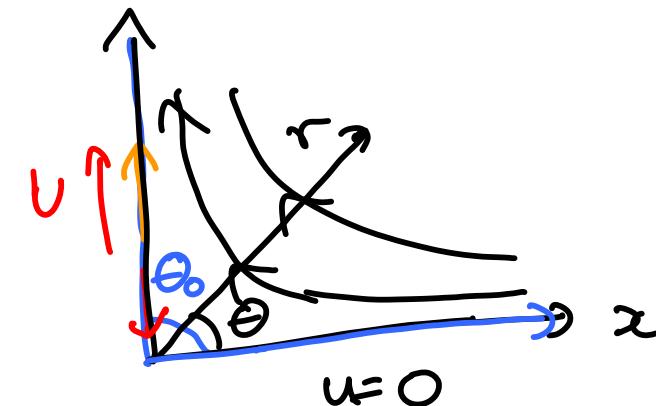
Boundary conditions for f :

$$\boxed{\text{At } \theta=0; \frac{df}{d\theta}=0; f(\theta)=0}$$

$$\boxed{\text{At } \theta=\Theta_0; \frac{df}{d\theta}=U; f(\theta)=0}$$

$$\nabla^2 \Psi = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \Psi}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \Psi}{\partial \theta^2} = \frac{1}{r} \left[\frac{d^2 f}{d\theta^2} + f \right]$$

$$\nabla^2 (\nabla^2 \Psi) = \frac{1}{r^3} \left[\frac{d^4 f}{d\theta^4} + 2 \frac{d^2 f}{d\theta^2} + f \right] = 0$$



$$0 \leq \theta \leq \Theta_0$$

$$\text{At } \theta=0; \frac{\partial \Psi}{\partial \theta} = \frac{\partial \Psi}{\partial r} = 0$$

$$\text{At } \theta=\Theta_0; \frac{\partial \Psi}{\partial r}=0; \frac{1}{r} \frac{\partial \Psi}{\partial \theta} = U$$

$$\frac{d^4 f}{d\theta^4} + \frac{2d^2 f}{d\theta^2} + f = 0$$

$$f = A \cos \theta + B \sin \theta + C \theta \cos \theta + D \theta \sin \theta$$

$$f = \frac{\nu [(\theta_0 - \theta)(\cos(\theta_0 - \theta) - \cos(\theta_0 + \theta)) - 2\theta_0 \sin(\theta_0 - \theta)]}{2(\theta_0^2 - \sin^2 \theta_0)}$$

$$\psi = r f$$

$$u_r = \frac{1}{r} \frac{\partial \psi}{\partial \theta} = \frac{df}{d\theta}; \quad u_{\theta} = -\frac{\partial \psi}{\partial r} = -f(\theta)$$

$$T_{r\theta} = \mu \left[\frac{r}{2} \frac{\partial}{\partial r} \left(\frac{u_{\theta}}{r} \right) + \frac{1}{2r} \frac{\partial u_r}{\partial \theta} \right]$$

$$= \frac{\mu}{2r} \left[\frac{d^2 f}{d\theta^2} + f(\theta) \right]$$

$$T_{r\theta}|_{\theta=\theta_0} = \frac{\mu}{2r} \left[\frac{2\theta_0 - \sin(2\theta_0)}{\theta_0^2 - \sin^2 \theta_0} \right]$$

Lubrication flows

$$BC: z=0, u_r=u_z=0$$

$$(r_c, z_c) = (0, R(1+\epsilon))$$

$$(r - r_c)^2 + (z - z_c)^2 = R^2$$

$$(z - R(1+\epsilon))^2 = R^2 - r^2$$

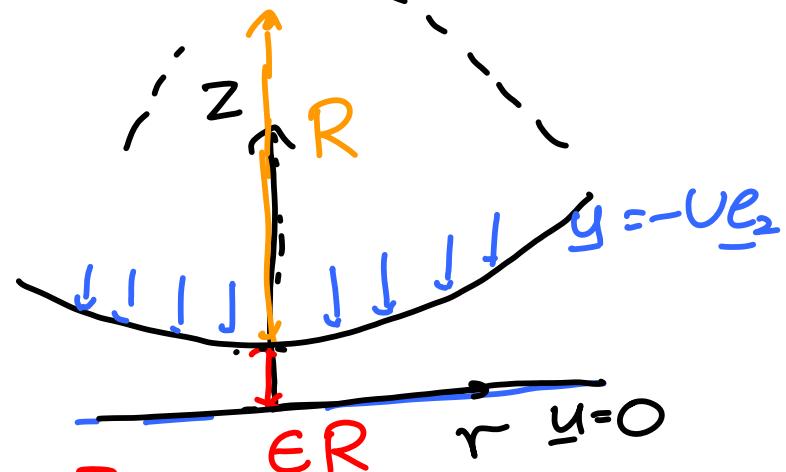
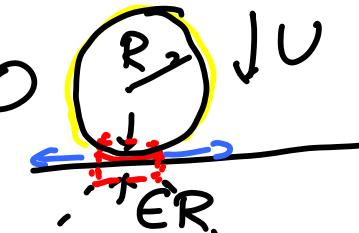
$$R(1+\epsilon) - z = \sqrt{R^2 - r^2}$$

$$z = R(1+\epsilon) - \sqrt{R^2 - r^2}$$

$$= R(1+\epsilon) - R \left(1 - \frac{r^2}{R^2} \right)^{1/2}$$

$$= R(1+\epsilon) - R \left(1 - \frac{1}{2} \frac{r^2}{R^2} \right) = R\epsilon + \frac{1}{2} \frac{r^2}{R}$$

$$z^* = 1 + \frac{1}{2} \frac{r^2}{R^2} \epsilon = 1 + \frac{1}{2} r^{*2} + \frac{1}{2!} \left(\frac{1}{2} \right)^2 \frac{r^4}{R^4 \epsilon}$$



$$z^* = \frac{2}{RE}$$

$$r^* = \frac{r}{RE}^{1/2}$$

Lubrication flow

$$z^* = \frac{z}{RE} \quad r^* = \frac{r}{RE^{1/2}} \quad z^* = h(r^*) \\ = \left(+ \frac{1}{2} r^{*2} \right)$$

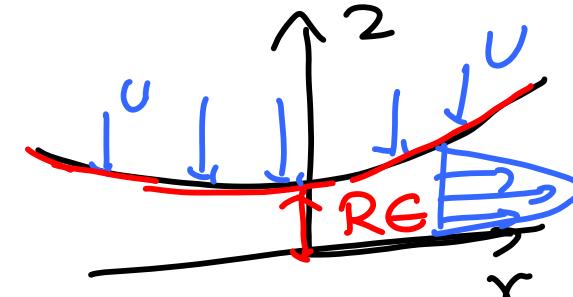
$$u_z^* = (u_z/U) \quad u_r^* = \frac{u_r}{(U/RE^{1/2})}$$

$$\frac{1}{r} \frac{\partial}{\partial r} (r u_r) + \frac{\partial u_z}{\partial z} = 0$$

$$\frac{1}{RE^{1/2}} \left(\frac{1}{r^*} \frac{\partial}{\partial r^*} (r^* u_r) \right) + \frac{U}{RE} \frac{\partial u_z^*}{\partial z^*} = 0$$

$$\left(\frac{E^{1/2}}{U} \right) \left(\frac{1}{r^*} \frac{\partial}{\partial r^*} (r^* u_r) \right) + \frac{\partial u_z^*}{\partial z^*} = 0$$

$$\frac{1}{r^*} \frac{\partial}{\partial r^*} (r^* u_r) + \frac{\partial u_z^*}{\partial z^*} = 0$$



At $z^* = 0, u_r = 0, u_z^* = 0$

At $z^* = h, u_r = 0, u_z^* = -1$

$$p^* = \frac{p}{(\mu U / RE^2)}$$

$$\text{Scalings} \quad z^* = \frac{z}{RE} \quad r^* = \frac{r}{RE^{1/2}} \quad u_r^* = \frac{u_r}{\sqrt{\epsilon}} \quad u_z^* = \frac{u_z}{(U/\epsilon^{1/2})}$$

$$t^* = t / (RE/U)$$

$$S \left(\frac{\partial u_r}{\partial t} + u_r \frac{\partial u_r}{\partial r} + u_z \frac{\partial u_r}{\partial z} \right) = - \frac{\partial p}{\partial r} + \mu \left(\frac{\partial^2 u_r}{\partial z^2} + \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_r}{\partial r} \right) \right)$$

$$S \left(\frac{U}{\epsilon^{1/2}} \frac{\partial u_r^*}{\partial t^*} + \left(\frac{U^2}{\epsilon} \right) \left(\frac{1}{RE^{1/2}} \right) u_r^* \frac{\partial u_r^*}{\partial r^*} + \left(\frac{U^2}{\epsilon^{1/2}} \right) \left(\frac{1}{RE} \right) u_z^* \frac{\partial u_r^*}{\partial z^*} \right) \\ = - \frac{1}{RE^{1/2}} \frac{\partial p}{\partial r^*} + \mu \left[\frac{U}{\epsilon^{1/2} (RE)^2} \frac{\partial^2 u_r^*}{\partial z^* \partial z^*} + \left(\frac{U}{\epsilon^{1/2}} \right) \left(\frac{1}{RE^2} \right) r^* \frac{\partial}{\partial r^*} \left(r^* \frac{\partial u_r^*}{\partial r^*} \right) \right]$$

$$\frac{S U^2}{RE^{3/2}} \left[\frac{\partial u_r^*}{\partial t^*} + u_r^* \frac{\partial u_r^*}{\partial r^*} + u_z^* \frac{\partial u_r^*}{\partial z^*} \right] = - \frac{1}{RE^{1/2}} \frac{\partial p}{\partial r^*}$$

$$+ \frac{\mu U}{RE^{5/2}} \left[\frac{\partial^2 u_r^*}{\partial z^* \partial z^*} + \epsilon \frac{1}{r^*} \frac{\partial}{\partial r^*} \left(r^* \frac{\partial u_r^*}{\partial r^*} \right) \right]$$

$$\left[\frac{S U R E}{\mu} \right] \left[\frac{\partial u_r^*}{\partial t^*} + u_r^* \frac{\partial u_r^*}{\partial r^*} + u_z^* \frac{\partial u_r^*}{\partial z^*} \right] = - \left(\frac{RE^2}{\mu U} \right) \frac{\partial p}{\partial r^*}$$

$$+ \mu \left[\frac{\partial^2 u_r^*}{\partial z^{*2}} + \frac{\epsilon}{r^*} \frac{\partial}{\partial r} \left(r^* \frac{\partial u_r^*}{\partial r} \right) \right]$$

$$\text{Re}_E \left[\frac{\partial u_r^*}{\partial t^*} + u_r^* \frac{\partial u_r^*}{\partial r^*} + u_z^* \frac{\partial u_r^*}{\partial z^*} \right] = - \frac{\partial p^*}{\partial r^*} + \mu \left[\frac{\partial^2 u_r^*}{\partial z^{*2}} + \frac{\epsilon}{r^*} \frac{\partial}{\partial r^*} \left(r^* \frac{\partial u_r^*}{\partial r^*} \right) \right]$$

$$\text{Re}_E = \left(\frac{\rho U R E}{\mu} \right)$$

$$- \frac{\partial p^*}{\partial r^*} + \frac{\partial^2 u_r^*}{\partial z^{*2}} = 0$$

$$\rho \left[\frac{\partial u_z}{\partial t} + u_r \frac{\partial u_z}{\partial r} + u_z \frac{\partial u_z}{\partial z} \right] = - \frac{\partial p}{\partial z} + \mu \left[\frac{\partial^2 u_z}{\partial z^2} + \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_z}{\partial r} \right) \right]$$

$u_z^* = (u_z / U); \quad u_r^* = u_r / (U / E^{1/2}); \quad z^* = \frac{z}{RE^{1/2}}; \quad r^* = \frac{r}{RE^{1/2}} \quad p^* = \frac{p}{(\mu U / RE^2)}$

$$\rho \left[\frac{U^2}{RE} \frac{\partial u_z^*}{\partial t^*} + \left(\frac{U^2}{E^{1/2}} \right) \left(\frac{1}{RE^{1/2}} \right) u_r^* \frac{\partial u_z^*}{\partial r^*} + \frac{U^2}{RE} u_z^* \frac{\partial u_z^*}{\partial z^*} \right]$$

$$= \left(\frac{\mu U}{R^2 E^3} \right) \frac{\partial p^*}{\partial z^*} + \mu \left[\frac{U}{R^2 E^2} \frac{\partial^2 u_2^*}{\partial z^{*2}} + \frac{U}{R^2 E} \frac{1}{r^*} \frac{\partial}{\partial r^*} \left(r^* \frac{\partial u_2^*}{\partial r^*} \right) \right]$$

$$\frac{\rho U^2}{RE} \left[\frac{\partial u_2^*}{\partial t^*} + u_r^* \frac{\partial u_2^*}{\partial r^*} + u_\theta^* \frac{\partial u_2^*}{\partial \theta^*} \right] = \left(\frac{\mu U}{R^2 E^3} \right) \frac{\partial p^*}{\partial z^*}$$

$$+ \frac{\mu U}{R^2 E^2} \left[\frac{\partial^2 u_2^*}{\partial z^{*2}} + E \frac{1}{r^*} \frac{\partial}{\partial r^*} \left(r^* \frac{\partial u_2^*}{\partial r^*} \right) \right]$$

$$\left[\frac{\rho U R E^2}{\mu} \right] \left[\frac{\partial u_2^*}{\partial t^*} + u_r^* \frac{\partial u_2^*}{\partial r^*} + u_\theta^* \frac{\partial u_2^*}{\partial \theta^*} \right] = \left[- \frac{\partial p^*}{\partial z^*} \right]$$

$$+ E \left[\frac{\partial u_2^*}{\partial z^{*2}} - \frac{1}{r^*} \frac{\partial}{\partial r^*} \left(r^* \frac{\partial u_2^*}{\partial r^*} \right) \right]$$

$$\frac{\partial p^*}{\partial z^*} = 0 ; - \frac{\partial p^*}{\partial r^*} + \frac{\partial^2 u_2^*}{\partial z^{*2}} = 0$$

Lubrication flows

at low Reynolds number

At $z=0, u_r=0, u_z=0$

At $z=h(r) \quad u_r=0 \quad u_z=-U$

$$z^* = (\rho/RE) \quad r^* = (r/RE^{1/2})$$

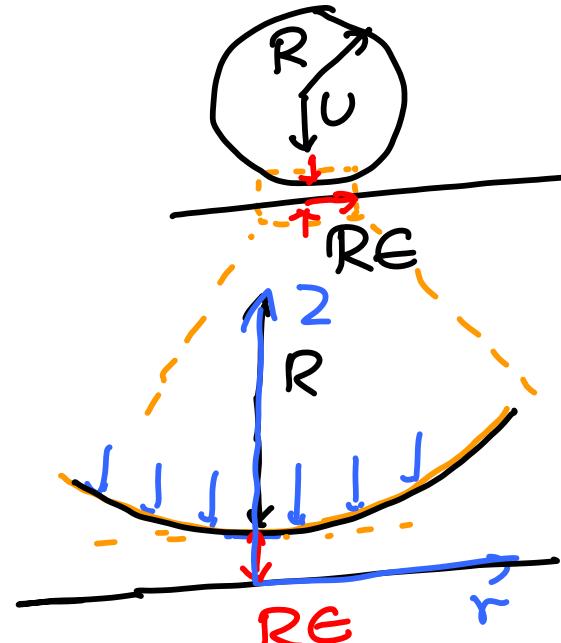
$$(z - z_c)^2 + r^2 = R^2$$

$$(z - R(1+\epsilon))^2 = R^2 - r^2$$

$$R(1+\epsilon) - z = \sqrt{R^2 - r^2}$$

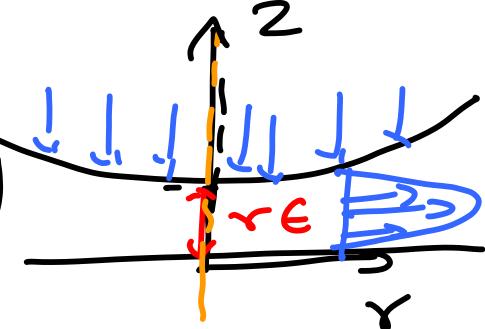
$$\vec{R} + RE - z = R \left[1 - \frac{r^2}{2R^2} \right]$$

$$z = \underline{RE} + \frac{1}{2} \frac{r^2}{R} \quad z^* = 1 + \frac{1}{2} r^{*2}$$



$$Z^* = \frac{r}{R_E}; \quad r^* = \frac{r}{R_E^{1/2}}; \quad h(r^*) = 1 + \frac{1}{2} r^{*2}$$

$$u_z^* = (u_z/v) \quad u_r^* = u_r/(v/R_E^{1/2}) \quad p^* = \frac{p}{(mv/R_E^2)}$$



$$\rho \left[\frac{\partial u_z}{\partial t} + u_r \frac{\partial u_z}{\partial r} + u_z \frac{\partial u_z}{\partial z} \right] = - \frac{\partial p}{\partial z} + \mu \left[\frac{\partial^2 u_z}{\partial z^2} + \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_z}{\partial r} \right) \right]$$

$$\frac{\rho U R_E^2}{\mu} \left[\frac{\partial u_z^*}{\partial t^*} + u_r^* \frac{\partial u_z^*}{\partial r^*} + u_z^* \frac{\partial u_z^*}{\partial z^*} \right] = - \frac{\partial p^*}{\partial z^*} + \epsilon \frac{\partial^2 u_z^*}{\partial z^{*2}} + \epsilon^2 \frac{1}{r^*} \frac{\partial}{\partial r^*} \left(r^* \frac{\partial u_z^*}{\partial r^*} \right)$$

$$\frac{\rho U R_E}{\mu} \ll 1$$

$$-\frac{\partial p^*}{\partial r^*} + \frac{\partial^2 u_r^*}{\partial z^{*2}} = 0 \quad \frac{1}{r^*} \frac{\partial}{\partial r^*} (r^* u_r^*) + \frac{\partial u_z^*}{\partial z^*} = 0$$

$$\frac{\partial p^*}{\partial z^*} = 0$$

B.C. At $z^* = 0$ $u_r^* = 0, u_z^* = 0$
 $z^* = h(r^*)$ $u_r^* = 0, u_z^* = -1$

$$\frac{\partial^2 u_r^*}{\partial z^{*2}} = \frac{\partial p^*}{\partial r^*}$$

$$u_r^* = \frac{\partial p^*}{\partial r^*} \frac{z^{*2}}{2} + G(r^*) z^* + C_2(r^*)$$

$$u_r^* = \frac{\partial p^*}{\partial r^*} \left(\frac{z^{*2}}{2} - \frac{z^* h}{2} \right)$$

$$\int_0^{h(r^*)} dz^* \frac{1}{r^*} \frac{\partial}{\partial r^*} (r^* u_r^*) + \int_0^{h(r^*)} dz \frac{\partial u_z^*}{\partial z^*} = 0$$

$$\int_0^{h(r^*)} dz^* \frac{1}{r^*} \frac{\partial}{\partial r^*} (r^* u_r^*) + \left[u_z^* \Big|_{z=h(r)} - u_z^* \Big|_{z=0} \right] = 0$$

$$\int_0^{h(r^*)} dz^* \frac{1}{r^*} \frac{\partial}{\partial r^*} (r^* u_{r^*}) + [-1 - 0] = 0$$

$$\frac{1}{r^*} \frac{\partial}{\partial r^*} \left(r^* \int_0^{h(r^*)} dz^* u_{r^*} \right) = 1$$

$$\frac{1}{r^*} \frac{\partial}{\partial r^*} \left[r^* \int_0^{h(r^*)} dz^* \left(\frac{\partial p^*}{\partial r^*} \right) \left(\frac{z^*^2}{2} - \frac{2^* h}{2} \right) \right] = 1$$

$$\frac{1}{r^*} \frac{\partial}{\partial r^*} \left[r^* \left(-\frac{h^3}{12} \frac{\partial p^*}{\partial r^*} \right) \right] = 1$$

$$\frac{\partial p^*}{\partial r^*} = -\frac{6 r^*}{h(r^*)^3} - \frac{C_1}{r^* h(r^*)^3}$$

$$h(r^*) = 1 + \frac{1}{2} r^{*2}$$

$$p^* = \frac{3}{(1 + \frac{1}{2} r^{*2})^2} + C_2$$

$$p^* \xrightarrow[r \rightarrow \infty]{} 0 \Rightarrow C_2 = 0$$

$$p^* \sim \frac{p w u}{R} \approx 0$$

$$p^* = \frac{p}{(\mu v / R)^2}$$

$$p^* = \frac{3}{(1 + \gamma_2 r^{*2})^2}$$

$$p \sim \frac{\mu U}{R E^2} \quad \text{Area} \sim R^2 E$$

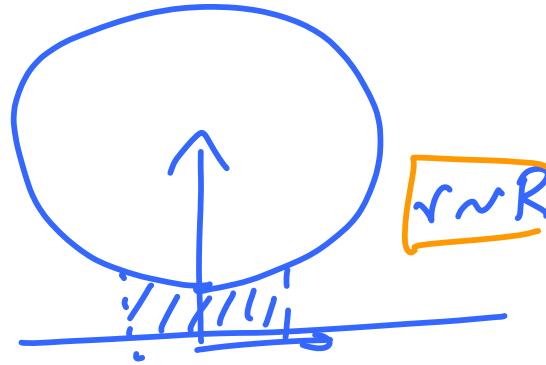
$$\text{Force} \sim \frac{\mu U}{R E^2} \times R^2 E \sim \frac{\mu U R}{E}$$

$$p \sim \frac{\mu U}{R} \quad \text{Area} \sim R^2$$

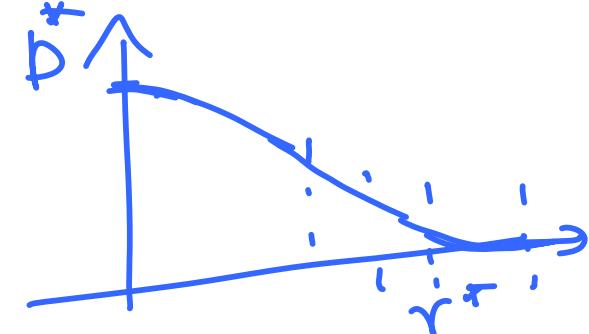
$$\text{Force} \sim \frac{\mu U R}{E}$$

$$0 < r < R$$

$$0 < r' < \frac{R}{R E^{1/2}}$$



$$\frac{r \sim R E^{1/2}}{r^* \sim 1}$$



$$F_2 = 2\pi \int r dr p = 2\pi (R^2 E) \left(\frac{\mu U}{R E^2}\right) \int_0^\infty r^* dr^* p^*$$

$$= 2\pi \frac{\mu R U}{E} \int_0^\infty r^* dr^* \frac{3}{(1 + \gamma_2 r^{*2})^2} = \frac{6\pi \mu R U}{E}$$

Low Reynolds number viscous flows:

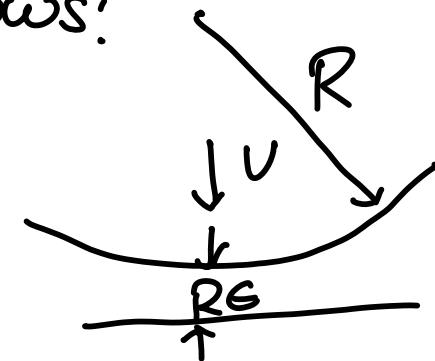
$$\nabla \cdot \underline{u} = 0$$

$$-\nabla p + \mu \nabla^2 \underline{u} = 0$$

$$\nabla^2 p = 0$$

$$\nabla^2 \underline{u}^{(g)} = 0$$

$$\underline{u} = \underline{u}^{(g)} + \frac{1}{2\mu} \nabla p \approx$$



$$u_x = \frac{\partial \psi}{\partial y} \quad u_y = -\frac{\partial \psi}{\partial x}$$

$$F = \frac{6\pi\mu R U}{E}$$



$$\nabla^2(\nabla^2 \psi) = 0$$

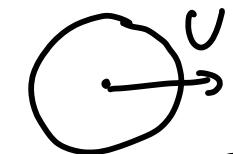
$$\nabla^4 \psi = 0$$

Inertial corrections to Stokes flow:

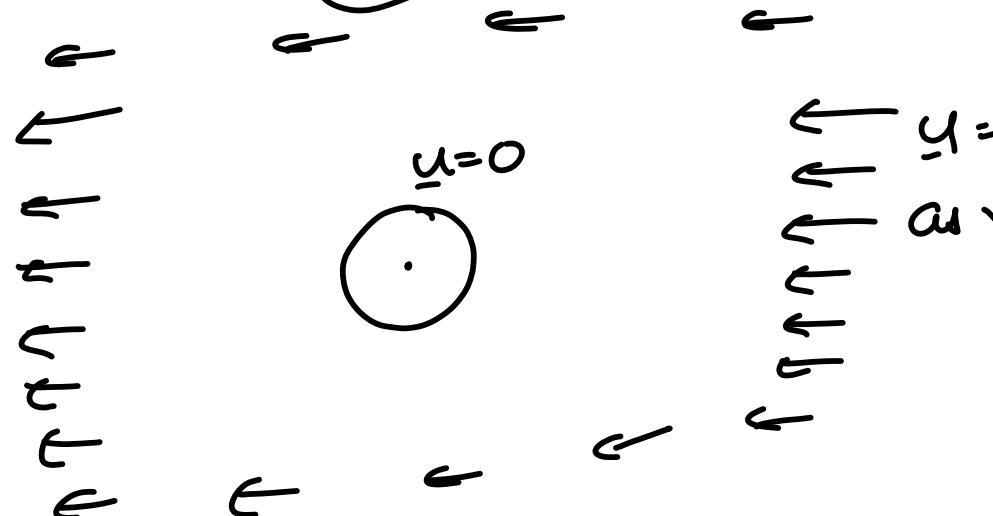
\underline{u}

$$\underline{u} = 0$$

$$a \rightarrow r \rightarrow \infty$$



$$\underline{u} = 0$$



$$\underline{u} = -\underline{v} + \underline{u}'(x)$$

$$\nabla \cdot \underline{u} = 0$$

$$S[\underline{u} \cdot \nabla \underline{u}] = -\nabla p + \mu \nabla^2 \underline{u}$$

$$S[(\underline{v} + \underline{u}') \nabla \underline{u}'] = -\nabla p + \mu \nabla^2 \underline{u}'$$

$$\underline{u}' \propto \frac{1}{r} \text{ as } r \rightarrow \infty \quad \underline{u}'^* \propto \left(\frac{R}{r}\right)$$

$$\nabla \underline{u}' \propto \frac{1}{r^2}$$

$$\nabla^2 \underline{u}' \propto \frac{1}{r^3}$$

$$\nabla^* \underline{u}'^* \propto \left(\frac{R}{r}\right)^2$$

$$\nabla^{*2} \underline{u}'^* \propto \left(\frac{R}{r}\right)^3$$

$$r^* = \left(r/R\right); \quad \underline{u}'^* = \left(\underline{u}'/\underline{v}\right) \quad \underline{v}^* = \left(\underline{v}/v\right); \quad \nabla^* = R^* \nabla$$

$$\operatorname{Re} \left[(-\underline{v}^* + \underline{u}'^*) \cdot \nabla^* \underline{u}'^* \right] = -\nabla^* p^* + \nabla^{*2} \underline{u}'^*$$

$$\operatorname{Re} = \left(\frac{\underline{v} R}{\underline{u}} \right)$$

$$\operatorname{Re} \left[\frac{(-\underline{v}^* + \underline{u}'^*)}{O(1)} \cdot \frac{\nabla^* \underline{u}'^*}{\left(R/r\right)^2} \right] = -\nabla^* p^* + \nabla^{*2} \underline{u}'^* \quad \left(\frac{R}{r}\right)^3$$

$$\operatorname{Re} \left(\frac{R}{r} \right)^2$$

$$\left(\frac{R}{r}\right)^3$$

Inertial terms become important

$$\text{for } \frac{r}{R} \propto Re^{-1} \Rightarrow r \propto \frac{\mu}{g u R}$$

$$\text{or } r \propto \frac{\mu}{g u}$$

$$Re \left[(\underline{u}^* + \underline{u}''). \nabla^* \underline{u}' \right] = -\nabla^* p^* + \nabla^{*2} \underline{u}'^*$$

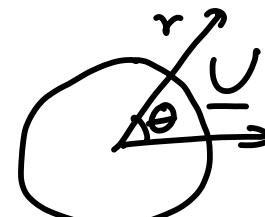
$\underline{O}(u) \quad \underline{O}\left(\frac{u R}{r}\right)$

$$\text{For } \frac{r}{R} \ll Re^{-1} \quad \text{For } \frac{r}{R} \gg Re^{-1} \quad \underline{u}'' \ll \underline{u}^*$$

$$-Re \underline{u}^* \cdot \nabla^* (\underline{u}'^*) = -\nabla^* p^* + \nabla^{*2} \underline{u}'^*$$

Oseen equation

$$-S \underline{u} \cdot \nabla \underline{u}' = -\nabla p + \underline{\mu} \nabla^2 \underline{u}'$$



$$u_r = \frac{1}{r^2 \sin \theta} \frac{\partial \psi}{\partial \theta} \quad u_\theta = \frac{-1}{r \sin \theta} \frac{\partial \psi}{\partial r}$$

$$\frac{1}{r^2} \frac{\partial}{\partial r} (r^2 u_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta u_\theta) = 0$$

$$\psi = UR^2 \left[-\frac{1}{4} \frac{R}{r} \sin^2 \theta + 3(1 - \cos \theta) \left[\frac{1 - \operatorname{erf}(-\frac{1}{8} \frac{\operatorname{Re}(1 + \cos \theta)}{r/R})}{2 \operatorname{Re}} \right] \right]$$

$$\operatorname{Re} = \frac{\rho U R}{\mu} \quad \psi = UR^2 \sin^2 \theta \left[-\frac{1}{4} \frac{R}{r} + \frac{3}{4} \frac{r}{R} \right]$$

$$F_i = 6\pi \mu R U_i \left(1 + \frac{3}{8} \operatorname{Re} \right) \text{ 'Oseen correction'}$$

High Reynolds number 'potential flow':

$$\nabla \cdot \underline{u} = 0 \quad \nabla \cdot (\nabla \phi) = 0 \quad \nabla^2 \phi = 0$$

$$\cancel{\rho} \left[\frac{\partial \underline{u}}{\partial t} + \underline{u} \cdot \nabla \underline{u} \right] = -\nabla p + \cancel{\underline{u} \nabla^2 \underline{u}} + f$$

① Inviscid

② Irrotational $\underline{\omega} = \nabla \times \underline{u} = 0$ // Potential

$$\underline{u} = \nabla \phi \Rightarrow \nabla \times \nabla \phi = 0$$

ϕ = Velocity potential

$$\rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = - \frac{\partial p}{\partial x_i} + f_i$$

$$\rho \left(\frac{\partial}{\partial t} \left(\frac{\partial \Phi}{\partial x_i} \right) + \frac{\partial}{\partial x_i} \left(\frac{1}{2} u_j^2 \right) \right) = - \frac{\partial p}{\partial x_i} + f_i$$

$$\frac{\partial}{\partial x_i} \left[\rho \frac{\partial \Phi}{\partial t} + \frac{1}{2} \rho u_j^2 \right] = - \frac{\partial p}{\partial x_i} + f_i$$

$$f_i = - \frac{\partial V}{\partial x_i}$$

$$\frac{\partial}{\partial x_i} \left[p + V + \rho \frac{\partial \Phi}{\partial t} + \frac{1}{2} \rho u_j^2 \right] = 0$$

$$p + V + \rho \frac{\partial \Phi}{\partial t} + \frac{1}{2} \rho u_j^2 = p_0$$

'Bernoulli equation'

$$p + \rho g z + \rho \frac{\partial \Phi}{\partial t} + \frac{1}{2} \rho u_j^2 = p_0$$

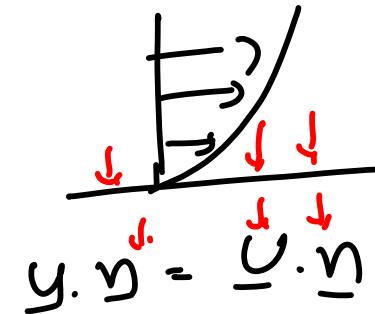
Potential flow equations

$$\nabla^2 \phi = 0$$

$$u_i = \frac{\partial \phi}{\partial x_i}$$

$$p + \frac{1}{2} \rho u_i^2 + \rho \frac{\partial \phi}{\partial x_i} + V = p_0$$

$$T_{ij} = -\rho \delta_{ij}$$



High Reynolds number potential flow:

Inviscid $\mu = 0$

Irrational $\omega = \nabla \times \underline{y} = 0$ $\underline{y} = \nabla \phi$

$$\nabla \cdot \underline{y} = 0 \quad \nabla^2 \phi = 0 \quad f = -\nabla V$$

$$g \left[\frac{\partial \underline{u}}{\partial t} + \underline{y} \cdot \nabla \underline{y} \right] = -\nabla p + \mu \nabla^2 \underline{y} + f$$

$$\frac{\partial}{\partial x_i} \left[p + \frac{1}{2} \rho \underline{y}_i^2 + V \right] = 0$$

$$p + \frac{1}{2} \rho \underline{y}_i^2 + V = p_0$$

$$T_{ij} = -p \delta_{ij}$$

$$\begin{cases} \frac{\partial c}{\partial t} + \underline{y} \cdot \nabla c = D \nabla^2 c \\ D \nabla^2 c = 0 \\ \frac{\partial c}{\partial t} + \underline{y} \cdot \nabla c = 0 \\ \underline{y} \cdot \nabla c = 0 \end{cases}$$

If there is no normal velocity at boundaries,
the fluid velocity is zero everywhere.

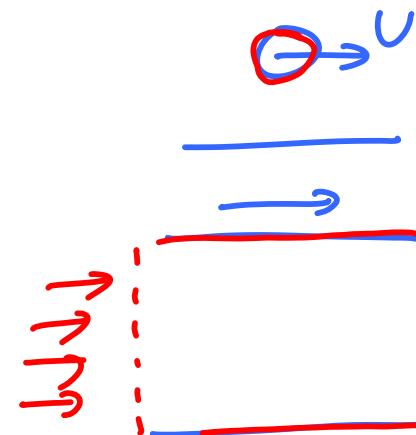
$$\text{Kinetic energy} = \int dV \left(\frac{1}{2} \rho u_i^2 \right) \geq 0$$

$$= \frac{1}{2} \rho \int dV u_i^2 = \frac{1}{2} \rho \int dV u_i \cdot x u_i$$

$$= \frac{1}{2} \rho \int dV u_i \cdot \frac{\partial \phi}{\partial x_i}$$

$$= \frac{1}{2} \rho \int dV \left(\frac{\partial}{\partial x_i} (u_i \phi) - \cancel{\phi \frac{\partial u_i}{\partial x_i}} \right)$$

$$= \frac{1}{2} \rho \int dV \frac{\partial}{\partial x_i} (u_i \phi) = \frac{1}{2} \rho \int dS \left(n_i u_i \phi \right)$$



Uniqueness: For specified normal velocity conditions at boundaries, the potential flow solution is unique.

Assume two solutions (u_i, u_i^*) satisfy the normal velocity conditions $\underline{u_i} \cdot \underline{n_i} = \underline{u_i^*} \cdot \underline{n_i}$ at the surface.

$$\underline{I} = \int dV (u_i^* - u_i)(u_i^* - u_i) \geq 0 = 0$$

$$= \int dV (u_i^* - u_i) \frac{\partial}{\partial x_i} (\phi^* - \phi)$$

$$= \int dV \left\{ \frac{\partial}{\partial x_i} [(u_i^* - u_i)(\phi^* - \phi)] - (\phi^* - \phi) \cancel{\frac{\partial}{\partial x_i}} (u_i^* - u_i) \right\}$$

$$= \int dV \cancel{\frac{\partial}{\partial x_i}} ((u_i^* - u_i)(\phi^* - \phi)) = \int ds \underline{n_i} \cancel{(u_i^* - u_i)} (\phi^* - \phi)$$

Minimum kinetic energy principle:

For a given set of zero normal velocity conditions at surface, the total kinetic energy of a potential flow is smaller than that of any other flow.

$$(\underline{y}, \underline{u}^*) \quad \underline{u} = \nabla \phi \quad \nabla \cdot \underline{u}^* = \nabla \cdot \underline{u} = 0$$

$$KE = \int dV \left(\frac{1}{2} \rho u^2 \right) \leq \int dV \frac{1}{2} \rho u^{*2}$$

$$\begin{aligned} KE^* - KE &= \frac{1}{2} \int dV \underline{(u_i^* - u_i)^2} \\ &= \frac{1}{2} \int dV \left[\underline{(u_i^* - u_i)^2} + 2 \underline{u_i} (\underline{u_i^* - u_i}) \right] \\ &= \frac{1}{2} \int dV (u_i^* - u_i)^2 + \int dV [u_i (u_i^* - u_i)] \\ &= \frac{1}{2} \int dV (u_i^* - u_i)^2 + \int dV \left(\frac{\partial \Phi}{\partial x_i} \right) (u_i^* - u_i) \\ &= \frac{1}{2} \int dV (u_i^* - u_i)^2 + \int dV \left[\frac{\partial}{\partial x_i} (\Phi(u_i^* - u_i)) - \Phi \frac{\partial}{\partial x_i} (u_i^* - u_i) \right] \end{aligned}$$

$$= \frac{1}{2} \oint dV (u_i^* - u_i)^2 + \oint dV \frac{\partial}{\partial x_i} (\phi(u_i^* - u_i))$$

$$KE^* - KE = \frac{1}{2} \oint dV (u_i^* - u_i)^2 + \oint dS n_i (u_i^* - u_i) \phi$$

$$KE = \frac{1}{2} \oint dV u_i^2 = \frac{1}{2} \oint dS n_i \phi u_i$$

Flow around a sphere:

$$\nabla^2 \phi = 0$$

$$\phi = A \underbrace{U_j \frac{\tilde{\Phi}_j^{(1)}}{r}}_{\text{--- --- ---}} = \frac{AU_i x_j}{r^3}$$

$$U_i = \frac{\partial \phi}{\partial x_i} = AU_j \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right]$$

$$U_i n_i = U_i n_i$$

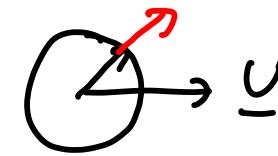
$$AU_j \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right] \frac{x_i}{r} = \frac{U_i x_i}{r} \quad \text{at } r=R$$

$$A \frac{U_i x_i}{r^4} - \frac{3AU_j x_i^2 x_j}{r^6} = \frac{U_i x_i}{r}$$

$$-2AU_j \frac{x_j}{r^4} > \frac{U_i x_i}{r} \quad \text{at } r=R$$

$$A = -\frac{R^3}{2}$$

As $r \rightarrow \infty$, $U_i = 0$

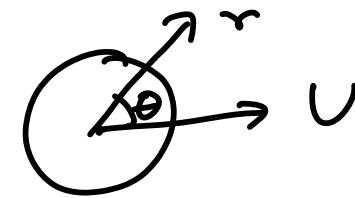


$$\text{At } r=R \quad U_i n_i = U_i n_i$$

$$n_i \frac{\partial \phi}{\partial x_i} = U_i n_i$$

$$n_i = \frac{x_i}{r}$$

$$\phi = -\frac{R^3}{2} \frac{U_i x_j}{r^3} = -\frac{R^3}{2} \frac{U \cos \theta}{r^2}$$

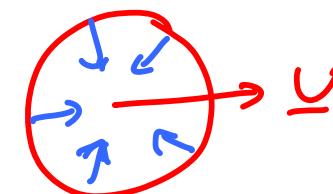


$$U_i = -\frac{R^3}{2} \left[\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right]$$

$$U_r = \frac{\partial \phi}{\partial r} = -\frac{R^3 U \cos \theta}{r^3}$$

$$U_\theta = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = \frac{R^3 U \sin \theta}{2r^3}$$

$$U_i n_i = U_i n_i$$



$$KE = \frac{1}{2} \oint ds \phi \underline{n}_i \underline{u}_j$$

$$= -\frac{1}{2} \oint ds \phi u_i \left(\frac{x_j}{r} \right)$$

$$= -\frac{1}{2} \oint ds \phi \frac{U_i x_j}{r}$$

$$\phi = -\frac{R^3}{2} \frac{U_i x_i}{r^3}$$

$$KE = \frac{R^3}{4} S \int ds \left(\frac{U_i x_i}{r^3} \right) \left(\frac{U_j x_j}{r} \right)$$

$$= \frac{S}{4R} U_i U_j \int ds x_i x_j$$

- - - - -

$$\int ds x_i x_j = A \delta_{ij} \quad A = \frac{4\pi R^3}{3}$$

$$= \frac{4\pi R^6}{3} \delta_{ij}$$

$$KE = \frac{8\pi R^3}{3} U_j^2 = \frac{1}{2} S U_j^2 \left(\frac{2\pi R^3}{3} \right)$$

$$= \frac{1}{2} M_a U_j^2$$

$$M_a = \text{Added mass} = S \left(\frac{2}{3} \pi R^3 \right)$$

$= \frac{1}{2}$ of mass of fluid displaced
by the sphere.

Potential flows:

Inviscid

Irrational $\nabla \times \underline{u} = \underline{\omega} = 0$

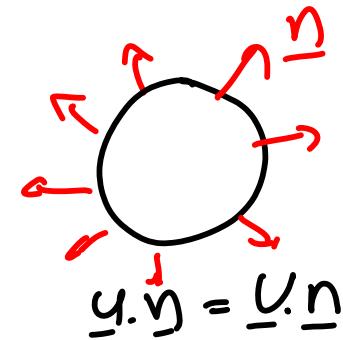
$\underline{u} = \nabla \phi$ 'Velocity potential'

$$\nabla \cdot \underline{u} = 0 \implies \nabla^2 \phi = 0$$

$$\rho \left(\frac{\partial \underline{u}}{\partial t} + \underline{u} \cdot \underline{\nabla} \underline{u} \right) = -\nabla p + \underline{f} \quad f = -\nabla V$$

$$\nabla \left(p + \frac{1}{2} \rho u^2 + \rho \frac{\partial \phi}{\partial t} + V \right) = 0 \quad T_{ij} = -p \delta_{ij}$$

$$p + \frac{1}{2} \rho u^2 + \rho \frac{\partial \phi}{\partial t} + V = p_0$$



$$\nabla^2 \phi = 0$$

$$\phi = \text{Linear}(U_i, \underline{\Phi}^{(n)})$$

$$= A U_j \underline{\Phi}_j^{(1)} = \frac{A U_j x_j}{r^3}$$

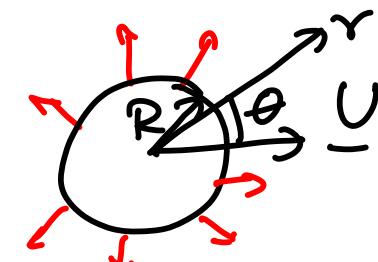
$$n_i = \frac{x_i}{r} = \frac{x_i}{R}$$

$$U_i n_i = U_i n_i$$

$$U_i = \frac{\partial \phi}{\partial x_i} = A U_j \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right)$$

$$A U_j \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right) \frac{x_i}{r} = \frac{U_i x_i}{r} \text{ at } r=R$$

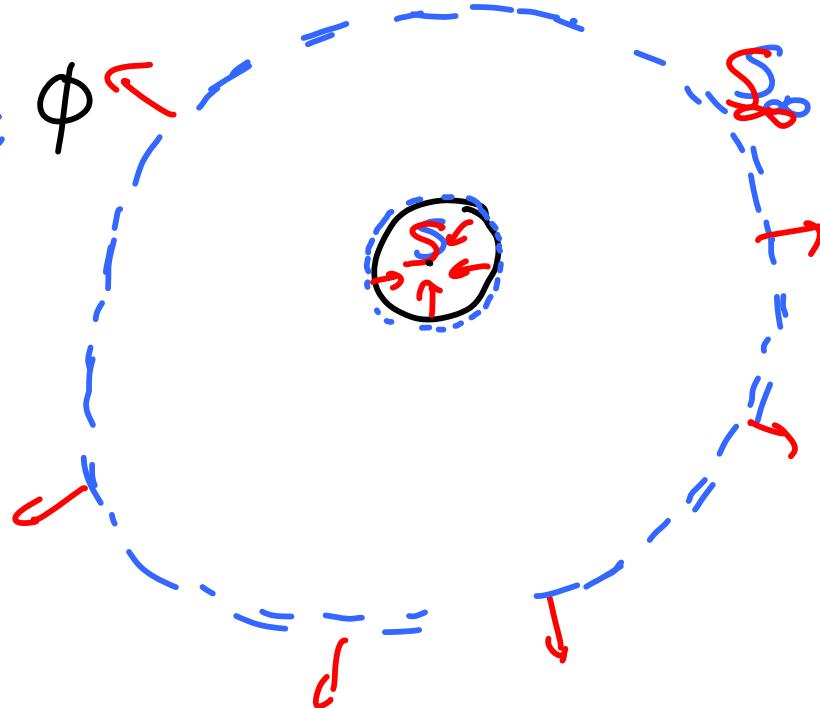
$$A = -\frac{R^3}{2} \Rightarrow \phi = -\frac{R^3}{2} \frac{U_j x_j}{r^3}; U_i = -\frac{R^3}{2} \left(\frac{\delta_{ij}}{r^3} - \frac{3x_i x_j}{r^5} \right)$$



$$U_i n_i = U_i n_i \text{ at } r=R$$

$$U_i \rightarrow 0 \text{ as } r \rightarrow \infty$$

$$\begin{aligned}
 KE &= \frac{1}{2} S \int dV u_i^2 = \frac{1}{2} S \int ds u_i n_i \phi \\
 &\quad \checkmark \\
 &= \frac{1}{2} S \int_{S_\infty} ds u_i n_i \phi + \\
 &\quad \text{---} \\
 &\quad \frac{1}{2} S \int_S ds u_i \left(-\frac{x_i}{r} \right) \phi \\
 &= -\frac{1}{2} S \int_S ds u_i \frac{x_i}{r} \phi \\
 &= -\frac{1}{2} S \int_S ds \frac{U_i x_i}{r} \phi \\
 &= -\frac{1}{2} S \int_S ds \frac{U_i x_i}{r} \left(-\frac{R^3}{2} \frac{\vec{U}_i \cdot \vec{x}_j}{r^3} \right) \\
 &= \frac{S U_i U_j}{4 R} \int_S ds x_i x_j = \frac{1}{2} M_a \bar{U_i}^2
 \end{aligned}$$



$$M_a = \left(\frac{2}{3} \pi R^3 S \right)$$

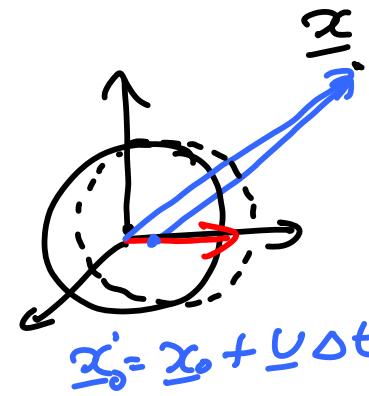
$$f_i = T_{ij} n_j = -\rho \delta_{ij} n_j = -\rho n_i$$

$$F_i = \int ds (-\rho n_i)$$

$$\rho + \frac{1}{2} \rho u_i^2 + \rho \frac{\partial \phi}{\partial t} + u_i = p_0$$

$$\rho = p_0 - \frac{1}{2} \rho u_i^2 - \rho \frac{\partial \phi}{\partial t}$$

$$\rho = p_0 - \frac{1}{2} \rho u_i^2 - \underbrace{\frac{\rho R^3 x_i}{2r^3} \frac{du_i}{dt}}_{\text{dashed}} + \rho u_i u_j$$



$$\phi = -\frac{R^3}{2} \frac{u_i x_i}{r^3}$$

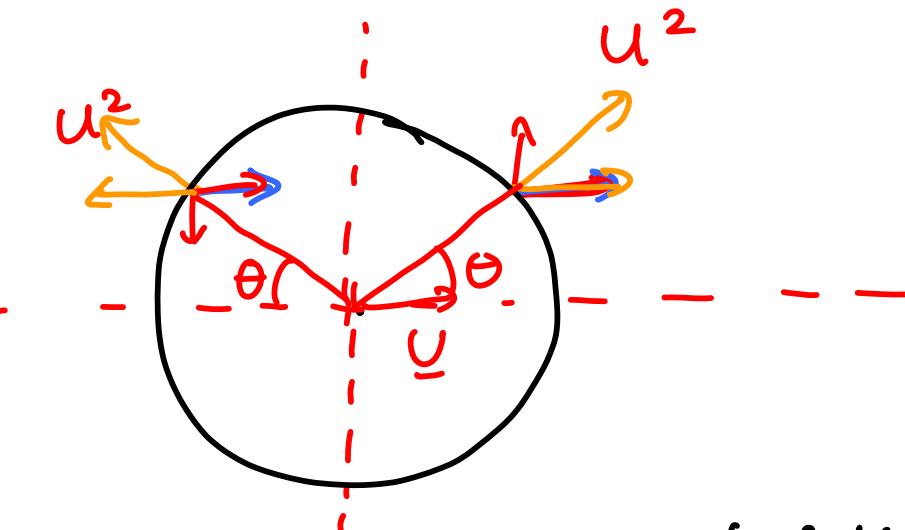
$$\frac{\partial \phi}{\partial t} = -\frac{R^3 x_i}{2r^3} \frac{du_i}{dt} - \frac{u_i u_i}{r^3}$$

For steady flow

$$\rho = p_0 - \frac{1}{2} \rho u_i^2 + \rho u_i u_j$$

$$F_i = \int ds n_i \left[p_0 - \frac{1}{2} \rho u_j^2 + \rho u_j u_j \right]$$

$F_i = 0$ 'd'Alembert's paradox'



$$F_i = \int dS n_i (-b) = \int dS n_i S \left[\frac{R^3}{2} \frac{dU_j}{dt} \frac{x_i}{r^3} \right]$$

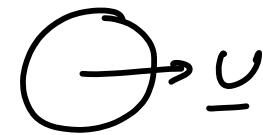
$$= \frac{S}{2} \frac{dU_j}{dt} \int dS \frac{x_i}{r} x_j$$

$$= M_a \frac{dU_j}{dt}$$

$$\text{where } M_a = \left(\frac{2}{3} \pi R^3 S \right)$$

Potential flow:

$$u_i = \frac{\partial \phi}{\partial x_i}$$



$$\frac{\partial u_i}{\partial x_i} = 0 \Rightarrow \nabla^2 \phi = 0$$

$$p + \frac{1}{2} \rho u_i^2 + \rho \frac{\partial \phi}{\partial t} = p_0$$

$$\left. \begin{aligned} F_i &= M_a \frac{d u_i}{d t} \\ K.E. &= \frac{1}{2} M_a u_i^2 \end{aligned} \right\} M_a = \rho \left(\frac{2}{3} \pi R^3 \right)$$

$$F_i = \int ds (-p n_i)$$

$$= - \int ds \left(p_0 - \frac{1}{2} \rho u_j^2 - \rho \frac{\partial \phi}{\partial t} \right) n_i$$

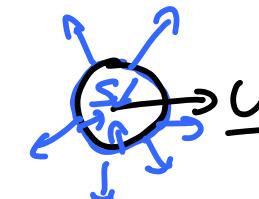
$$= - \int ds \left(p_0 - \frac{1}{2} \rho u_j^2 + \rho u_j n_j \right) n_i$$

$$= \int ds \left(\frac{1}{2} \rho u_j^2 - \rho u_i u_j \right) \underline{n_i}$$

$$\int dV \frac{\partial}{\partial x_i} \left(\frac{\rho u_j^2}{2} - \rho u_i u_j \right) = \int_{S_\infty} ds n_i \left(\frac{\rho u_j^2}{2} - \rho u_i u_j \right) - \int_{S_\infty} \underline{n_i} \left(\frac{\rho u_i^2}{2} - \rho u_i u_j \right)$$

$$= \int_{S_\infty} ds n_i \left(\frac{\rho u_j^2}{2} - \rho u_i u_j \right) - F_i$$

$$F_i = \int_{S_\infty} ds n_i \left(\frac{\rho u_i^2}{2} - \rho u_i u_j \right) - \int dV \frac{\partial}{\partial x_i} \left(\frac{\rho u_i^2}{2} - \rho u_i u_j \right)$$



S_∞

$$= \int_{S_\infty} dS n_i \left(\frac{8u_j^2}{2} - 8u_j u_i \right) - \int dV \left[8u_j \frac{\partial u_i}{\partial x_j} - 8u_j \frac{\partial u_i}{\partial x_i} \right]$$

$$F_i = \int_{S_\infty} dS n_i \left(\frac{8u_j^2}{2} - 8u_j u_i \right) - \int dV \left[8u_j \frac{\partial u_i}{\partial x_j} - 8u_j \frac{\partial u_i}{\partial x_i} \right]$$

$$8u_j \frac{\partial u_i}{\partial x_j} \equiv 8 \frac{\partial}{\partial x_j} (u_i u_j) - 8u_i \cancel{\frac{\partial u_j}{\partial x_j}}$$

$$8u_j \frac{\partial u_i}{\partial x_i} \equiv 8 \frac{\partial}{\partial x_i} (u_i u_j)$$

$$F_i = \int_{S_\infty} dS \left[n_i \left(\frac{8u_j^2}{2} - 8u_j u_i \right) \right] - \int dV \left[8 \frac{\partial}{\partial x_j} (u_i u_j) - 8 \frac{\partial}{\partial x_i} (u_i u_j) \right]$$

$$= \int_{S_\infty} dS \left[n_i \left(\frac{8u_j^2}{2} - 8u_j u_i \right) \right] - \left[\int_{S_\infty} dS n_j \left(8u_i u_j - 8u_i u_j \right) - \int_S dS n_j \left(8u_i u_j - 8u_i u_j \right) \right]$$

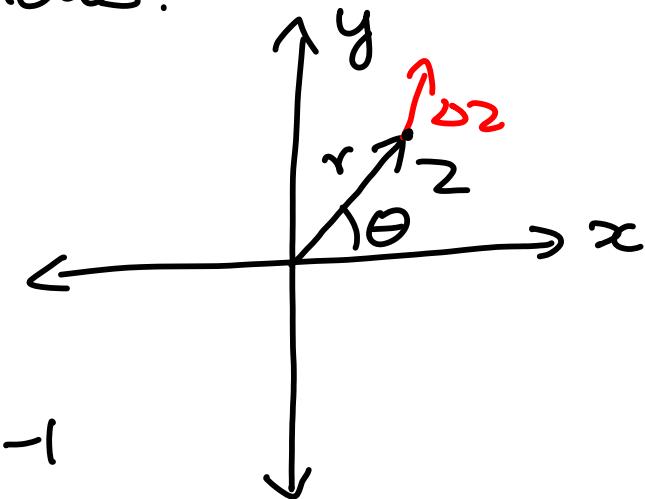
$$F_i = \int_{S_\infty} ds n_i \left(\frac{8u_i^2}{2} - 8u_i U_0 \right) - \int_{S_\infty} ds n_j (8u_i u_j - 8u_i U_j) + \int_S ds (8u_i) (n_j u_j - n_j U_j)$$

Two-dimensional potential flows:

$$\nabla^2 \phi = 0 \quad \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = 0$$

$$z = x + iy = re^{i\theta}$$

$$e^{i\theta} = \cos \theta + i \sin \theta$$



$$i^2 = -1$$

$$F(z) = \underbrace{\phi(x,y)}_{---} + i \underbrace{\psi(x,y)}_{---}$$

Analytic function:

$$F(z + \Delta z) - F(z) = \Delta F = \left(\frac{dF}{dz} \right) \underline{\Delta z} = \frac{dF}{dz}(dx + idy)$$

$$\Delta F = \Delta x \left(\frac{\partial \phi}{\partial x} + i \frac{\partial \psi}{\partial x} \right) + \Delta y \left(\frac{\partial \phi}{\partial y} + i \frac{\partial \psi}{\partial y} \right)$$

$$= \Delta x \left(\frac{\partial \phi}{\partial x} + i \frac{\partial \psi}{\partial x} \right) + \underline{i \Delta y} \left(\underline{-i \frac{\partial \phi}{\partial y}} + \frac{\partial \psi}{\partial y} \right)$$

$$\frac{\partial}{\partial y} \left[\frac{\partial \Phi}{\partial x} = \frac{\partial \Psi}{\partial y} \right] \quad \text{For the potential flow}$$

$$\frac{\partial}{\partial x} \left[\frac{\partial \Phi}{\partial y} = -\frac{\partial \Psi}{\partial x} \right] \quad F = \Phi(x, y) + i\Psi(x, y)$$

Potential function = Φ

$$\frac{\partial^2 \Phi}{\partial x^2} + \frac{\partial^2 \Phi}{\partial y^2} = 0 \quad u_x = \frac{\partial \Phi}{\partial x} \quad u_y = \frac{\partial \Phi}{\partial y}$$

$$\frac{\partial^2 \Psi}{\partial x^2} + \frac{\partial^2 \Psi}{\partial y^2} = 0$$

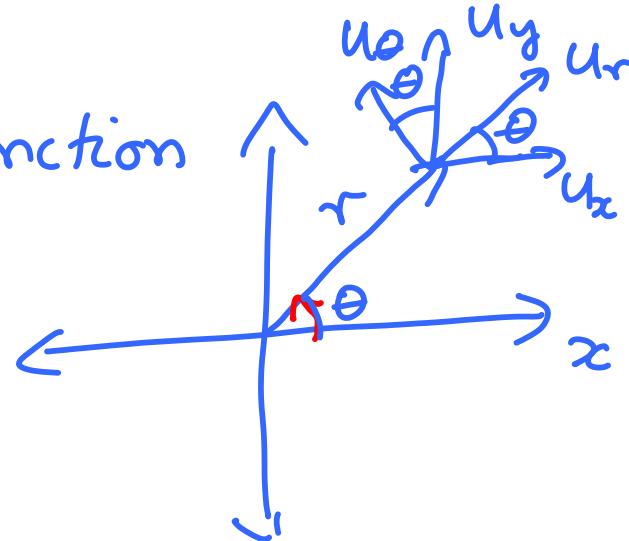
$$\Delta F = (\Delta x + i\Delta y) \left(\frac{\partial \Phi}{\partial x} + i \frac{\partial \Psi}{\partial x} \right)$$

$$\Delta F = \Delta z \left(\frac{\partial \Phi}{\partial x} - i \frac{\partial \Psi}{\partial y} \right) = \Delta z (u_x - i u_y)$$

$$W = \frac{dF}{dz} = u_x - i u_y$$

$$\left. \begin{aligned} \frac{\partial \Phi}{\partial x} &= u_x = \frac{\partial \Psi}{\partial y} \\ \frac{\partial \Phi}{\partial y} &= u_y = -\frac{\partial \Psi}{\partial x} \end{aligned} \right\}$$

Ψ = Stream function



$$F(z) = \phi(x, y) + i \psi(x, y)$$

$$\frac{dF}{dz} = u_x - i u_y = w$$

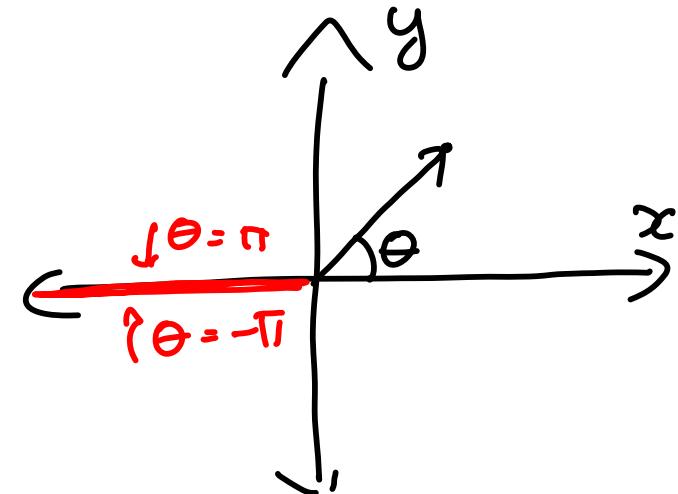
$$u_x = u_r \cos \theta - u_\theta \sin \theta$$

$$u_y = u_r \sin \theta + u_\theta \cos \theta$$

$$\begin{aligned} \frac{dF}{dz} &= (u_r \cos \theta - u_\theta \sin \theta) - i(u_r \sin \theta + u_\theta \cos \theta) \\ &= (u_r - i u_\theta)(\cos \theta - i \sin \theta) = (u_r - i u_\theta)e^{-i\theta} \end{aligned}$$

$$F(z) = \phi(x,y) + i\psi(x,y)$$

$$\begin{aligned} W &= \frac{dF}{dz} = u_x - iu_y \\ &= (u_r - iu_\theta) e^{-i\theta} \end{aligned}$$



$F(z)$ which are analytic?

$$\theta \rightarrow \theta + 2\pi$$

$$= z, z^2, \dots, z^n, e^z, \sin z, \cos z,$$

$$\dots, \frac{1}{z}, \frac{1}{z^2}, \dots$$

$$\begin{aligned} z &= x+iy \\ \bar{z} &= x-iy \end{aligned}$$

$\log z$

$$\begin{aligned} F(z) &= \log(z) = \log(re^{i\theta}) \\ &= \log r + i\theta \end{aligned}$$

Potential flow:

Inviscid

Irrational $\underline{\omega} = \nabla \times \underline{u} = 0$

$$\underline{u} = \nabla \phi \quad T_{ij} = -\rho \delta_{ij}$$

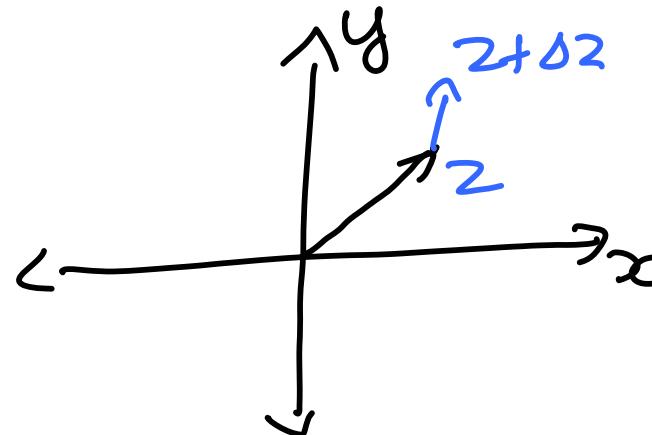
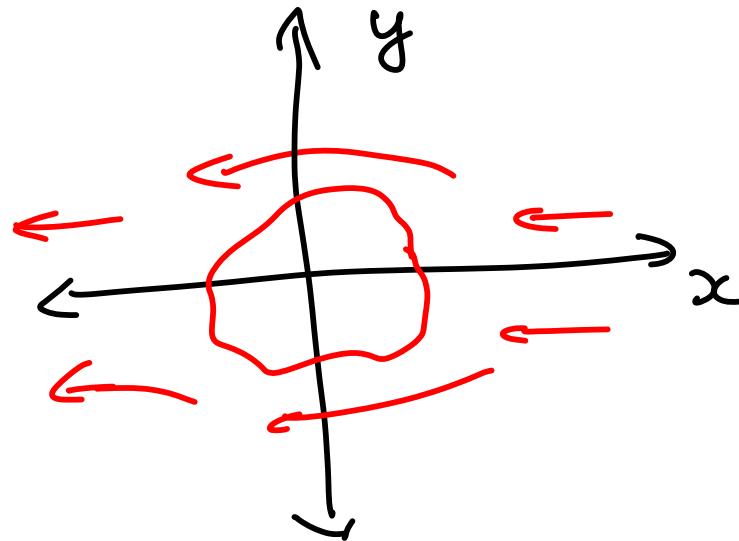
$$\nabla \cdot \underline{u} = 0 \Rightarrow \nabla^2 \phi = 0$$

$$\rho \left(\frac{\partial \underline{u}}{\partial t} + \underline{u} \cdot \nabla \underline{u} \right) = -\nabla p + \underline{f} \quad \underline{f} = -\nabla V$$

$$\nabla \left(p + \frac{1}{2} \rho u^2 + \rho \frac{\partial \phi}{\partial t} \right) = 0$$

$$p + \frac{1}{2} \rho u^2 + \rho \frac{\partial \phi}{\partial t} = p_0$$

Two dimensional potential flow:



$F(z)$ is analytic if

$$\lim_{\delta z \rightarrow 0} F(z + \delta z) - F(z) = \frac{dF}{dz}|_{z=z}$$

$\delta z \rightarrow 0$

$$F(z) = \underline{\phi(x,y)} + i \psi(x,y)$$

$$\begin{aligned}\frac{\partial \phi}{\partial x} &= \frac{\partial \psi}{\partial y} \\ \frac{\partial \phi}{\partial y} &= -\frac{\partial \psi}{\partial x}\end{aligned} \Rightarrow \begin{aligned}\nabla^2 \phi &= 0 \\ \nabla^2 \psi &= 0\end{aligned}$$

$F = \text{Complex Potential} = \phi + i\psi$

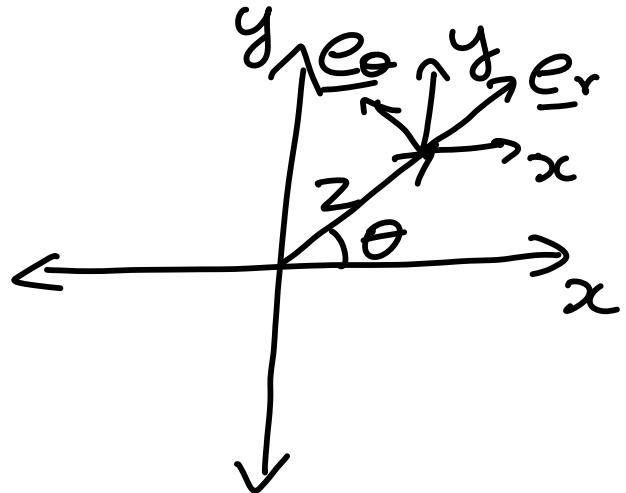
$\phi = \text{Velocity potential}$

$$u_x = \frac{\partial \phi}{\partial x} = \frac{\partial \psi}{\partial y} \quad u_y = \frac{\partial \phi}{\partial y} = -\frac{\partial \psi}{\partial x}$$

$\psi = \text{Stream function}$

$$\omega = \frac{dF}{dz} = u_x - iu_y = (u_r - iu_\theta)e^{-i\theta}$$

$$z = re^{i\theta} = x + iy$$



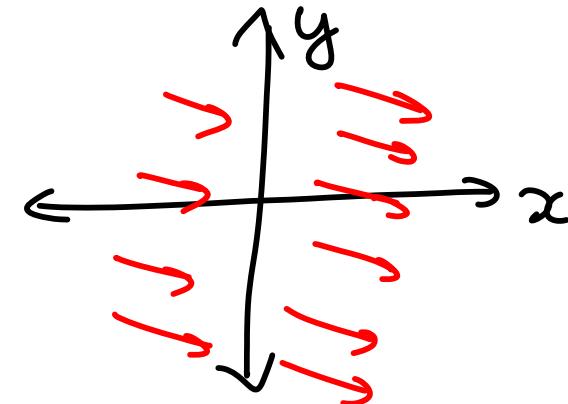
$$F = U z \quad W = U = (U_x - iU_y)$$

$$U_x = U, \quad U_y = 0$$

$$= U e^{i\alpha} z \quad W = U e^{i\alpha} \\ = U(\cos \alpha + i \sin \alpha)$$

$$= U_x - iU_y$$

$$U_x = U \cos \alpha \quad U_y = -U \sin \alpha$$



$$F = Az^2 \Rightarrow w = 2Az = u_x - iu_y$$

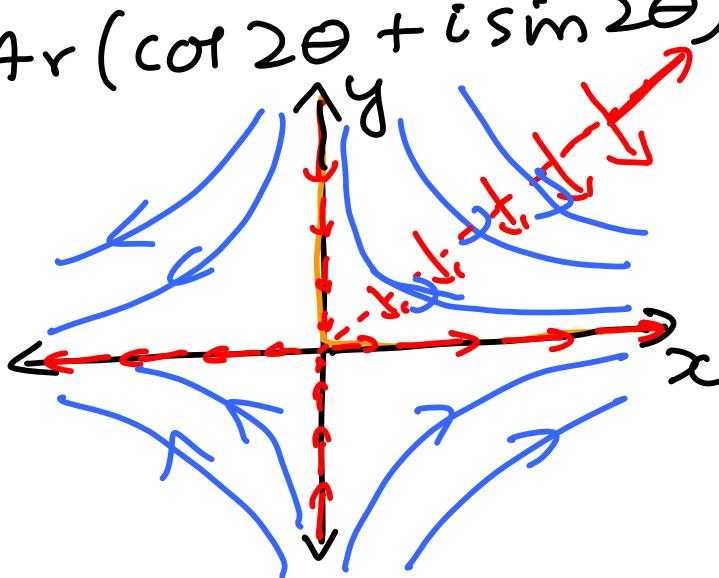
$$= 2Ar e^{i\theta} = (u_r - iu_\theta) e^{-i\theta}$$

$$u_r - iu_\theta = 2Ar e^{2i\theta}$$

$$= 2Ar (\cos 2\theta + i \sin 2\theta)$$

$$u_r = 2Ar \cos 2\theta$$

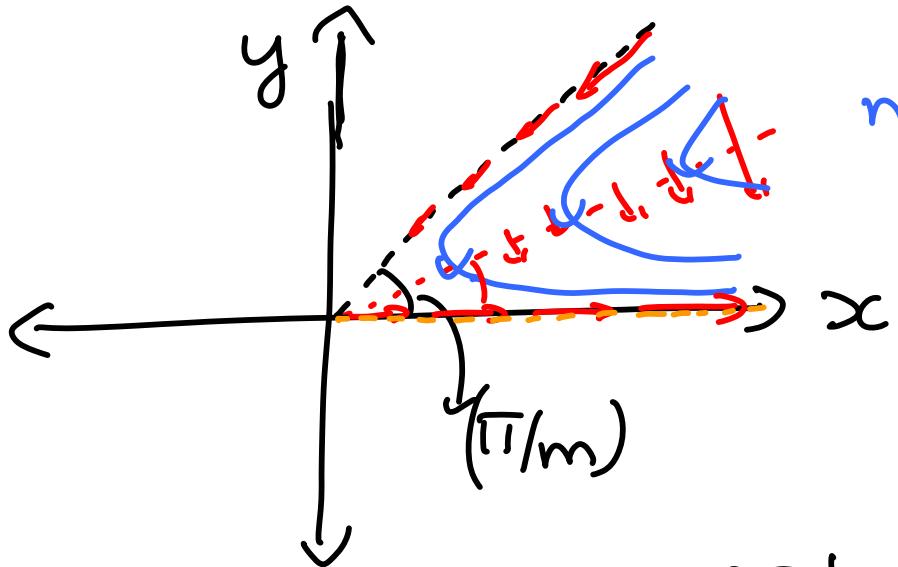
$$u_\theta = -2Ar \sin 2\theta$$



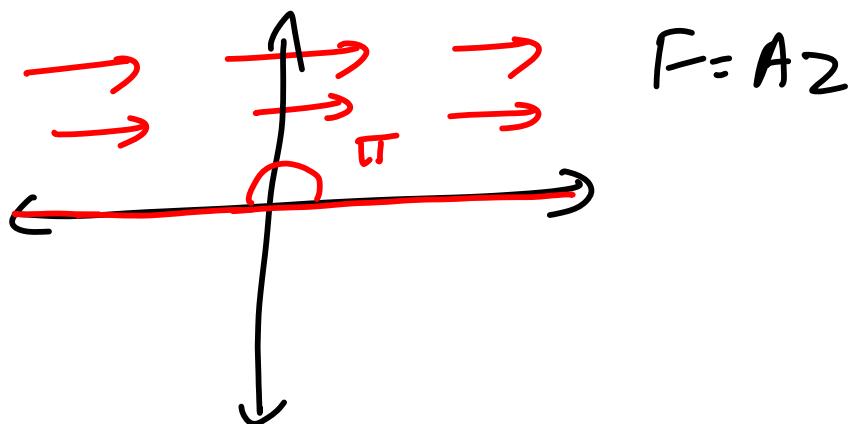
$$F = A \dot{z}^m \quad W = \frac{dF}{dz} = m A z^{m-1} = m A r^{m-1} e^{i(m-1)\theta}$$

$$m A r^{m-1} e^{i(m-1)\theta} = (u_r - i u_\theta) e^{-i\theta} \quad \left| \begin{array}{l} u_r = m A r^{m-1} \cos(m\theta) \\ u_\theta = -m A r^{m-1} \sin(m\theta) \end{array} \right.$$

$$m A r^{m-1} e^{im\theta} = u_r - i u_\theta$$

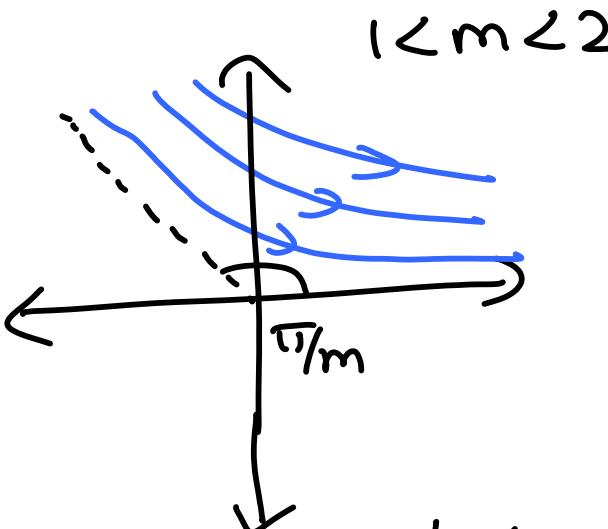


$$m > 2$$

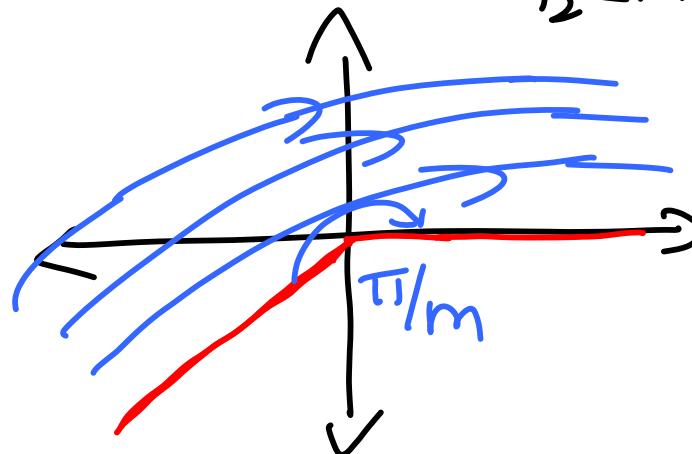


$$m = 1$$

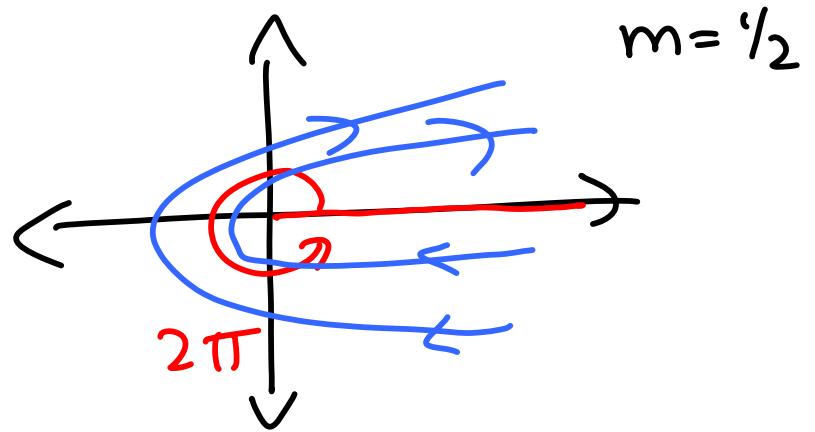
$$F = A z$$



$$1 < m < 2$$

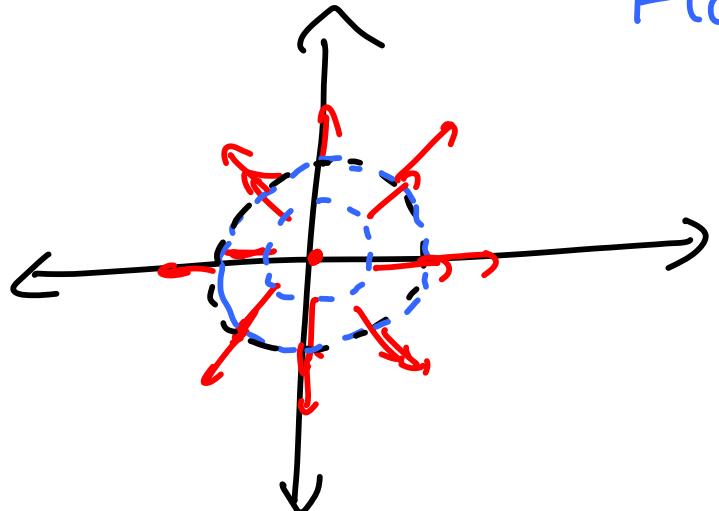


$$0 < m < 1$$



$$F = \frac{m}{2\pi} \log 2 \quad W = \frac{m}{2\pi r} = \left(\frac{m}{2\pi r}\right) e^{-i\theta} = (u_r - i u_\theta) e^{-i\theta}$$

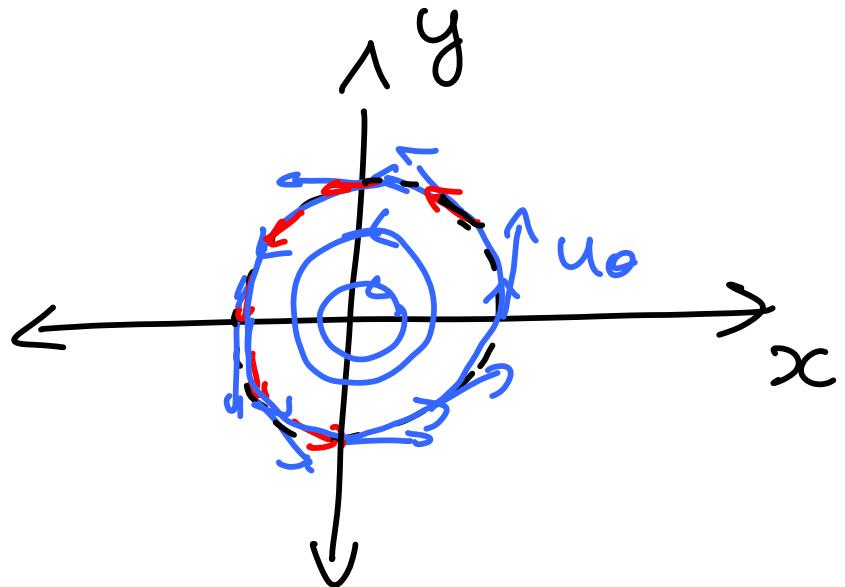
$$u_r = \frac{m}{2\pi r} \quad u_\theta = 0 \quad \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) = 0$$



$$\begin{aligned} \text{Flux} &= \int dS u_r \\ &= \int_0^{2\pi} r d\theta \left(\frac{m}{2\pi r} \right) \\ &= m \end{aligned}$$

$$F = -\frac{i\Gamma}{2\pi} \log z \Rightarrow w = -\frac{i\Gamma}{2\pi z} = \frac{-i\Gamma}{2\pi r} e^{-i\theta} = (u_r - iu_\theta) e^{-i\theta}$$

$$u_r = 0; u_\theta = \frac{\Gamma}{2\pi r} \quad \text{Circulation} = \oint d\mathbf{x} \cdot \mathbf{u}$$



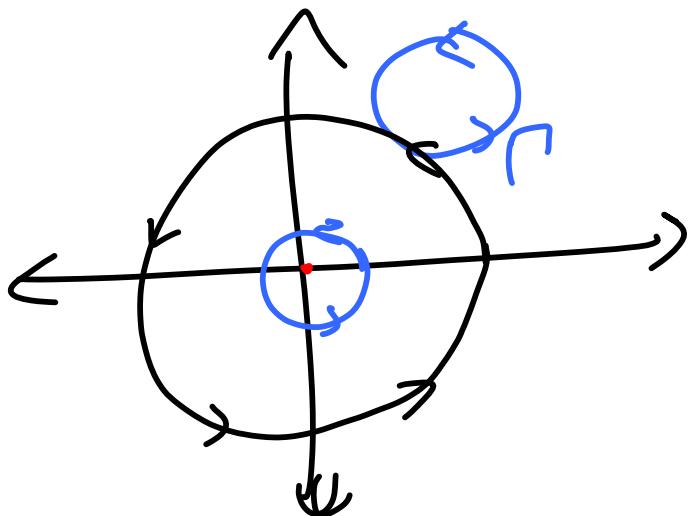
'Line vortex'

$$= \oint (r d\theta) u_\theta$$

$$= \oint r d\theta \frac{\Gamma}{2\pi r} = \Gamma$$

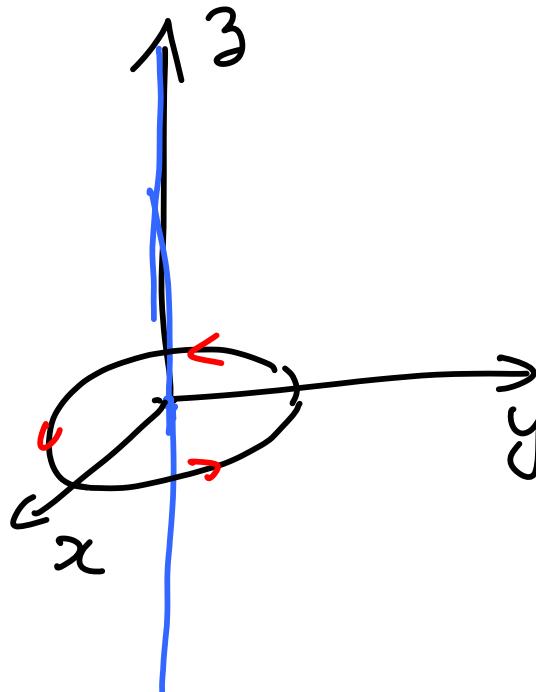
$$\int d\mathbf{s} \, \underline{n} \cdot (\nabla \times \underline{A}) = \oint d\underline{x} \cdot \underline{A}$$

$$\int d\mathbf{s} \, \underline{n} \cdot \underline{\omega} = \oint d\underline{x} \cdot \underline{\omega} = \Gamma$$



$$\underline{\omega} = r \delta(\underline{x}) \quad \omega_\theta = \frac{\Gamma}{2\pi r}$$

$$F(z) = -\frac{i}{2\pi} \Gamma \log z$$



Two-dimensional potential flows:

$$F(z) = \phi(x, y) + i\psi(x, y)$$

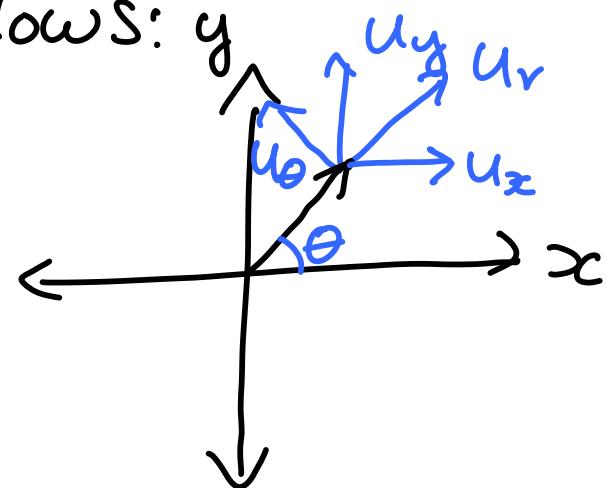
'Analytic' $\Delta F = \left(\frac{dF}{dz}\right) \Delta z$

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = 0$$

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = 0$$

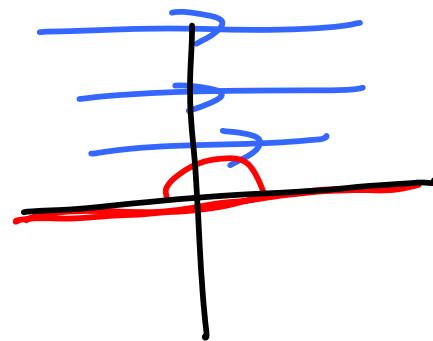
ϕ = Velocity potential ψ = Stream fn.

$$W(z) = \frac{dF}{dz} = u_x - iu_y$$
$$= (u_r - iu_\theta) e^{-i\theta}$$

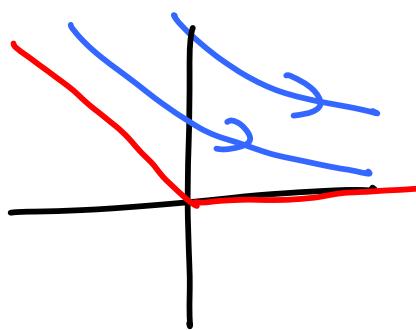


$$F = A \cdot 2^n$$

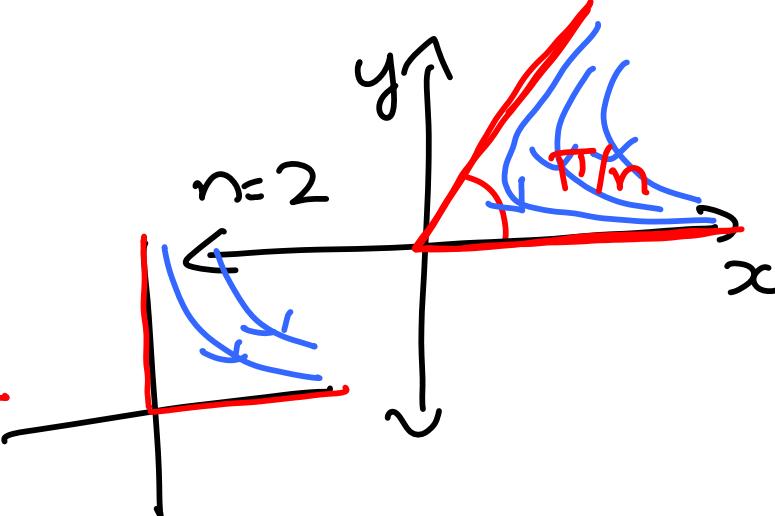
$n=1$



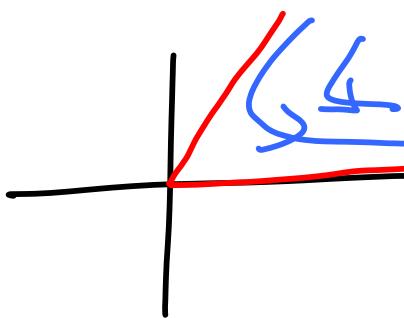
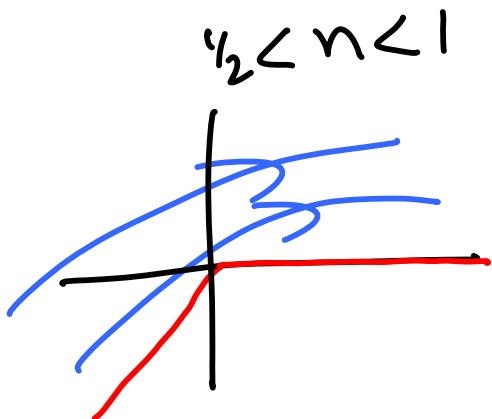
$1 < n < 2$



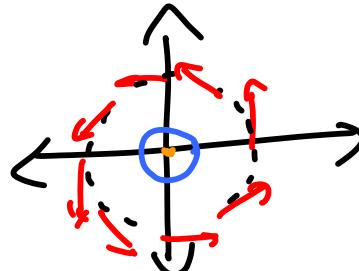
$n=2$



$n > 2$



$$\int_S d\mathbf{s} \cdot \underline{n} \cdot (\nabla \times \underline{u}) = \oint_C d\underline{x} \cdot \underline{u}$$

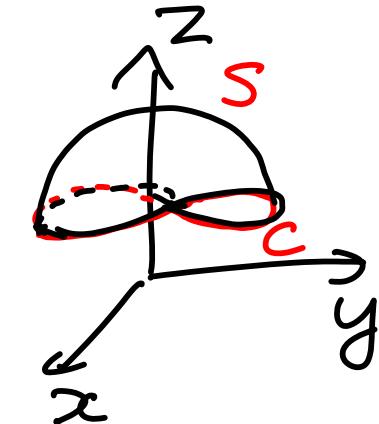


$$\int_S d\mathbf{s} \cdot \underline{n} \cdot \underline{w} = \oint_C d\underline{x} \cdot \underline{u}$$

$$\frac{\int_S d\mathbf{s} \omega_2}{\dots} = \Gamma$$

$$\underline{\omega}_2 = \Gamma \delta(\underline{x})$$

$$\int_S d\mathbf{s} \delta(z) = 1$$



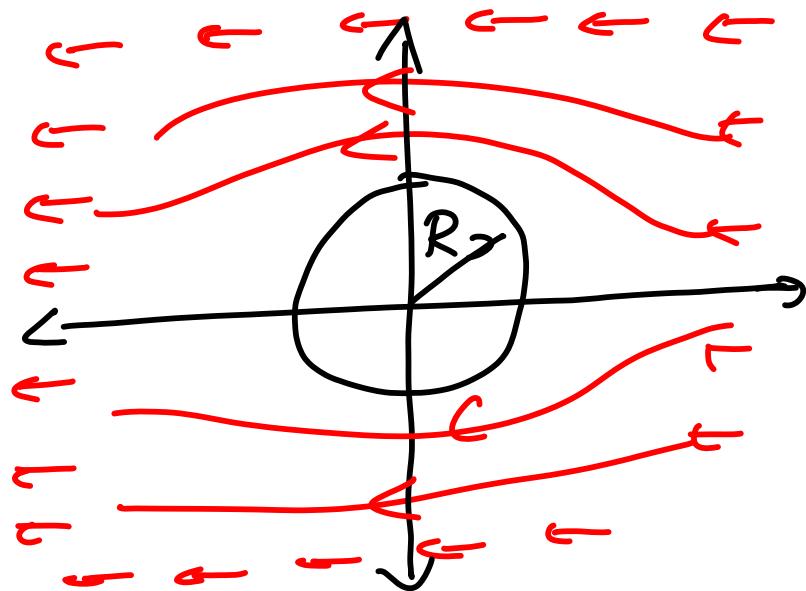
$$\left\{ \begin{array}{l} F(z) = \frac{-i\Gamma}{2\pi} \log z \\ \underline{\omega} = -\frac{i\Gamma}{2\pi z} \end{array} \right.$$

$$u_r = 0 \quad u_\theta = \frac{\Gamma}{2\pi r}$$

$$\Gamma = \oint_C d\underline{x} \cdot \underline{u}$$

$$F = -U_2 - \frac{UR^2}{z} - \frac{i\Gamma}{2\pi} \log z$$

$$\begin{aligned} w &= \left[U + \frac{UR^2}{z^2} - \frac{i\Gamma}{2\pi z} \right] \\ &= \left[-U + \frac{UR^2}{r^2} e^{-2i\theta} - \frac{i\Gamma}{2\pi r} e^{-i\theta} \right] \\ &= \left[-Ue^{i\theta} + \frac{UR^2}{r^2} e^{-i\theta} - \frac{i\Gamma}{2\pi r} \right] e^{-i\theta} \end{aligned}$$



$$\underline{y} \cdot \underline{y} = \underline{v} \cdot \underline{v} = 0 \quad \text{at } r=R$$

$$u_r = -U \cos \theta + \frac{UR^2}{r^2} \cos \theta = U \cos \theta \left[-1 + \frac{R^2}{r^2} \right]$$

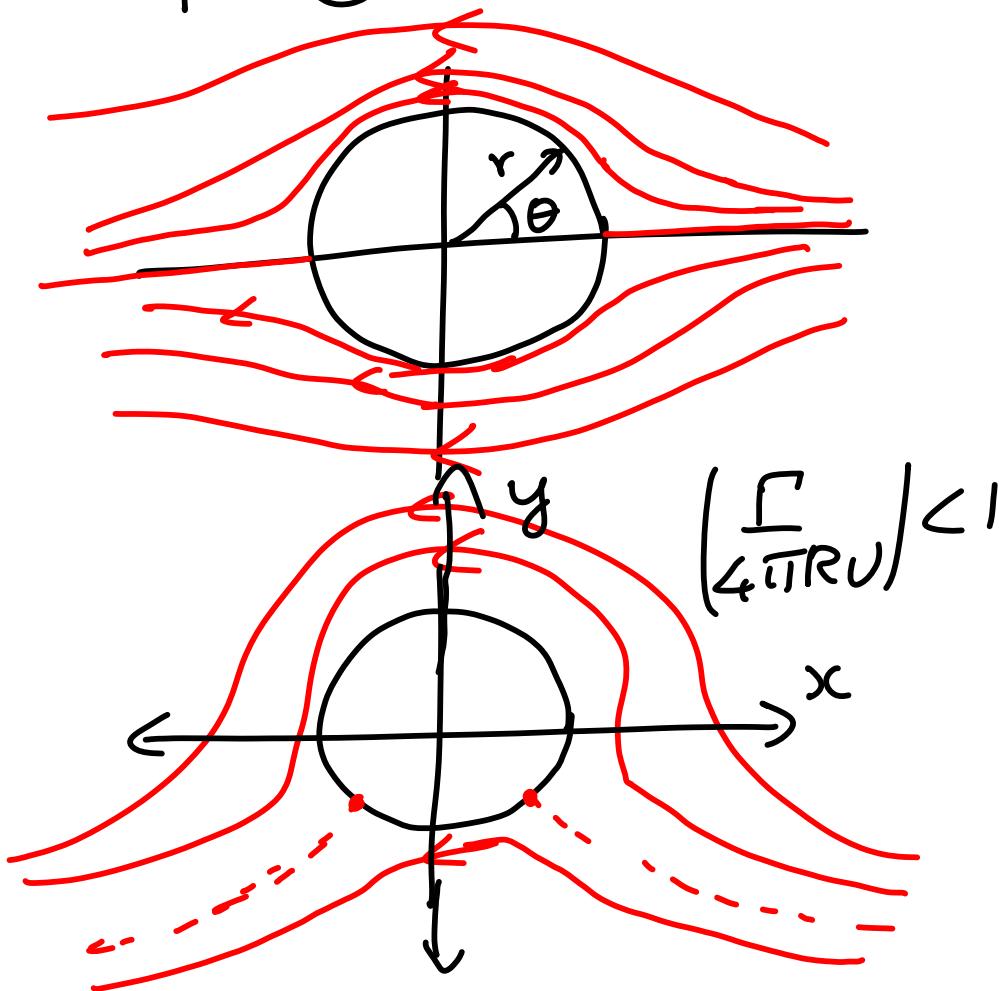
$$u_\theta = +U \sin \theta + \frac{UR^2}{r^2} \sin \theta + \frac{\Gamma}{2\pi r}$$

$$\text{At } r=R, u_r=0, \quad u_\theta = 2U \sin \theta + \frac{\Gamma}{2\pi r}$$

Flow around a cylinder:

$$U_r = U \cot \theta \left[-1 + \frac{R^2}{r^2} \right] \quad U_\theta = U \sin \theta \left[1 + \frac{R^2}{r^2} \right] + \frac{\Gamma}{2\pi r}$$

$$\Gamma = 0$$



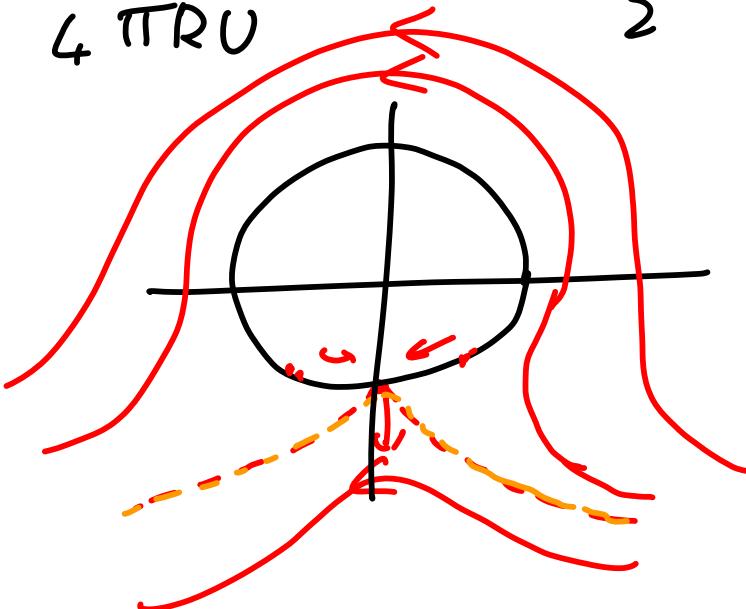
$$\text{At } r=R, U_\theta = 2U \sin \theta + \frac{\Gamma}{2\pi R}$$

$$\sin \theta = -\frac{\Gamma}{4\pi R U}$$

$$u_r = U \cos \theta \left[-1 + \frac{R^2}{r^2} \right]$$

$$u_\theta = U \sin \theta \left(1 + \frac{R^2}{r^2} \right) + \frac{\Gamma}{2\pi r}$$

$$\frac{\Gamma}{4\pi R U} = 1 \Rightarrow \theta = \frac{3\pi}{2}$$

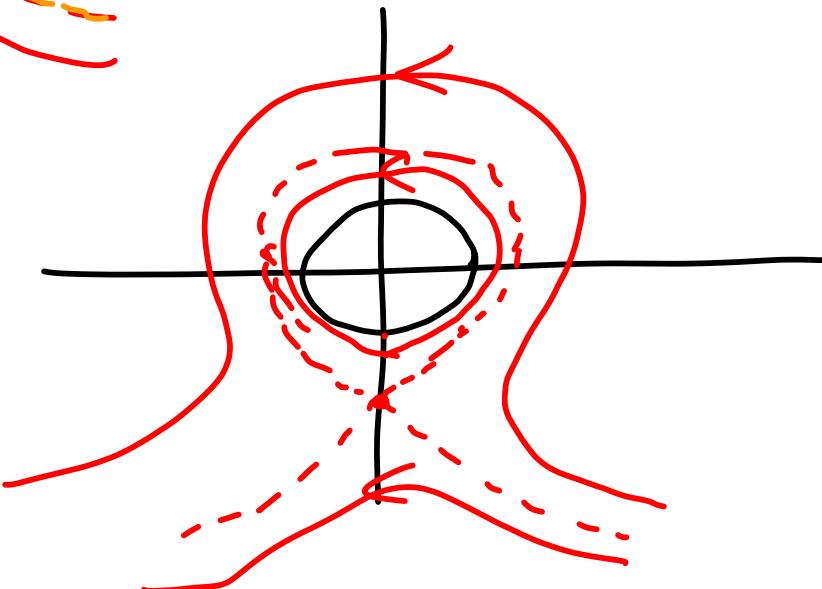


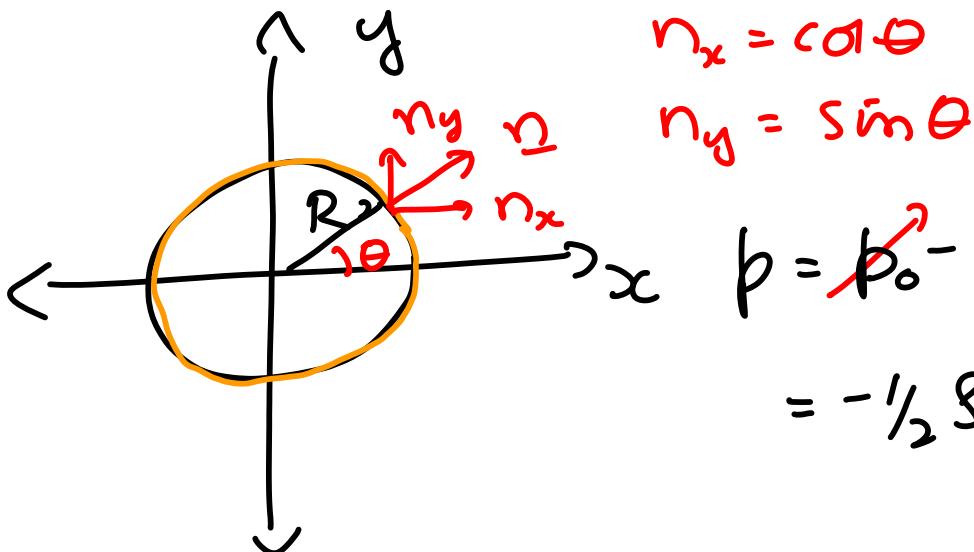
$$\frac{\Gamma}{4\pi R U} > 1$$

$$\text{At } r=R, u_\theta = 2U \sin \theta + \frac{\Gamma}{2\pi R}$$

For $\frac{\Gamma}{4\pi R U} > 1$, $\sin \theta = -1$

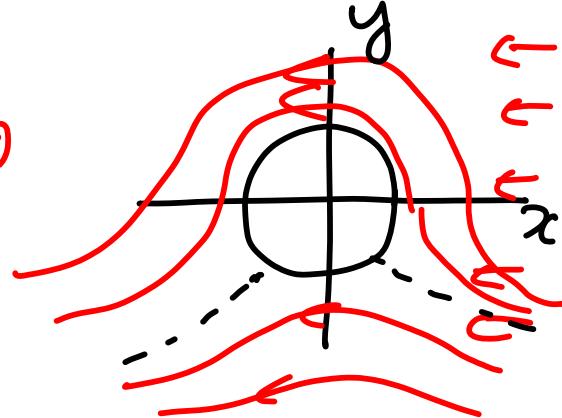
$$u_\theta = 0 \text{ at } -U \left(1 + \frac{R^2}{r^2} \right) + \frac{\Gamma}{2\pi r} = 0$$





$$p = p_0 - \frac{1}{2} \delta u^2 - \cancel{\frac{\delta \phi}{\delta t}}$$

$$= -\frac{1}{2} \delta (u_r^2 + u_\theta^2)$$



$$\text{At } r=R, u_r=0, u_\theta = 2U \sin \theta + \frac{\Gamma}{2\pi r}$$

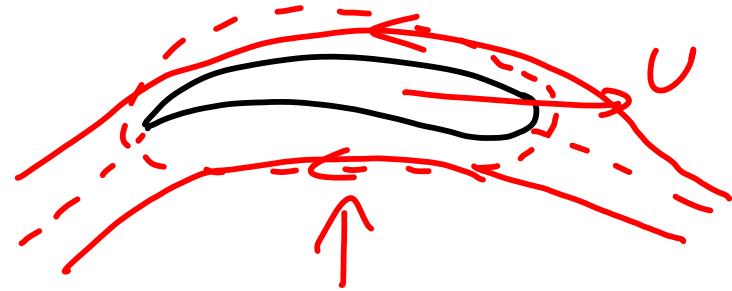
$$F_i = \int ds (-pn_i) = \int_0^{2\pi} R d\theta \left[\frac{1}{2} \delta \left(2U \sin \theta + \frac{\Gamma}{2\pi R} \right)^2 \right] n_i$$

$$= \frac{1}{2} \delta R \int d\theta \left[4U^2 \sin^2 \theta + \left(\frac{\Gamma}{2\pi R} \right)^2 + \frac{2U \sin \theta \Gamma}{\pi R} \right] n_i$$

$$F_x = \frac{1}{2} \delta R \int d\theta \left[4U^2 \sin^2 \theta + \left(\frac{\Gamma}{2\pi R} \right)^2 + \frac{2U \sin \theta \Gamma}{\pi R} \right] \cos \theta = 0$$

$$F_y = \frac{1}{2} \delta R \int_0^{2\pi} d\theta \left[4U^2 \sin^2 \theta + \left(\frac{\Gamma}{2\pi R} \right)^2 + \frac{2U \sin \theta \Gamma}{\pi R} \right] \sin \theta$$

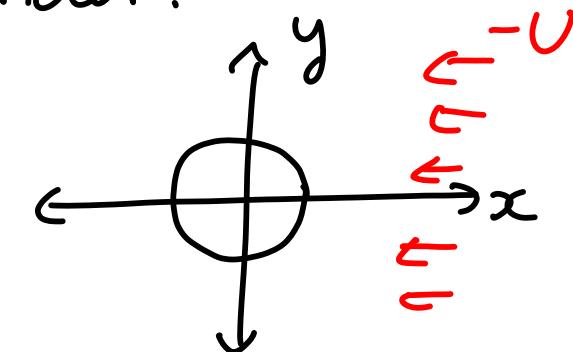
$$= 8U \Gamma \quad \text{'Lift force'}$$



$$\int d\mathbf{x} \cdot \mathbf{y} = \Gamma$$

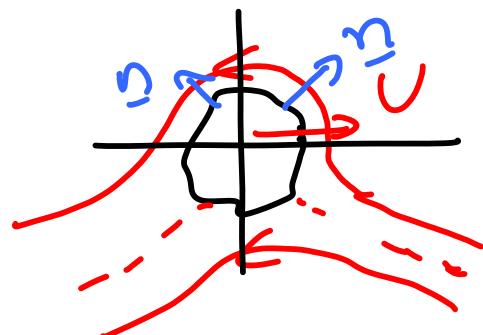
Potential flow around a cylinder:

$$F(z) = -Uz - \frac{UR^2}{2} - \frac{iR}{2\pi} \log z$$



$$F_x = 0 \quad F_y = 8UR$$

$$F(z) = -\frac{UR^2}{2} - \frac{iR}{2\pi} \log z$$



$$\oint d\zeta \cdot \underline{u} = R$$

$$\begin{aligned} p &= p_0 - \frac{1}{2} \rho u_j^2 - \rho \frac{\partial \phi}{\partial \epsilon} \\ &= p_0 - \frac{1}{2} \rho u_j^2 + \rho u_j v_j \end{aligned}$$

$$\begin{aligned} F_i &= \int ds (-bn_i) = \int ds \left(\frac{1}{2} \rho u_j^2 - \rho u_j v_j \right) n_i \\ &= \rho \int ds \left(\frac{1}{2} u_j^2 - u_j v_j \right) \underline{n}_i \end{aligned}$$

$$\oint \int dV \frac{\partial}{\partial x_i} \left(\frac{1}{2} u_j^2 - u_i \cdot u_j \right) = \oint_{S_\infty} ds n_i \left(\frac{1}{2} u_j^2 - u_i \cdot u_j \right) - \oint_{S_\infty} ds n_i \left(\frac{1}{2} u_j^2 - u_i \cdot u_j \right)$$

$n_i \cdot u_j = n_j \cdot u_i$

$$= \oint_{S_\infty} ds n_i \left(\frac{1}{2} u_j^2 - u_i \cdot u_j \right) - F_i$$

$$F_i = \oint_{S_\infty} ds n_i \left(\frac{1}{2} u_j^2 - u_i \cdot u_j \right) - \oint \int dV \frac{\partial}{\partial x_i} \left(\frac{1}{2} u_j^2 - u_i \cdot u_j \right)$$

$$- \oint \int dV \left(u_j \frac{\partial u_i}{\partial x_i} - u_j \frac{\partial u_i}{\partial x_i} \right)$$

$$- \oint \int dV \left(u_j \frac{\partial u_i}{\partial x_j} - u_i \frac{\partial u_i}{\partial x_j} \right)$$

$$- \oint \int dV \left[\frac{\partial}{\partial x_j} (u_i u_j) - u_i \frac{\partial u_j}{\partial x_j} - \frac{\partial}{\partial x_j} (u_i u_j) \right]$$

$$F_i = \oint_{S_\infty} ds n_i \left(\frac{1}{2} u_j^2 - u_i \cdot u_j \right) - \oint \int dV \frac{\partial}{\partial x_j} [u_i u_j - u_i u_j]$$

$$F_i = \oint_{S_\infty} ds n_i (\frac{1}{2} u_j^2 - u_j \cdot u_i) - \left[\oint_{S_\infty} ds n_j [u_i u_j - u_i \cdot u_j] - \oint_S ds u_i (n_j u_j - n_j u_i) \right]$$

$$= \oint_{S_\infty} ds \left[n_i (\frac{1}{2} u_j^2 - u_j \cdot u_i) - n_j (u_i u_j - u_i \cdot u_j) \right]$$

$$F(z) = -\frac{UR^2}{z} - \frac{i\Gamma}{2\pi} \log z$$

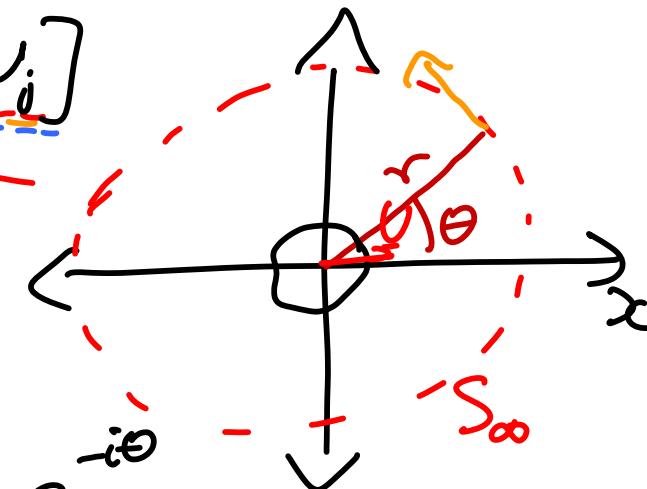
$$w = \frac{UR^2}{z^2} - \frac{i\Gamma}{2\pi z} = \frac{UR^2}{r^2} e^{-2i\theta} - \frac{i\Gamma}{2\pi r} e^{-i\theta}$$

$$u_r = \frac{UR^2}{r^2} \cos\theta \quad u_\theta = \frac{UR^2}{r^2} \sin\theta + \frac{\Gamma}{2\pi r}$$

$$F_i = \oint_{S_\infty} ds u_j (n_j u_i - n_i u_j)$$

$$F_x = 0$$

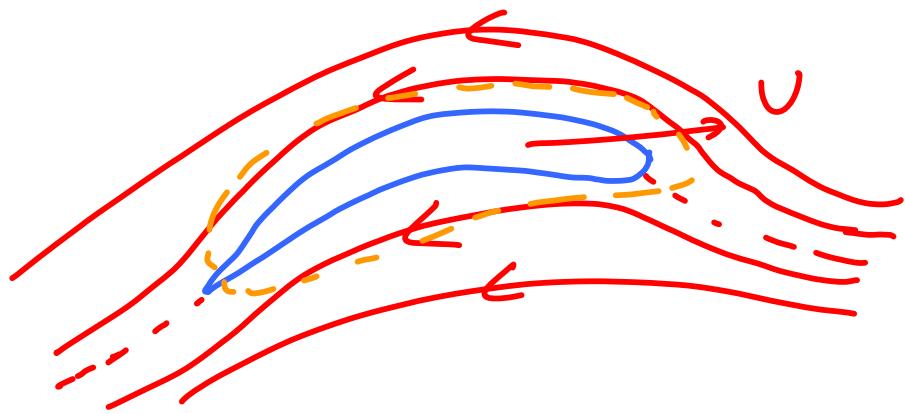
$$F_y = \oint r d\theta u_x [n_x u_y - n_y u_x]$$



$n_x = \cos\theta$
 $n_y = \sin\theta$
 $u_\theta = u \cos\theta \quad u_y = u \sin\theta$
 $u_x = -u \sin\theta$
 $u_y = u \cos\theta$

$$= \rho \int_0^{2\pi} r d\theta U_x [\cos\theta (\cos\theta u_0) - \sin\theta (-\sin\theta u_0)]$$

$$= \rho \int_0^{2\pi} r d\theta U_x \left(\frac{r}{2\pi r} \right) = \boxed{\rho U \Gamma}$$

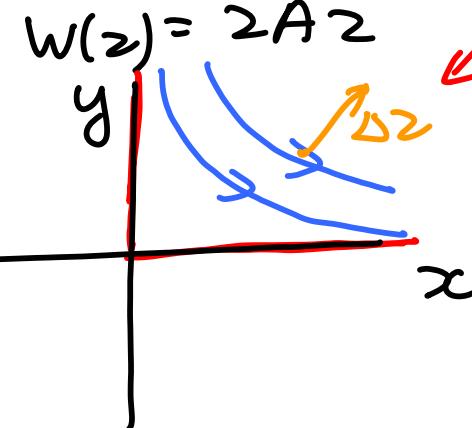
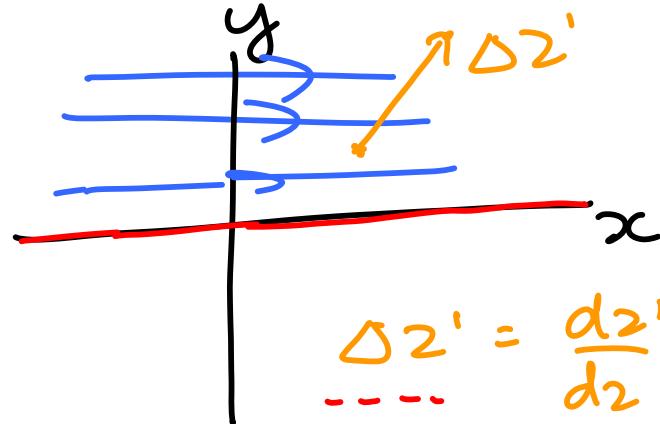


$$\oint dx \cdot y = \Gamma$$

Conformal mappings: $F(z) = Az^2$

$$z' = z^2$$

$$F(z') = Az'$$



$$\Delta z' = \frac{dz'}{dz} \Delta z$$

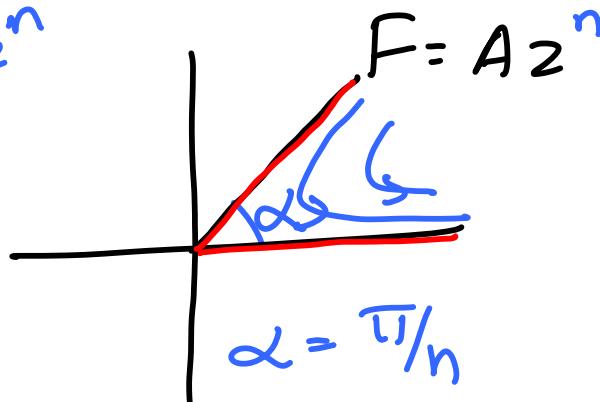
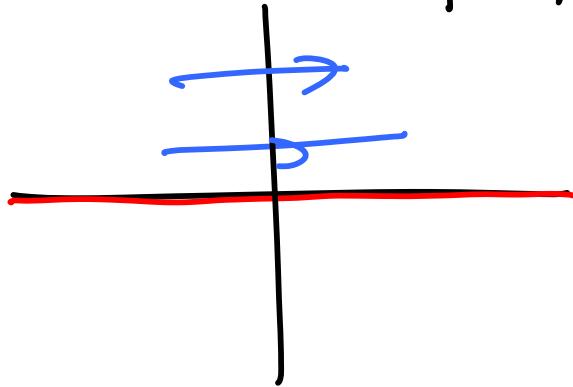
$$w(z) = \frac{dF}{dz}$$

$$w(z') = \frac{dF}{dz'} = \frac{dF}{dz} \left(\frac{dz}{dz'} \right)$$

$$\underline{w(z')} = w(z) \left(\frac{dz}{dz'} \right)$$

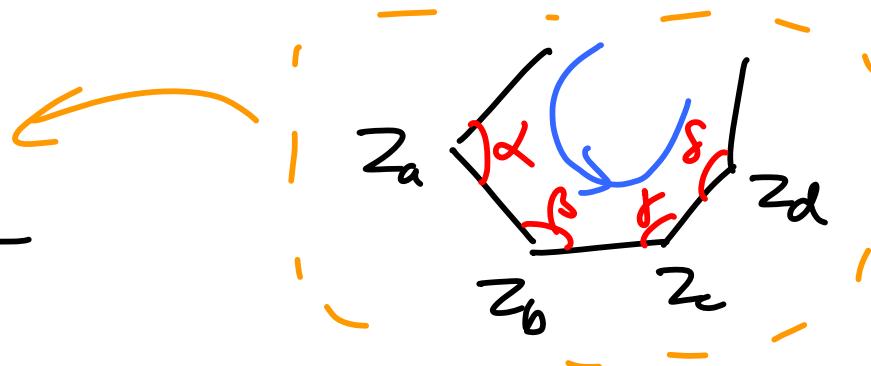
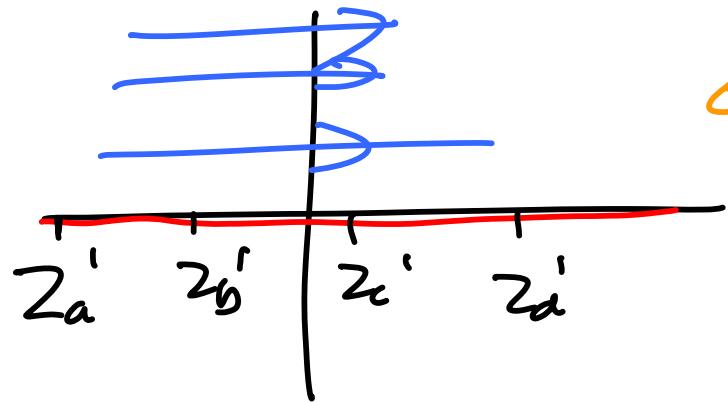
$$\Gamma = \oint dz \cdot u \quad KE = \int ds \left(\frac{1}{2} \rho u^2 \right)$$

$$F = A z' \quad z' = z^n$$



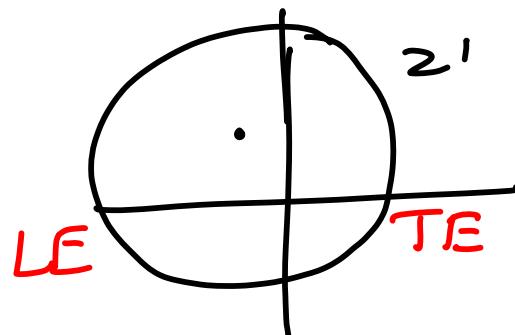
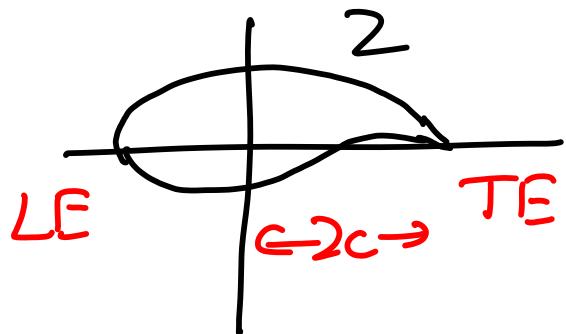
$$z' = z^n$$

$$\begin{aligned}\frac{dz'}{dz} &= n z^{n-1} \\ &= n (z')^{\frac{n-1}{n}} \\ &= n (z')^{1 - \alpha/\pi}\end{aligned}$$



$$\frac{dz'}{dz} = k \left(z' - z_a \right)^{1-\alpha/\pi} \left(z' - z_b \right)^{1-\beta/\pi} \left(z' - z_c \right)^{1-\gamma/\pi} \left(z' - z_d \right)^{1-\delta/\pi}$$

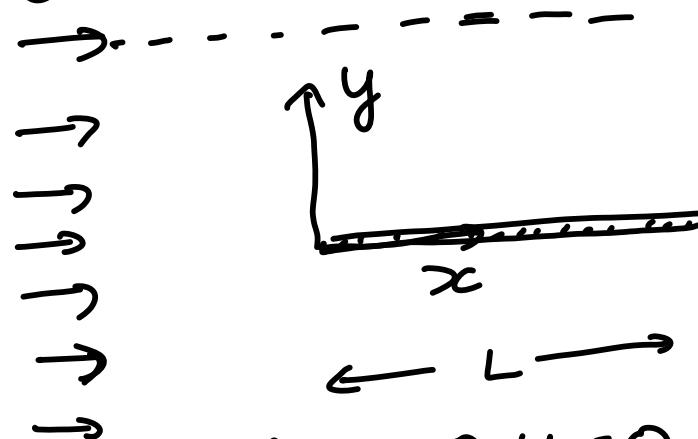
Schwarz-Christoffel transform



$$z = z' + \frac{C^2}{z'}$$

Boundary layer theory: High Reynolds number

$$\frac{\partial u_i}{\partial x_i} = 0$$



$$\cancel{\rho \left(u_j \frac{\partial u_i}{\partial x_j} \right)} = - \frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2}$$

$$\cancel{\rho \left(u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} \right)} = - \frac{\partial p}{\partial x} + \mu \left(\frac{\partial^2 u_x}{\partial x^2} + \frac{\partial^2 u_x}{\partial y^2} \right)$$

$$\rho \left(u_x \frac{\partial u_y}{\partial x} + u_y \frac{\partial u_y}{\partial y} \right) = - \frac{\partial p}{\partial y} + \mu \left(\frac{\partial^2 u_y}{\partial x^2} + \frac{\partial^2 u_y}{\partial y^2} \right)$$

At $y=0, u_x=0, u_y=0$

for $x > 0$

As $y \rightarrow \infty, u_x = U$

For $x \leq 0, u_x = U$ for all y

$$x^* = (x/L); \quad y^* = (y/L); \quad u_x^* = (u_x/U); \quad u_y^* = (u_y/U); \quad \beta^* = P/8U^2$$

$$\left(u_x^* \frac{\partial u_x^*}{\partial x^*} + u_y^* \frac{\partial u_x^*}{\partial y^*} \right) = - \frac{\partial \beta^*}{\partial x^*} + Re^{-1} \left(\frac{\partial^2 u_x^*}{\partial x^{*2}} + \frac{\partial^2 u_x^*}{\partial y^{*2}} \right)$$

$$\left(u_x^* \frac{\partial u_y^*}{\partial x^*} + u_y^* \frac{\partial u_y^*}{\partial y^*} \right) = - \frac{\partial \beta^*}{\partial y^*} + Re^{-1} \left(\frac{\partial^2 u_y^*}{\partial x^{*2}} + \frac{\partial^2 u_y^*}{\partial y^{*2}} \right)$$

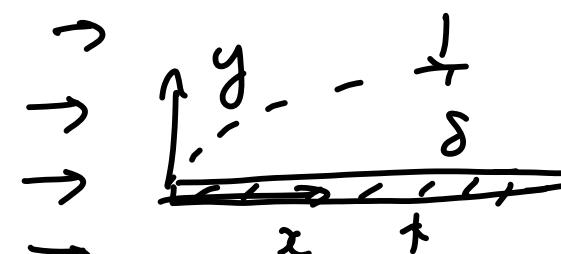
$$Re = \frac{8UL}{\mu} = \frac{UL}{\delta} \quad x_i \sim L \Rightarrow \frac{\partial}{\partial x_i} \sim \frac{1}{L}$$

$$u_j^* \frac{\partial u_i^*}{\partial x_j^*} = - \frac{\partial \beta^*}{\partial x_i^*} \quad y \sim \delta \Rightarrow \frac{\partial}{\partial y} \sim \frac{1}{\delta}$$

$$y \cdot \nabla c = 0$$

$$x^* = (x/L); \quad y^* = (y/\delta) \quad u_x^* = (u_x/U) \quad u_y^* = u_y/(U\delta/L)$$

$$p^* = (p/\rho U^2)$$

$$\rho \left(u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} \right) = - \frac{\partial p}{\partial x} + \mu \left(\frac{\partial^2 u_x}{\partial x^2} + \frac{\partial^2 u_x}{\partial y^2} \right)$$


$$\rho \left(\frac{U^2}{L} u_x^* \frac{\partial u_x^*}{\partial x^*} + \left(\frac{U\delta}{L} \right) \left(\frac{U}{\delta} \right) u_y^* \frac{\partial u_x^*}{\partial y^*} \right) = - \frac{1}{L} \frac{\partial p}{\partial x^*} + \mu \left(\frac{U}{L^2} \frac{\partial^2 u_x^*}{\partial x^{*2}} + \frac{U}{\delta^2} \frac{\partial^2 u_x^*}{\partial y^{*2}} \right)$$

$$\frac{\rho U^2}{L} \left[u_x^* \frac{\partial u_x^*}{\partial x^*} + u_y^* \frac{\partial u_x^*}{\partial y^*} \right] = - \frac{1}{L} \frac{\partial p}{\partial x^*} + \frac{\mu U}{(\delta^2)} \left[\frac{\partial^2 u_x^*}{\partial y^{*2}} + \frac{\delta^2}{L^2} \frac{\partial^2 u_x^*}{\partial x^{*2}} \right]$$

$$u_x^* \frac{\partial u_x^*}{\partial x^*} + u_y^* \frac{\partial u_x^*}{\partial y^*} = - \frac{\partial p^*}{\partial x^*} + \frac{\mu L}{\rho U \delta^2} \left[\frac{\partial^2 u_x^*}{\partial y^{*2}} + \left(\frac{\delta}{L} \right)^2 \frac{\partial^2 u_x^*}{\partial x^{*2}} \right]$$

$$\frac{\rho U \delta^2}{\mu L} = O(1) \Rightarrow \left(\frac{\rho U L}{\mu} \right) \left(\frac{\delta}{L} \right)^2 = C$$

$$\left(\frac{\delta}{L} \right) = C \operatorname{Re}^{-1/2} = \operatorname{Re}^{-1/2}$$

$$\rho \left(u_x \frac{\partial u_y}{\partial x} + u_y \frac{\partial u_y}{\partial y} \right) = - \frac{\partial p}{\partial y} + \mu \left(\frac{\partial^2 u_y}{\partial x^2} + \frac{\partial^2 u_y}{\partial y^2} \right)$$

$$u_x^* = (u_x/U); \quad u_y^* = u_y/(U\delta/L); \quad x^* = x/L; \quad y^* = y/\delta; \quad p^* = \frac{p}{SU^2}$$

$$\rho \left(U \left(\frac{U\delta}{L} \right) f_L \right) u_x^* \frac{\partial u_y^*}{\partial x^*} + \left(\frac{U\delta}{L} \right)^2 \frac{1}{\delta} u_y^* \frac{\partial u_y^*}{\partial y^*} = - \frac{SU^2}{\delta} \frac{\partial p^*}{\partial y^*}$$

$$+ \mu \left(\frac{U\delta}{L} \right) \left[\frac{1}{L^2} \frac{\partial^2 u_y^*}{\partial x^{*2}} + \frac{1}{\delta^2} \frac{\partial^2 u_y^*}{\partial y^{*2}} \right]$$

$$\frac{SU^2\delta}{L^2} \left(u_x^* \frac{\partial u_y^*}{\partial x^*} + u_y^* \frac{\partial u_y^*}{\partial y^*} \right) = - \boxed{\frac{SU^2}{\delta} \frac{\partial p^*}{\partial y^*}}$$

$$+ \mu \left(\frac{U\delta}{L} \right) \left(\frac{1}{\delta^2} \right) \left[\frac{\partial^2 u_y^*}{\partial y^{*2}} + \boxed{\left(\frac{\delta}{L} \right)^2 \frac{\partial^2 u_y^*}{\partial x^{*2}}} \right]$$

$$\boxed{\left(\frac{\delta^2}{L^2} \right)} \left[u_x^* \frac{\partial u_y^*}{\partial x^*} + u_y^* \frac{\partial u_y^*}{\partial y^*} \right] = - \frac{\partial p^*}{\partial y^*} + \boxed{\left(\frac{\mu}{SUL} \right) \frac{\partial^2 u_y^*}{\partial y^{*2}}}$$

$$\frac{\partial p^*}{\partial y^*} = 0$$

$$S\left(u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y}\right) = \underbrace{-\frac{\partial p}{\partial x}}_{\frac{\partial b}{\partial y} = 0} + \mu \frac{\partial^2 u_x}{\partial y^2} \rightarrow \vec{U}(x) = \vec{U}$$

$\overline{Re^{-1}}$

$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} = 0$$

Boundary layer equations

$$U \frac{\partial U}{\partial x} + u_y \frac{\partial U}{\partial y} = \underbrace{-\frac{\partial p}{\partial x}}_{=0} \quad \begin{array}{l} \text{Outer} \\ \text{Inviscid flow} \end{array}$$

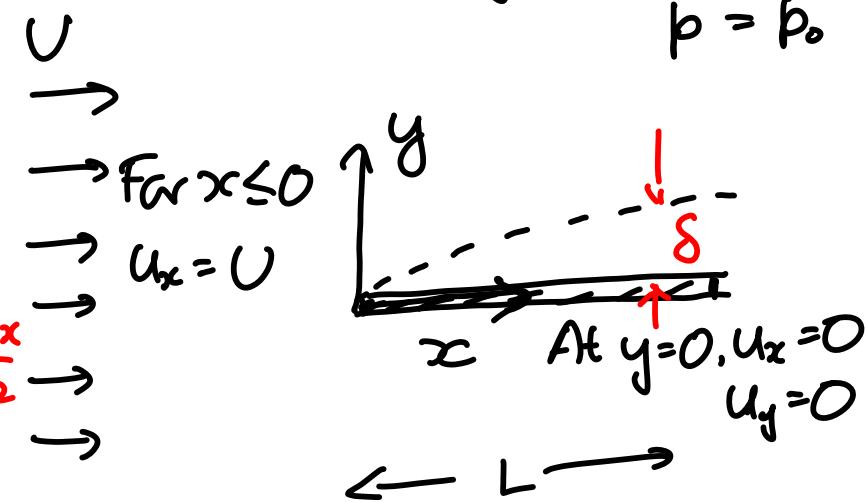
$$S\left(u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y}\right) = U \frac{\partial U}{\partial x} + \mu \frac{\partial^2 u_x}{\partial y^2}$$

Boundary layer theory:

$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} = 0$$

$$\rho \left(u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} \right) = - \frac{\partial p}{\partial x} + \nu \frac{\partial^2 u_x}{\partial y^2}$$

$$\rho \left(u_x \frac{\partial u_y}{\partial x} + u_y \frac{\partial u_y}{\partial y} \right) = - \frac{\partial p}{\partial y}$$



$$Re = \frac{UL}{\nu} \gg 1$$

'Boundary layer logic'

$$x^* = (x/L); \quad y^* = (y/\delta); \quad u_x^* = (u_x/U); \quad u_y^* = u_y/(U\delta/L) \quad p^* = p/(bSU^2)$$

$$\left(u_x^* \frac{\partial u_x^*}{\partial x^*} + u_y^* \frac{\partial u_x^*}{\partial y^*} \right) = - \frac{\partial p^*}{\partial x^*} + \frac{\partial^2 u_x^*}{\partial y^{*2}}$$

$$O = - \frac{\partial p^*}{\partial y^*}$$

$$u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} = \frac{\partial^2 u_x}{\partial y^2}$$

$$\underline{u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y}} = \sim \frac{\partial^2 u_x}{\partial y^2}$$

$$\frac{\partial p}{\partial y} = 0$$

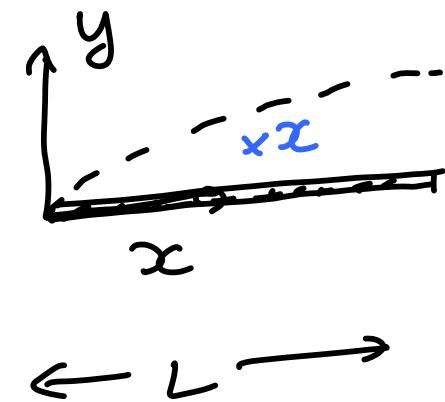
$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} = 0$$

$$\underline{y^* = \frac{y}{(Nx/U)^{1/2}}} = \eta$$

$$u_x = \frac{\partial \Psi}{\partial y} \quad u_y = -\frac{\partial \Psi}{\partial x}$$

$$S = Re^{-1/2} L = \left(\frac{NL}{U}\right)^{1/2} = \left(\frac{Nx}{U}\right)^{1/2}$$

$$= \left(\frac{M}{SUL}\right)^{1/2} L$$



$$u_x = \frac{\partial \Psi}{\partial y} \quad u_y = -\frac{\partial \Psi}{\partial x} \quad \eta = y/\sqrt{\frac{vx}{U}} \quad \Psi = \sqrt{vxU} f(\eta)$$

$$= \sqrt{vxU} \frac{1}{\sqrt{vxU}} \frac{df}{d\eta}$$

$$= U f'(\eta)$$

$$u_y = -\frac{\partial \Psi}{\partial x} = -\frac{1}{x} \left[\sqrt{vxU} f(\eta) \right]$$

$$= -\frac{1}{2} \sqrt{\frac{vU}{x}} f(\eta) - \sqrt{vxU} f'(\eta) \frac{\partial \eta}{\partial x}$$

$$= -\frac{1}{2} \sqrt{\frac{vU}{x}} f(\eta) - \sqrt{vxU} f'(\eta) \left(\frac{-\eta}{2x} \right)$$

$$= \frac{1}{2} \sqrt{\frac{vU}{x}} \left[\eta f' - f \right]$$

$$\begin{aligned} \frac{\partial \eta}{\partial y} &= \frac{1}{\sqrt{vxU}} \\ \left(\frac{\partial \eta}{\partial x} \right) &= \frac{-y}{2x^{3/2} (vU)^{1/2}} \\ &= \frac{-y}{2x (vU)^{1/2}} = \frac{-\eta}{2x} \end{aligned}$$

$$u_x = U f'(n) \quad u_y = \frac{1}{2} \left(\frac{U}{x} \right)^{1/2} (n f' - f)$$

$$\begin{aligned} \frac{\partial u_x}{\partial x} &= U f''(n) \frac{\partial n}{\partial x} \quad | \quad \frac{\partial u_x}{\partial y} = U f'' \frac{\partial n}{\partial y} \quad | \quad \frac{\partial^2 u_x}{\partial y^2} = \frac{U f'''}{(n x / U)} \\ &= U f'' \left[-\frac{n}{2x} \right] \quad | \quad = U f'' \left[\frac{1}{\sqrt{n x / U}} \right] \end{aligned}$$

$$u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} = N \frac{\partial^2 u_x}{\partial y^2}$$

$$(U f') \left[U f'' \left(-\frac{n}{2x} \right) \right] + \frac{1}{2} \left(\frac{U}{x} \right)^{1/2} (n f' - f) \frac{U f''}{\sqrt{n x / U}} = \left(\frac{N}{n x / U} \right) U f'''$$

$$\frac{U^2}{x} \left[-\frac{1}{2} n f' f'' + \frac{1}{2} n f' f'' - \frac{1}{2} f f''' \right] = \frac{U^2}{x} f'''$$

$$f''' + \frac{1}{2} f f'' = 0 \quad \text{Blasius boundary layer eqn.}$$

$$\psi = (\nu x \cup)^{1/2} f(n)$$

$$u_x = \nu f'(n) = \nu \frac{df}{d\eta}$$

$$u_y = \frac{1}{2} \left(\frac{\nu \nu}{\nu c} \right)^{1/2} (n f' - f)$$

As $y \rightarrow \infty$, $\frac{u_x}{\nu} = 1 \Rightarrow \frac{df}{d\eta} = 1$

At $y=0$, $u_x=0$ $\frac{df}{d\eta} = 0$

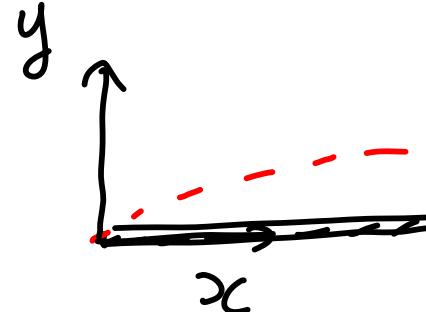
$\eta=0$ $u_y=0$ $f=0$

For $x \leq 0$, $u_x=\nu \Rightarrow \frac{df}{d\eta} = 1$

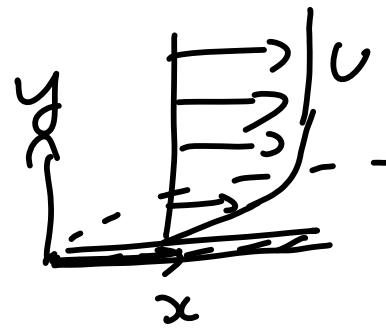
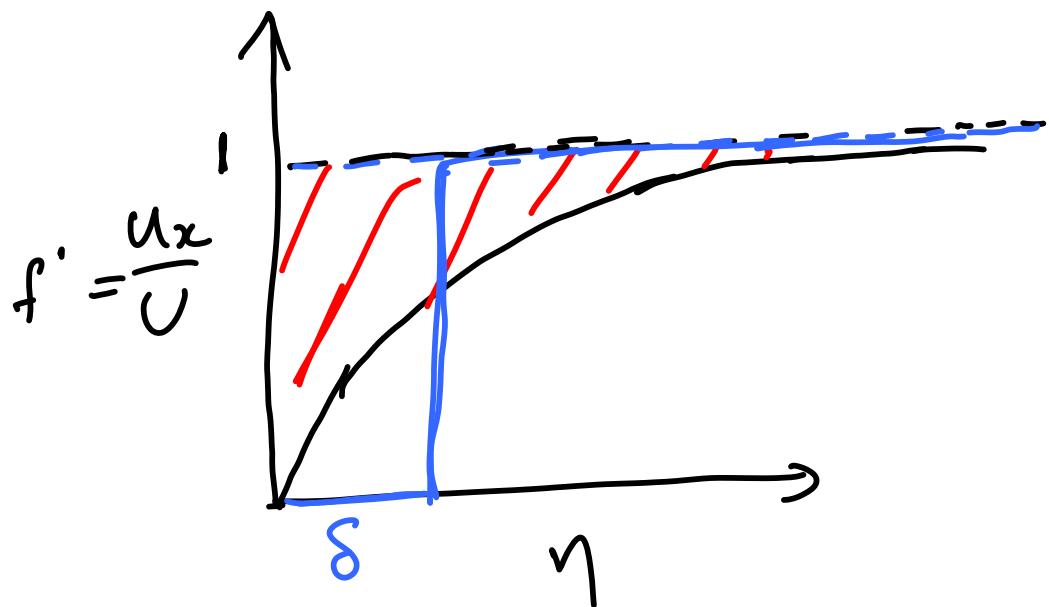
$\eta \rightarrow \infty$

$$\delta = \left(\frac{\nu x}{\nu} \right)^{1/2} \quad \text{As } y \rightarrow \infty, u_x = \nu$$

$$\eta = \frac{y}{\sqrt{\nu x / \nu}}$$



$$f''' + \frac{1}{2} f f'' = 0$$



$$\eta = \sqrt{\frac{U_x}{U}}$$

$$\psi = (U_x U)^{1/2} f(\eta)$$

$$U_x = U f'(\eta)$$

$$\delta_{0.99} = 4 \cdot 9 \left(\frac{U_x}{U} \right)^{1/2}$$

$$\text{Total flow rate} = \int_0^\infty dy S U_x$$

$$\text{Potential flow rate} = \int_0^\infty dy S U$$

$$S S U = \int_0^\infty dy S U - \int_0^\infty dy S U_x$$

$$\delta = \int_0^\infty dy \left(1 - \frac{U_x}{U} \right) = 1.72 \left(\frac{U_x}{U} \right)^{1/2}$$

Flow past flat plate:

$$\vec{v}$$

$$\delta = Re^{-1/2} L$$

$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} = 0$$

$$\rightarrow$$



$$u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} = + \left[N \frac{\partial^2 u_x}{\partial y^2} \right]$$

$$\rightarrow$$

$$\frac{\partial p}{\partial y} = 0$$

$$\leftarrow L \rightarrow$$

$$Re = \left(\frac{UL}{N} \right) \gg 1$$

$$\delta = (Nx/U)^{1/2} \quad \eta = y/\delta = y/\sqrt{Nx/U}$$

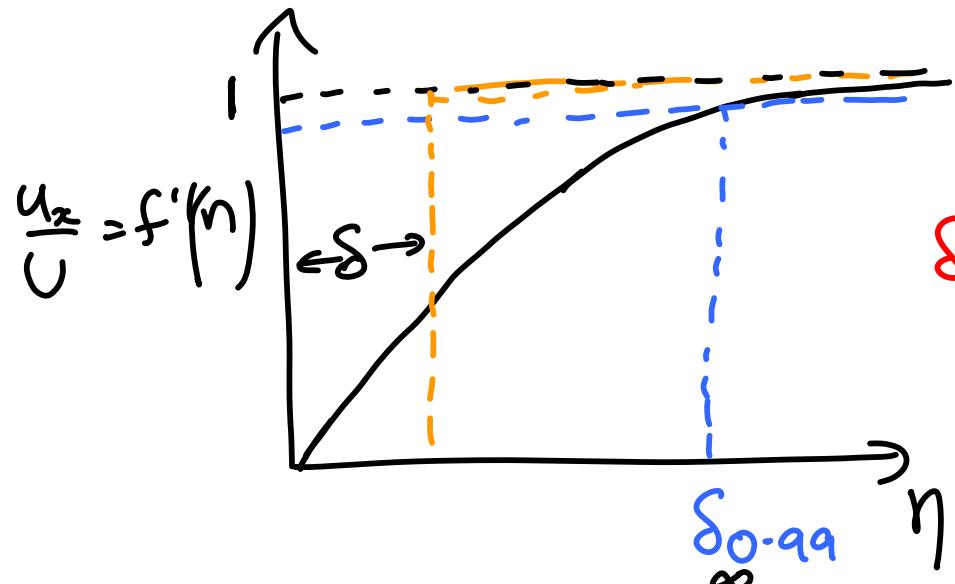
$$u_x = \frac{\partial \psi}{\partial y} \quad u_y = -\frac{\partial \psi}{\partial x} \quad \psi = (NxU)^{1/2} f(\eta)$$

$$f''' + \frac{1}{2} ff'' = 0$$

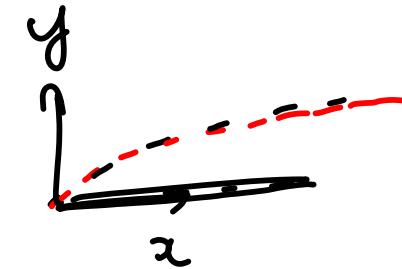
$$\text{At } y=0, u_x=0 \quad (f'(0)=0) \quad u_y=0 \quad (f(0)=0) \quad (\eta=0)$$

$$\text{As } y \rightarrow \infty, u_x = U \quad (f'(\eta) = 1) \quad \eta \rightarrow \infty$$

$$\text{As } x \rightarrow \infty, u_x = U \quad (f'(0) = 1)$$



$$\delta_{0.99} = 4.9 \left(\frac{Ux}{U}\right)^{1/2}$$



$$\eta = y / \sqrt{Ux}/\delta$$

Total flow rate = $\int_{-\infty}^{\infty} dy u_x$

Potential flow = $\int_{-\infty}^{\infty} dy V$

Corrected flow rate = $\int_{-\infty}^{\infty} dy V = \int_{-\infty}^{\infty} dy u_x$

$$\int_{-\infty}^{\infty} dy V - \int_{-\infty}^{\infty} dy u_x = \int_{-\infty}^{\infty} dy u_x$$

$$\int_{-\infty}^{\infty} dy (V - u_x) = \int_{-\infty}^{\infty} dy V = U \delta \Rightarrow \delta = \int_{-\infty}^{\infty} dy \left(\frac{V - u_x}{U}\right)$$

$$= 1.72 \sqrt{\frac{Ux}{U}}$$

van-Karman momentum thickness:

$$\Theta = \int_0^\infty dy \left(\frac{u_x}{U} \right) \left(1 - \frac{u_x}{U} \right) = 0.664 \sqrt{\frac{v_x}{U}}$$

$$T_{xy} = \mu \left. \frac{du_x}{dy} \right|_{y=0} = \left. \frac{\mu v}{\sqrt{v_x/U}} f''(n) \right|_{n=0} = \left. \frac{\mu v}{\sqrt{v_x/U}} \right|_{n=0} 0.332$$

$$C_f = \frac{T_w}{\frac{1}{2} S U^2} = 2 \left. f''(n) \right|_{n=0} Re_x^{-1/2} = 0.664 Re_x^{-1/2}$$

$$Re_x = \left(\frac{Ux}{\nu} \right)^{1/2}$$

$$F_x = \int_0^L dx T_{xy} = \int_0^L dx (0.332) \frac{\mu v}{\sqrt{v_x/U}}$$

$$C_D = \frac{F_x}{\frac{1}{2} S U^2 L} = 1.338 Re_v^{-1/2}$$

Stagnation point flow

$$F(z) = Az^2 \Rightarrow w = 2Az$$

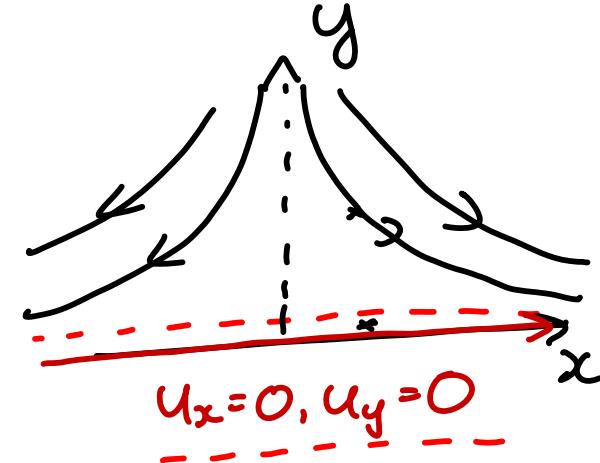
$$= \phi(x, y) + i\psi(x, y) = 2A(x + iy)$$

$$= u_x - iu_y$$

$$= A(x^2 - y^2 + 2xyi)$$

$$\underline{u_x = 2Ax} = \boxed{Kx}$$

$$\underline{u_y = -2Ay} = -Ky$$



$$\psi = Kxy$$

$$p = p_0 - \frac{1}{2} \rho S u^2 = p_0 - \frac{1}{2} \rho 8k^2 (x^2 + y^2) \quad \frac{\partial p}{\partial x} = (-8k^2 x)$$

$$\delta = \left(\frac{u_x}{u} \right)^{1/2} = \left(\frac{N}{K} \right)^{1/2}$$

$$u_{xc} = \frac{\partial \psi}{\partial y} = Kx$$

$$u_{x^*} = \frac{u_x}{Kx} = \left(\frac{N}{K} \right)^{1/2} \frac{\partial \psi}{\partial \eta} \quad \mid \quad \psi = Kx \left(\frac{N}{K} \right)^{1/2} f(\eta)$$

$$\Psi = \boxed{Kx} \left(\frac{N}{k} \right)^{1/2} f(\eta) \quad \eta = \frac{y}{(N/k)^{1/2}}$$

$$u_x = \frac{\partial \Psi}{\partial y} = Kx \frac{df}{d\eta} = kx \left(\frac{N}{k} \right)^{1/2} \frac{1}{(N/k)^{1/2}} \frac{df}{d\eta}$$

$$u_y = - \frac{\partial \Psi}{\partial x} = -K \left(\frac{N}{k} \right)^{1/2} f(\eta)$$

$$\frac{\partial u_x}{\partial x} = kf'(n) \quad \frac{\partial u_x}{\partial y} = \frac{kx}{(N/k)^{1/2}} f''(n) \quad \frac{\partial^2 u_x}{\partial y^2} = \frac{kx}{(N/k)} f'''(n)$$

$$u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} = -\frac{1}{S} \frac{\partial p}{\partial x} + N \frac{\partial^2 u_x}{\partial y^2}$$

- - - -

$$\frac{\partial f}{\partial y} = 0$$

$$(Kx f') (kf') + \left(-K \left(\frac{N}{k} \right)^{1/2} f \right) \left(\frac{kx}{(N/k)^{1/2}} f'' \right) = k^2 x + \frac{N K x}{(N/k)} f'''$$

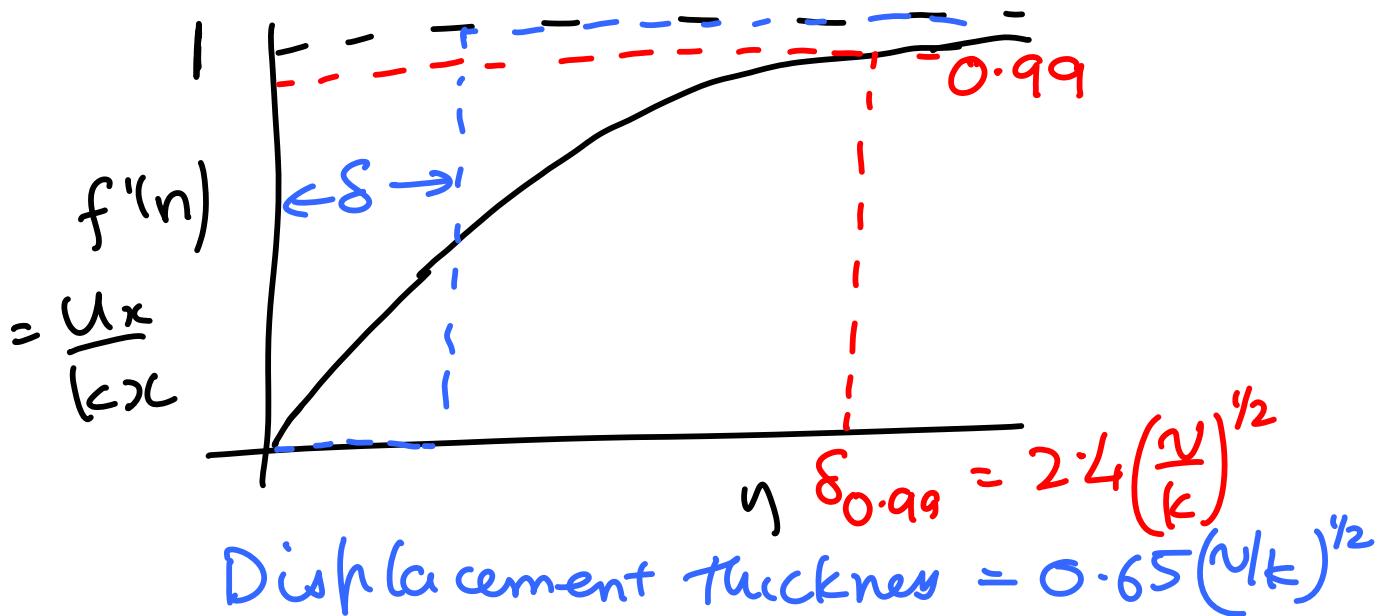
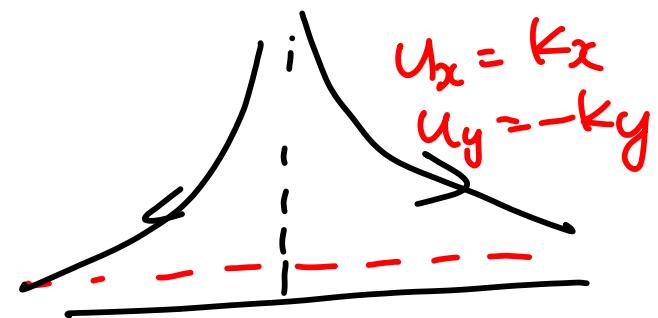
$$\cancel{K^2} \cancel{x} [f'^2 - ff''] = \cancel{K^2} \cancel{x} [1 + f''']$$

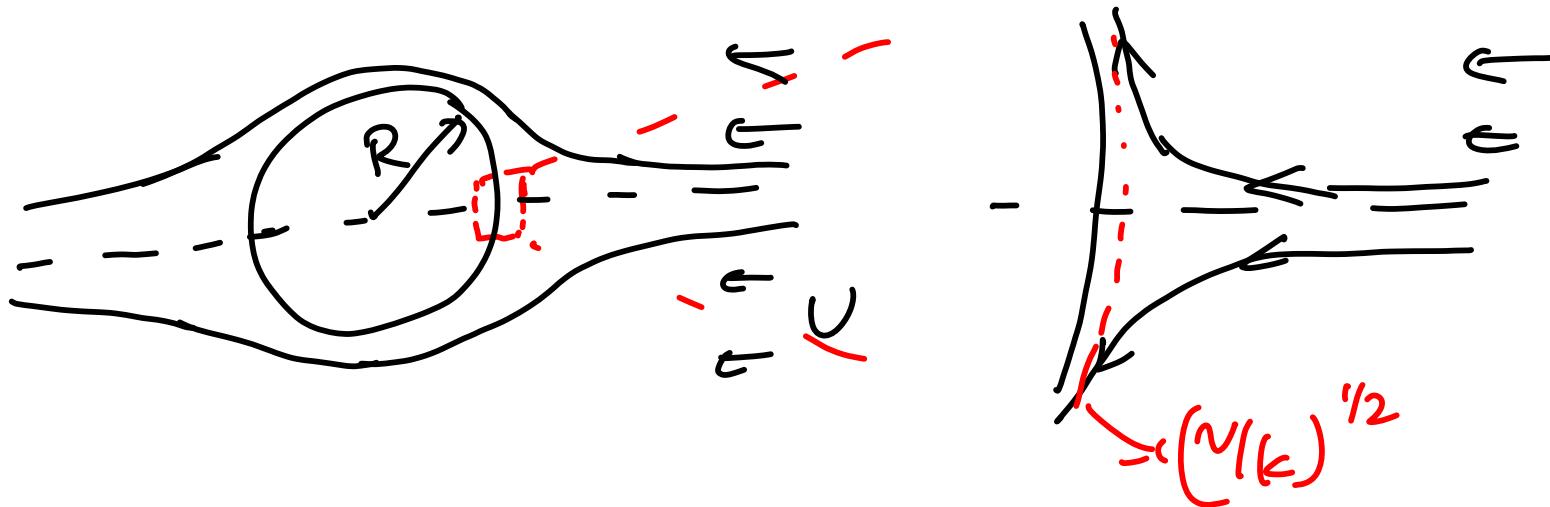
$$f''' + ff'' + (1 - f'^2) = 0$$

$$\text{At } y=0, u_x=0 \Rightarrow \frac{df}{d\eta} = 0$$

$$\eta=0 \quad u_y=0 \Rightarrow f=0$$

$$\begin{aligned} \text{As } y \rightarrow \infty, \quad u_x &= Kx = Kx f'(\eta) \\ \eta \rightarrow \infty \quad &\quad f'(\eta) > 1 \end{aligned}$$





Stagnation point flow

$$\left(\frac{N}{K}\right)^{1/2} \ll R$$

$$u_x = Kx$$

$$u_y = -Ky$$

$$K \propto \left(\frac{U}{R}\right) \quad \left(\frac{N}{U/R}\right)^{1/2} \ll R \quad \text{or} \quad \left(\frac{N}{UR}\right)^{1/2} \ll 1$$

$$Re^{-1/2} \ll 1$$

Boundary layer theory:

$$\frac{\partial U_x}{\partial x} + \frac{\partial U_y}{\partial y} = 0$$

$$U_x \frac{\partial U_x}{\partial x} + U_y \frac{\partial U_x}{\partial y} = -\frac{1}{\rho} \left(\frac{\partial p}{\partial x} \right) + \nu \frac{\partial^2 U_x}{\partial y^2}$$

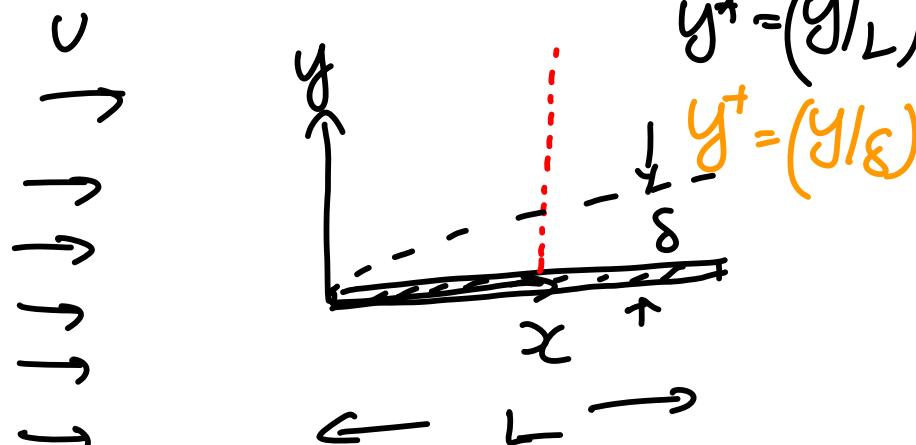
$$\frac{\partial p}{\partial y} = 0$$

$$p = p_0 - \frac{1}{2} \rho U^2 = p_0 - \frac{1}{2} \rho (U_x^2 + U_y^2)$$

$$\frac{\partial p}{\partial x} = -\rho \left(U_x \frac{\partial U_x}{\partial x} + U_y \frac{\partial U_y}{\partial x} \right) = -\rho U_x \frac{\partial U_x}{\partial x}$$

$$= -\rho U \frac{\partial U}{\partial x} \Big|_{y^* \rightarrow 0}$$

At $y=0$, $U_x=0$, $U_y=0$



In boundary layer
 $y^* \propto (\delta/L) \rightarrow 0$

Approach Potential flow
 from BL
 $y^* \propto (H_\delta) \rightarrow \infty$
 $\eta \rightarrow \infty$

$$U_x \frac{\partial U_x}{\partial x} + U_y \frac{\partial U_x}{\partial y} = U \frac{\partial U}{\partial x} + N \frac{\partial^2 U_x}{\partial y^2}$$

$$\boxed{\frac{\partial U_x}{\partial x} + \frac{\partial U_y}{\partial y} = 0}$$

$$\eta = y/\delta(x) \quad \text{where } \delta(x) = \left(\frac{Nx}{U}\right)^{1/2}$$

$$U_x = U \frac{df}{d\eta}$$

$$\frac{\delta(x)}{x} = \left(\frac{N}{xU}\right)^{1/2} = Re_x^{-1/2}$$

$$\Psi = (NxU)^{1/2} f(\eta)$$

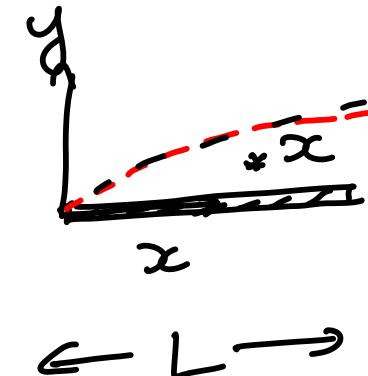
$$U_x = \frac{\partial \Psi}{\partial y} \quad U_y = -\frac{\partial \Psi}{\partial x}$$

$$\frac{d^3 f}{d\eta^3} + \frac{1}{2} f \frac{d^2 f}{d\eta^2} = 0$$

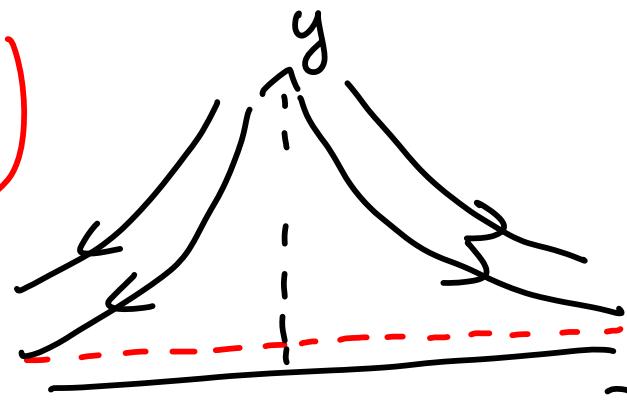
At $y=0$, $f=0, \frac{df}{d\eta}=0$

$$\eta=0$$

As $y \rightarrow \infty$
($\eta \rightarrow \infty$) $\frac{df}{d\eta} = 1$



$$\delta(x) = \left(\frac{N x}{U}\right)^{1/2} \equiv \left(\frac{N}{k}\right)^{1/2} \quad n = \left(\frac{y}{\delta(x)}\right)$$



Potential flow solution

$$u_x = kx, u_y = -ky$$

$$\psi = kxy$$

$$p = -\frac{1}{2}k^2x^2 + p_0$$

$$\psi = (NxU)^{1/2} f(n)$$

$$= (Nk)^{1/2} x f(n)$$

$$u_x = kx f'(n)$$

$$f'' + ff'' + (1-f'^2) = 0$$

General velocity profile $V(x)$

$$S = \left(\frac{V(x)}{U_\infty} \right)^{1/2} = \left(\frac{V(x)}{f} \right)^{1/2} = S(x) \quad \eta = y/\delta(x)$$

$$\Psi = \underbrace{U(x) \delta(x)}_{\text{---}} f(\eta)$$

$$U_x = \frac{\partial \Psi}{\partial y} = U(x) \frac{df}{d\eta}$$

$$U_y = -\frac{\partial \Psi}{\partial x} = -\frac{d}{dx}(U\delta) f + (U\delta) \left(\frac{\eta}{\delta} \frac{df}{dx} \right) \frac{df}{d\eta}$$

$$= -\frac{d}{dx}(U\delta) f + U \eta \frac{df}{dx} \frac{df}{d\eta}$$

$$\frac{\partial U_x}{\partial x} = \left(\frac{dU}{dx} \right) \frac{df}{d\eta} - \frac{\eta}{\delta} \frac{d\delta}{dx} U(x) \frac{d^2 f}{d\eta^2}$$

$$\frac{\partial}{\partial x} \equiv \frac{\partial \eta}{\partial x} \frac{\partial}{\partial \eta} = -\frac{y}{\delta^2} \frac{df}{dx} \frac{d}{d\eta}$$

$$= -\frac{\eta}{\delta} \frac{df}{dx} \frac{d}{d\eta}$$

$$\frac{\partial}{\partial y} \equiv \frac{\partial \eta}{\partial y} \frac{\partial}{\partial \eta} = \frac{1}{\delta} \frac{\partial}{\partial \eta}$$

$$\frac{\partial u_x}{\partial y} = \frac{U(x)}{\delta} \frac{d^2 f}{d\eta^2} ; \quad \frac{\partial^2 u_x}{\partial y^2} = \frac{U(x)}{\delta^2} \frac{d^3 f}{d\eta^3}$$

$$u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} = U \frac{du}{dx} + N \frac{\partial^2 u_x}{\partial y^2}$$

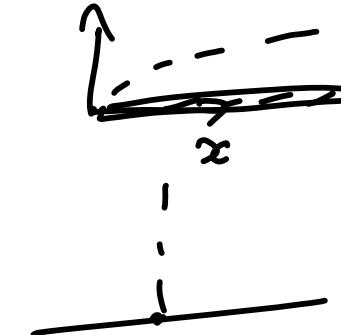
$$\left(\frac{U \frac{df}{d\eta}}{\delta} \right) \left(\frac{du}{dx} \frac{df}{d\eta} - \frac{U \eta \frac{d\delta}{dx} \frac{d^2 f}{d\eta^2}}{\delta^2} \right) + \left[- \frac{d}{dx} (U\delta) f(\eta) + \eta \frac{U d\delta}{dx} \frac{df}{d\eta} \right] \left[\frac{U \frac{df}{d\eta}}{\delta} \right] = U \frac{du}{dx} + \frac{NU}{\delta^2} \frac{d^3 f}{d\eta^3}$$

$$\underline{U \frac{du}{dx} \left(\frac{df}{d\eta} \right)^2 - \frac{U}{\delta} \frac{d}{dx} (U\delta) f \frac{d^2 f}{d\eta^2}} = U \frac{du}{dx} + \frac{NU}{\delta^2} \frac{d^3 f}{d\eta^3}$$

$$\frac{d^3 f}{d\eta^3} + \frac{\delta^2}{N} \frac{d^2 U}{dx^2} \left[1 - \frac{d^2 f}{d\eta^2} \right] + \frac{\delta}{N} \frac{d}{dx} (U\delta) \left(f \frac{d^2 f}{d\eta^2} \right) = 0$$

$$\underline{\frac{\delta}{N} \frac{d}{dx} (U\delta) = \alpha} \quad \underline{\frac{\delta^2}{N} \frac{d^2 U}{dx^2} = \beta}$$

$$\frac{\delta^2}{N} \frac{dU}{dx} + \frac{\delta U}{N} \frac{d\delta}{dx} = \alpha \implies \frac{\delta U}{N} \frac{d\delta}{dx} = \alpha - \beta$$



$$\frac{1}{N} \frac{d}{dx} (\delta^2 U) = \frac{2\delta U}{N} \frac{d\delta}{dx} + \frac{\delta^2}{N} \frac{dU}{dx}$$

$$= (2\alpha - \beta) \quad \delta = \left(\frac{Nx}{J} \right)^{1/2}$$

$$\frac{d}{dx} (\delta^2 U) = N(2\alpha - \beta)$$

$$\delta^2 U = N(2\alpha - \beta)x + C$$

$$\delta^2 U = N(2\alpha - \beta)x = \left(\frac{N(2\alpha - \beta)}{J} x \right)^{1/2}$$

$$= Nx$$

$$\frac{\delta^2}{N} \frac{dU}{dx} = \beta \quad \frac{1}{N} \left(\frac{Nx}{J} \right) \frac{dU}{dx} = \beta$$

$$\frac{x}{J} \frac{dU}{dx} = \beta \implies \frac{dU}{J} = \frac{\beta dx}{x}$$

$$\implies U = K x^\beta$$

Boundary layer theory:

$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} = 0$$

$$u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \frac{\partial^2 u_x}{\partial y^2}$$

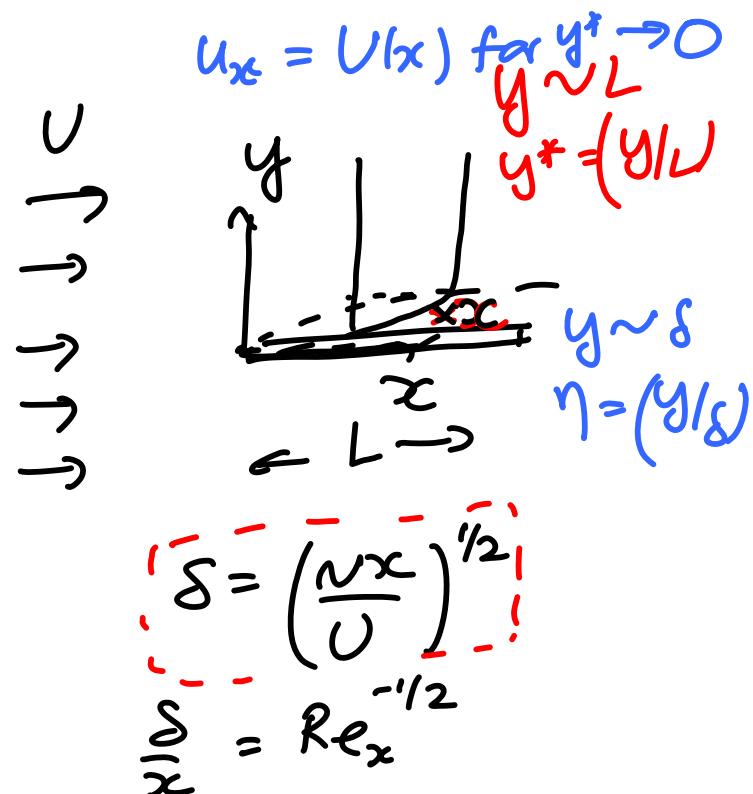
$$\frac{\partial p}{\partial y} = 0$$

Potential flow for $y^* \rightarrow 0$

$$p = p_0 - \frac{1}{2} \rho (u_x^2 + u_y^2) = p_0 - \frac{1}{2} \rho S U^2$$

$$\frac{\partial p}{\partial x} = -\rho U \frac{du}{dx}$$

$$u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} = U \frac{du}{dx} + \nu \frac{\partial^2 u_x}{\partial y^2}$$



$$\psi = \underbrace{U S f(n)}_{\dots} \quad \eta = (y/\delta(x))$$

$$\delta(x) = \left(\frac{nx}{U}\right)^{1/2}$$

$$u_x = \frac{\partial \psi}{\partial y} \quad u_y = -\frac{\partial \psi}{\partial x}$$

$$u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} = \underbrace{U \frac{\partial U}{\partial x}}_{\dots} + \underbrace{N \frac{\partial^2 u_x}{\partial y^2}}_{\dots}$$

$$\frac{d^3 f}{dn^3} + \underbrace{\left(\frac{\delta^2}{N} \frac{dU}{dx} \right)}_{\dots} \left(1 - \left(\frac{df}{dn} \right)^2 \right) + \underbrace{\left(\frac{\delta}{N} \frac{d(U\delta)}{dx} \right)}_{\dots} \left[f \frac{d^2 f}{dn^2} \right] = 0$$

$$\textcircled{1} \quad \underbrace{\left(\frac{\delta^2}{N} \frac{dU}{dx} \right)}_{\dots} = \beta \quad \textcircled{2} \quad \underbrace{\frac{\delta}{N} \frac{d(U\delta)}{dx}}_{\dots} = \alpha$$

$$\textcircled{3} \quad \underbrace{\frac{1}{N} \frac{d}{dx} (\delta^2 U)}_{\dots} = (2\alpha - \beta)$$

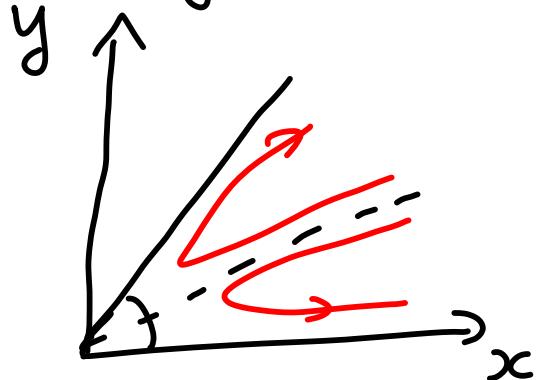
$$\delta^2 U = N(2\alpha - \beta)x$$

$$\begin{aligned} \delta &= \sqrt{\frac{(2\alpha - \beta)Nx}{U}} \\ &= \left(\frac{nx}{U}\right)^{1/2} \end{aligned}$$

$$\frac{\delta^2}{\lambda} \frac{dU}{dx} = \beta \Rightarrow \left(\frac{\lambda x}{U}\right) \frac{1}{\lambda} \frac{dU}{dx} = \beta$$

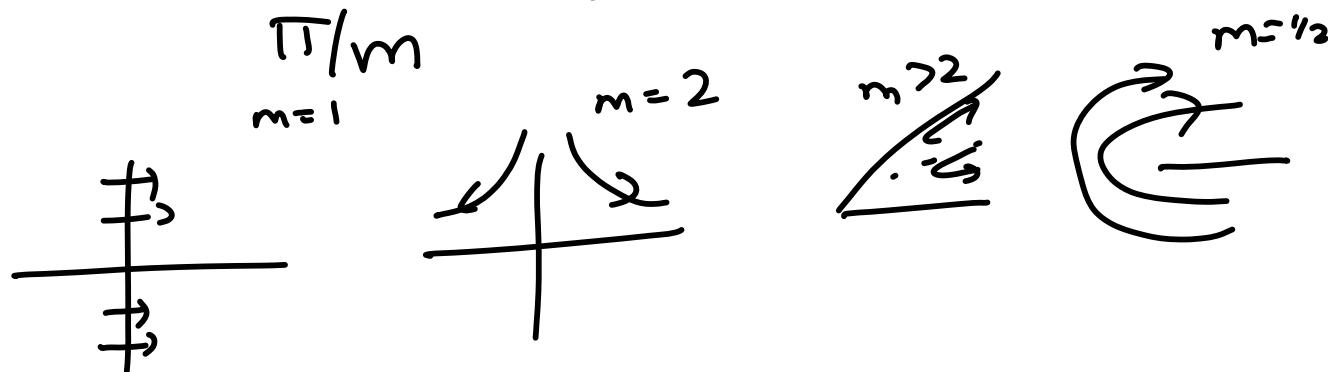
$$\frac{1}{U} \frac{dU}{dx} = \frac{\beta}{x} \Rightarrow U = Kx^\beta \Rightarrow \begin{aligned} K &= mA \\ \beta &= m-1 \end{aligned}$$

$$U(x) = \lim_{y^* \rightarrow 0} u_x(x)$$



As $y \rightarrow 0$

$$\begin{aligned} F &= Az^m \\ W &= mA z^{m-1} = mA(x+iy)^{m-1} = mA x^{m-1} \\ &= (u_x - iu_y) \end{aligned}$$



$$\frac{d^3 f}{d\eta^3} + \frac{\delta^2}{N} \frac{dU}{dx} \left(1 - \left(\frac{df}{d\eta} \right)^2 \right) + \frac{\delta}{N} \frac{d}{dx} (U\delta) \left(f \frac{d^2 f}{d\eta^2} \right) = 0$$

$$\frac{\delta^2}{N} \frac{dU}{dx} = \beta = m - 1 \quad 2\alpha - \beta = 1 \Rightarrow \delta(x) = \left(\frac{Nx}{J} \right)^{1/2}$$

$$\frac{\delta}{N} \frac{d}{dx} (U\delta) = \frac{1}{2} (1 + \beta) = \frac{m}{2}$$

'Falkner-Skan equation'

$$\frac{d^3 f}{d\eta^3} + \beta \left(1 - \frac{df}{d\eta^2} \right) + \frac{1}{2} (1 + \beta) f \frac{d^2 f}{d\eta^2} = 0$$

$$\text{Flat plate } \beta = 0, m = 1 \quad f''' + \frac{1}{2} ff'' = 0$$

$$\text{Stagnation point } \beta = 1, m = 2 \quad f''' + (1 - f'^2) + ff'' = 0$$

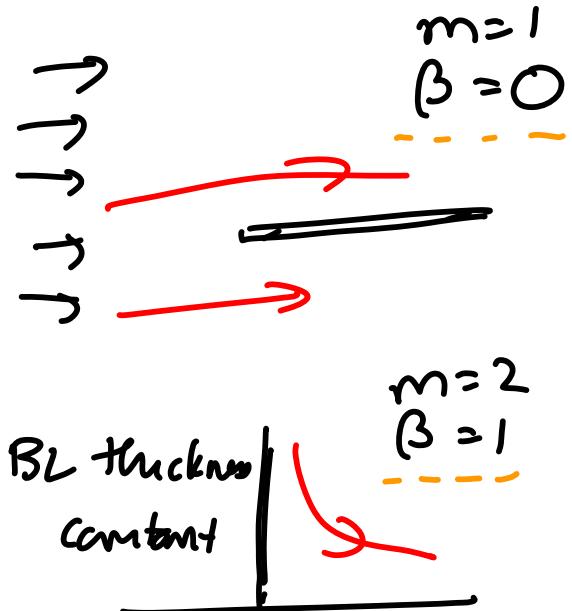
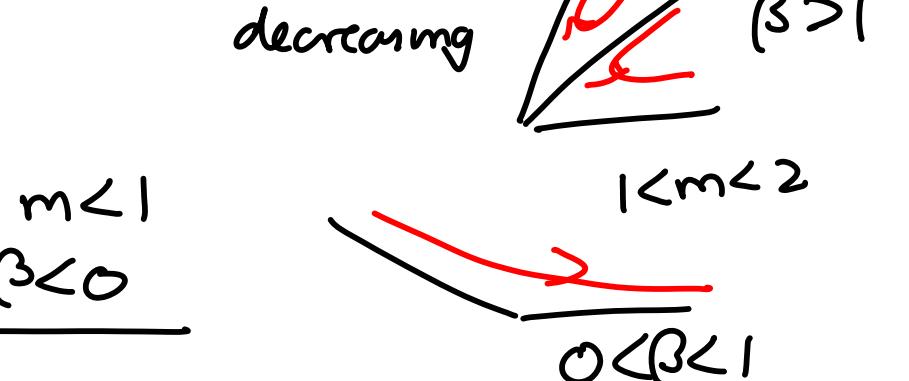
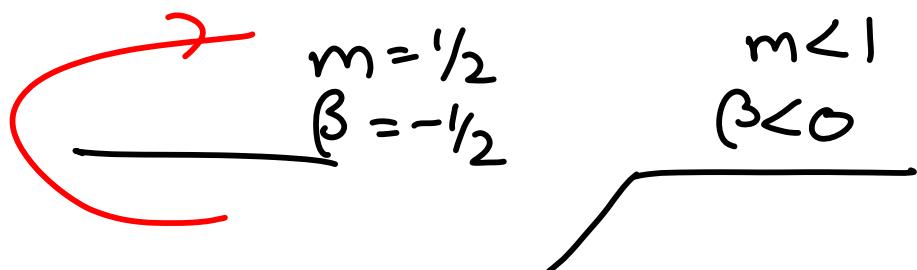
$$\delta = \left(\frac{Nx}{U}\right)^{1/2} = \left(\frac{Nx}{kx^\beta}\right)^{1/2} = \left(\frac{N}{k}\right)^{1/2} x^{(1-\beta)/2}$$

$$T_{xy} = \mu \frac{du_x}{dy} = \frac{\mu U}{\delta} \left(\frac{d^2 f}{d y^2} \right)$$

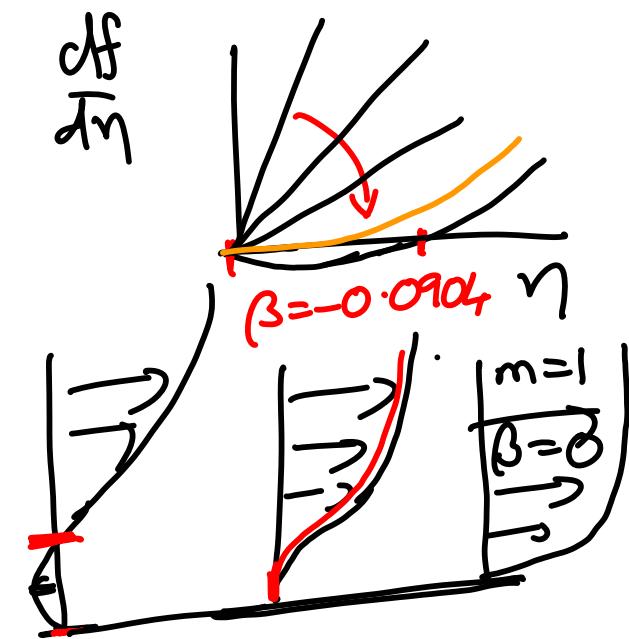
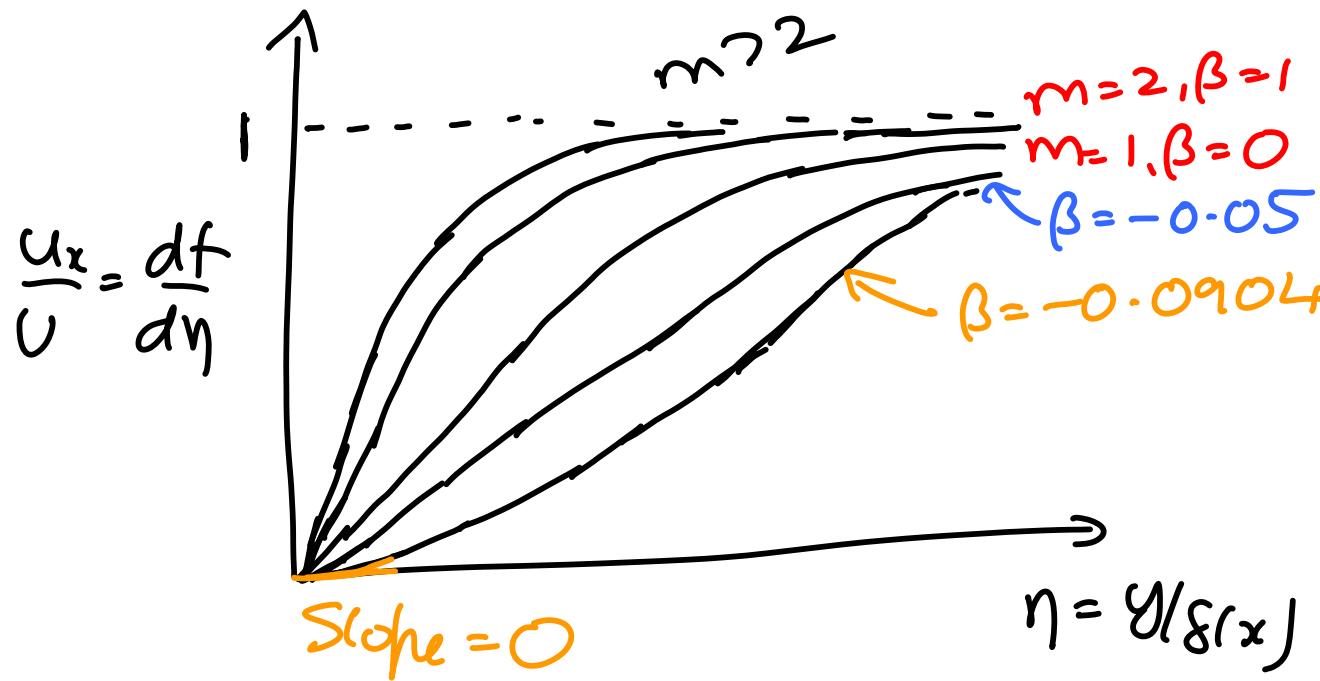
$$= \frac{\mu U}{(Nx/U)^{1/2} d y^2} \frac{d^2 f}{d y^2} = \frac{\mu U^{3/2}}{x^{1/2} N^{1/2}} f''$$

$$= \frac{\mu k^{3/2} x^{(\frac{3\beta}{2}-1)}}{N^{1/2}} f''$$

$$T_{xy} \propto x^{(\frac{3\beta-1}{2})}$$

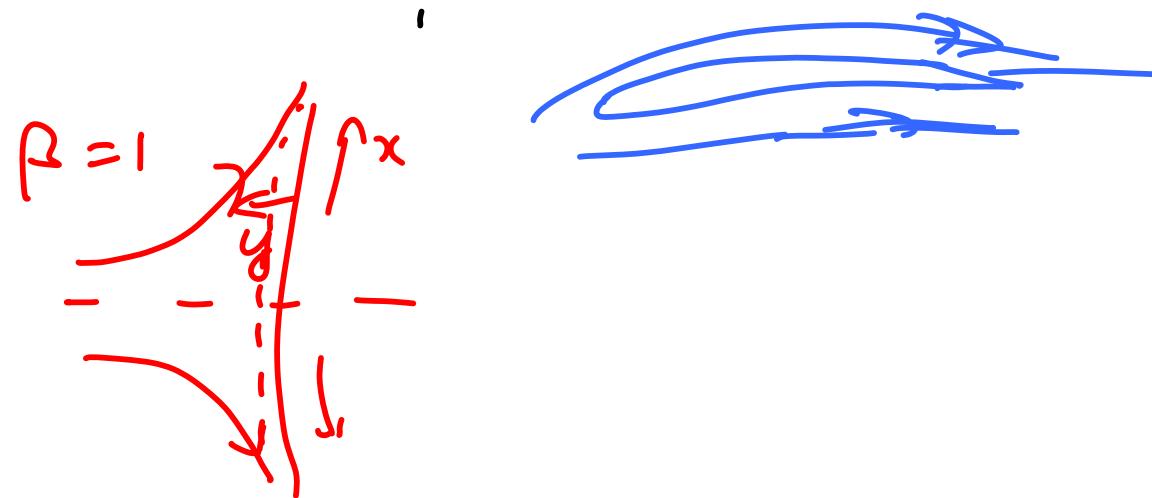
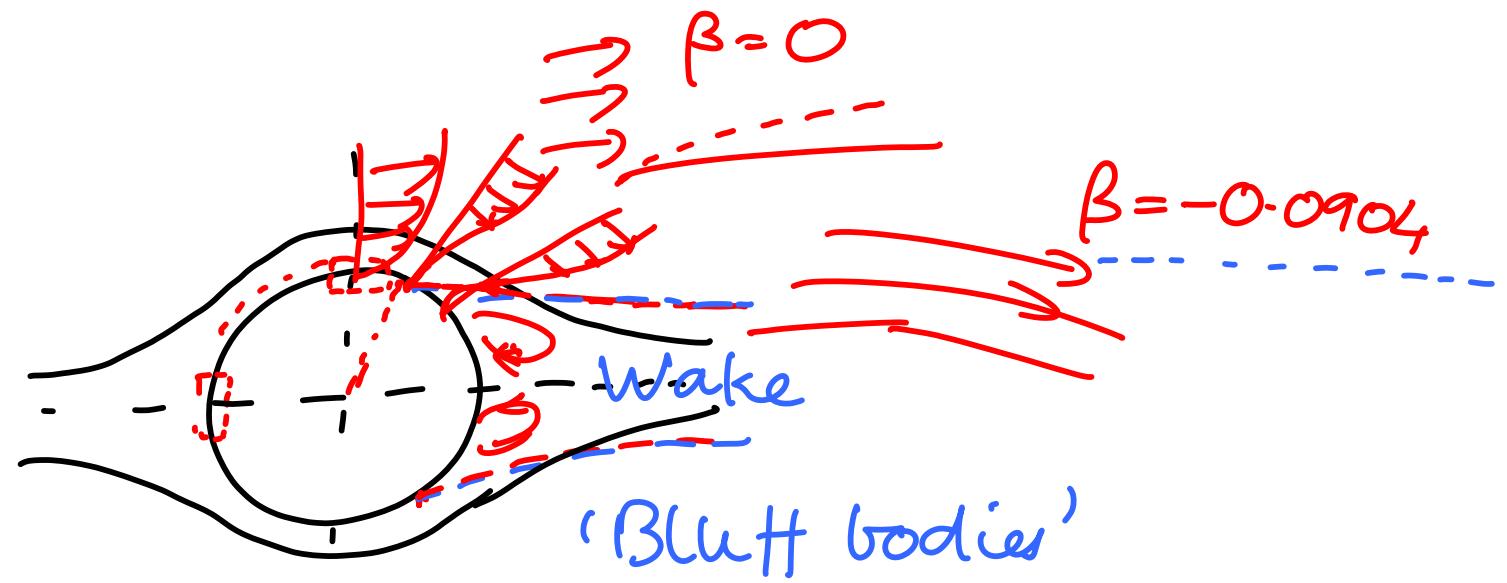


Falkner-Skan Solutions



$$u_x = U \frac{df}{d\eta} = U(x) \frac{df}{d\eta} \Rightarrow \frac{u_x}{U(x)} = \frac{df}{d\eta}$$

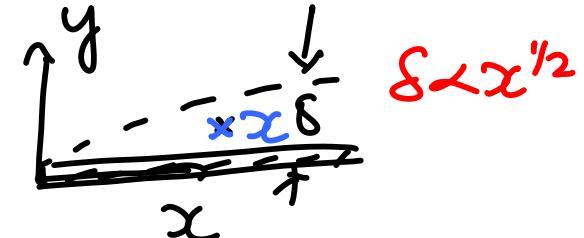
$\cancel{x \parallel}$ $\overset{\rightarrow}{\cancel{\beta=1}} \quad \overset{\rightarrow}{\cancel{\beta=0}} \quad \overset{\rightarrow}{\cancel{\beta<0}}$



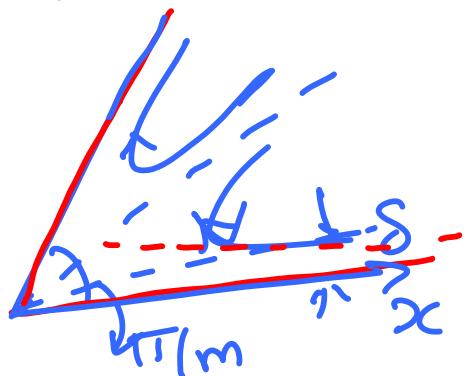
Boundary layer:

$$U \propto x^\beta$$

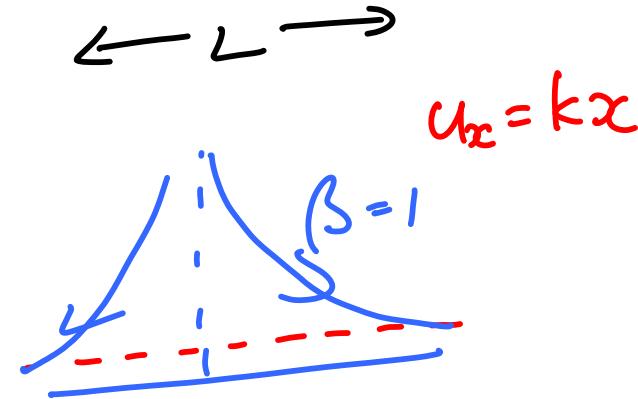
$$\delta \propto Re_x^{-1/2}$$



Falkner-Skan solutions



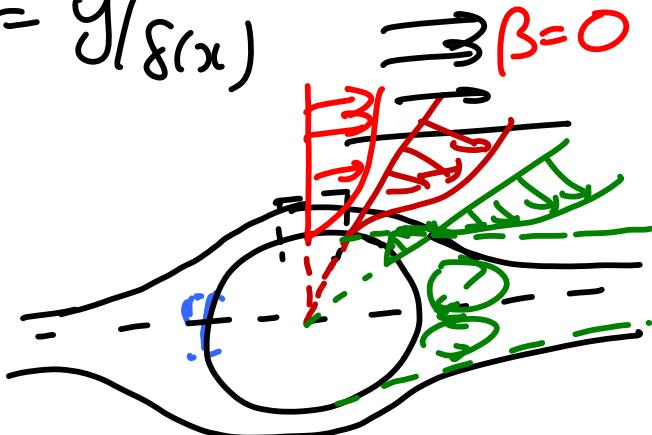
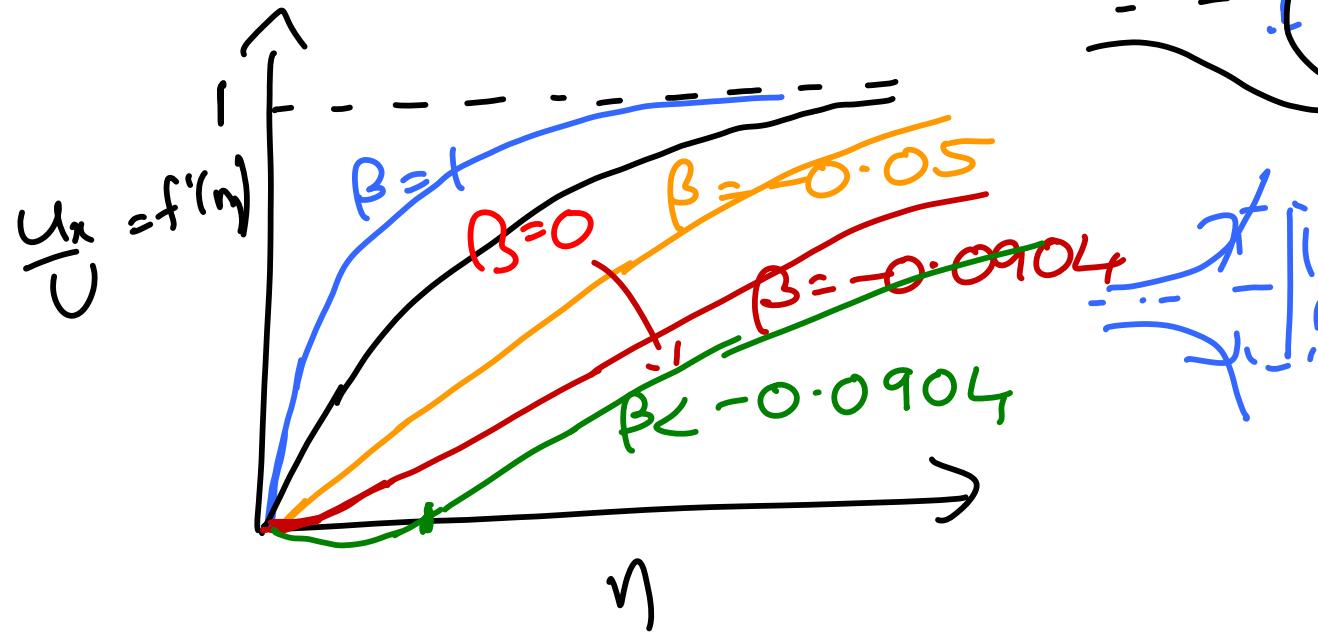
$$\delta = \left(\frac{Nx}{U(x)} \right)^{1/2}$$



$$\text{when } \beta = m - 1$$

$$\gamma = (SU) f(\eta) \quad \text{where} \quad \eta = y/\delta(x)$$

$$u_x = U(x) f'(\eta)$$



'Bluff bodies'

'Slender bodies'

Vorticity dynamics:

$$\omega_i = \epsilon_{ijk} \frac{\partial u_k}{\partial x_j}$$

$$\underline{\omega} = \nabla \times \underline{u} \quad \left| \int_C \underline{f} d\underline{x} \cdot \underline{y} = \int_C ds \underline{n} \cdot (\nabla \times \underline{y}) \right.$$

$$= \int_C ds \underline{n} \cdot \underline{\omega}$$

$$\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial p}{\partial x_i} + \left[N \frac{\partial^2 u_i}{\partial x_j^2} \right]$$



$$\frac{\partial u_i}{\partial t} + \frac{\partial}{\partial x_i} \left(\frac{1}{2} u_j^2 \right) - \left[\epsilon_{ijk} u_j \omega_k \right]$$

$$= -\frac{1}{\rho} \frac{\partial p}{\partial x_i} - \left[N \epsilon_{ijk} \frac{\partial}{\partial x_j} \omega_k \right]$$

$$\epsilon_{ijk} \frac{\partial}{\partial x_j} \left[\frac{\partial u_k}{\partial t} + \left(\frac{\partial}{\partial x_k} \left(\frac{1}{2} u_i^2 \right) - \epsilon_{ikm} u_i \omega_m \right) \right] = -\frac{1}{\rho} \frac{\partial p}{\partial x_k} + \left[N \frac{\partial^2 u_k}{\partial x_i^2} \right]$$

$$\epsilon_{ijk} \frac{\partial}{\partial x_j} \left(\frac{\partial u_k}{\partial t} \right) = \frac{\partial}{\partial t} \left(\epsilon_{ijk} \frac{\partial u_k}{\partial x_j} \right) = \frac{\partial \omega_i}{\partial t}$$

$$\epsilon_{ijk} \frac{\partial}{\partial x_j} \left(\frac{\partial}{\partial x_k} \left(\frac{1}{2} u_i^2 \right) \right) = 0$$

$$-\epsilon_{ijk} \frac{\partial}{\partial x_j} (\epsilon_{kcm} u_c w_m) = -\epsilon_{ijk} \epsilon_{kcm} \frac{\partial}{\partial x_j} (u_c w_m)$$

$$= -(\delta_{ic} \delta_{jm} - \delta_{im} \delta_{jc}) \frac{\partial}{\partial x_j} (u_c w_m)$$

$$= -\frac{\partial}{\partial x_j} (u_i w_j) + \frac{\partial}{\partial x_j} (u_j w_i)$$

$$= -w_j \frac{\partial u_i}{\partial x_j} - \cancel{u_i \frac{\partial w_j}{\partial x_j}} + u_j \frac{\partial w_i}{\partial x_j} + w_i \cancel{\frac{\partial u_j}{\partial x_j}}$$

$$= -w_j \frac{\partial u_i}{\partial x_j} + u_j \frac{\partial w_i}{\partial x_j}$$

$$-\epsilon_{ijk} \frac{\partial}{\partial x_j} \left(\frac{\partial p}{\partial x_k} \right) = 0$$

$$N \epsilon_{ijk} \frac{\partial}{\partial x_j} \left(\frac{\partial^2 u_k}{\partial x_i^2} \right) = N \frac{\partial^2}{\partial x_i^2} \left(\epsilon_{ijk} \frac{\partial u_k}{\partial x_j} \right)$$

$$= N \frac{\partial^2 w_i}{\partial x_i^2}$$

$$\left(\frac{\partial w_i}{\partial t} + u_j \frac{\partial w_i}{\partial x_j} \right) - \left(w_j \frac{\partial u_i}{\partial x_j} \right) = N \frac{\partial^2 w_i}{\partial x_j^2}$$

$$\frac{\partial w_i}{\partial t} = \boxed{w_j \frac{\partial u_i}{\partial x_j}} + \nu \frac{\partial^2 w_i}{\partial x_j^2}$$

$$\left(\frac{\partial \Delta x_i}{\partial t} \right) = \Delta x_i \cdot \nabla u$$

$$= \boxed{\Delta x_j} \frac{\partial u_i}{\partial x_j}$$

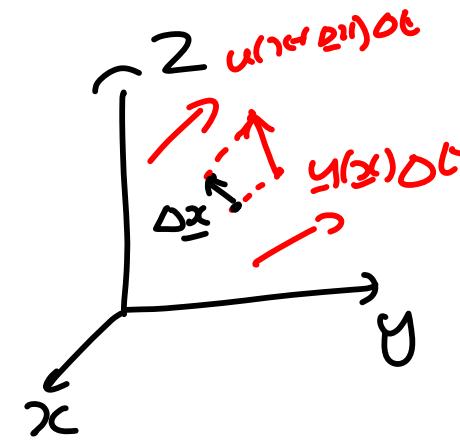
$$\frac{\partial w_i}{\partial t} = \boxed{w_j} \frac{\partial u_i}{\partial x_j}$$

$$w_j \frac{\partial u_i}{\partial x_j} = w_j (S_{ij} + A_{ij})$$

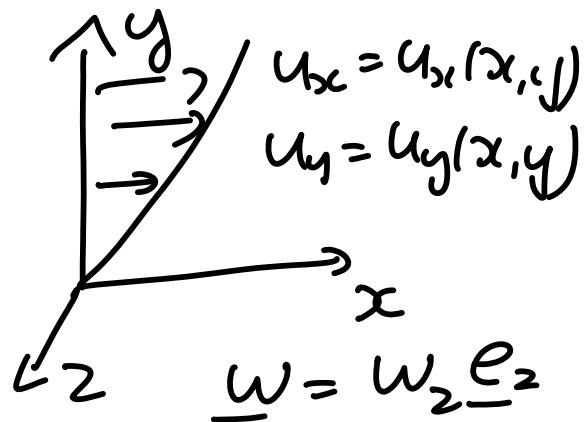
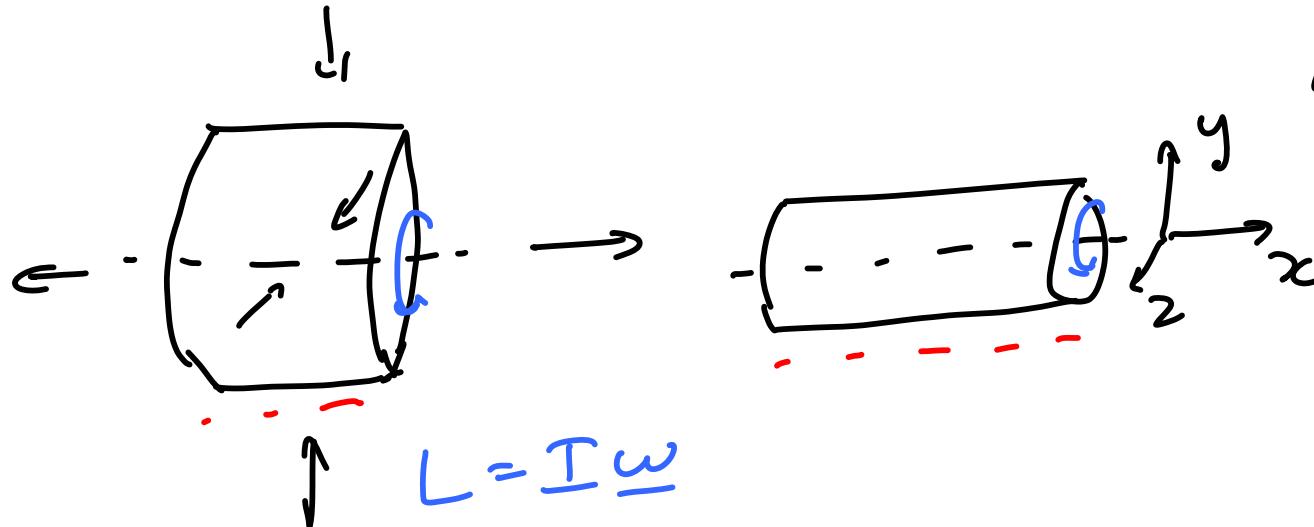
$$= w_j (S_{ij} - \frac{1}{2} \epsilon_{ijk} w_k)$$

$$= w_j S_{ij} - \cancel{\frac{1}{2} \epsilon_{ijk} w_k} w_j$$

$$= w_j S_{ij}$$



$$\frac{Dw_i}{Dt} = (\bar{w}_j - \bar{s}_{ij}) + N \frac{\partial^2 w_i}{\partial x_j^2}$$



$$\bar{w}_j - \bar{s}_{ij} = 0$$

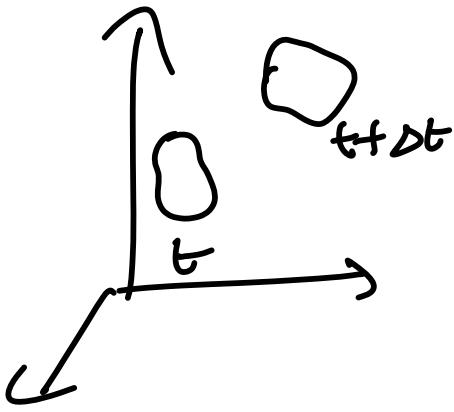
Vorticity $\underline{\omega} = \omega_x \underline{e}_x$

Kelvin's circulation theorem

$$\frac{d}{dt} \oint d\bar{x}_i \cdot \bar{u} = \frac{d}{dt} \oint dx_i u_i$$

$$= \oint dx_i \frac{Du_i}{Dt} + \int u_i dx_j \left(\frac{\partial u_i}{\partial x_j} \right)$$

- - -



$$\frac{d}{dt} \Delta x_i = \Delta x_j \frac{\partial u_i}{\partial x_j}$$

$$\begin{aligned} \frac{d}{dt} \oint dx_i \cdot u &= \oint dx_i \left(-\frac{1}{8} \cancel{\frac{\partial p}{\partial x_i}} + \nu \frac{\partial^2 u_i}{\partial x_j^2} \right) \\ &\quad + \oint dx_j \left(\cancel{\frac{\partial}{\partial x_j} \left(\frac{1}{2} u_i^2 \right)} \right) \\ &= \oint dx_i \left(\nu \frac{\partial^2 u_i}{\partial x_j^2} \right) \\ &= \oint dx_i \left(-\nu \epsilon_{ijk} \frac{\partial \omega_k}{\partial x_j} \right) \end{aligned}$$

Vorticity dynamics:

$$\underline{\omega} = \nabla \times \underline{u} \Rightarrow \omega_i = \epsilon_{ijk} \frac{\partial u_k}{\partial x_j}$$

$$\frac{\partial u_i}{\partial t} + \frac{\partial}{\partial x_i} \left(\frac{1}{2} u_j^2 \right) - \epsilon_{ijk} u_j \omega_k = - \frac{1}{\rho} \frac{\partial p}{\partial x_i} - \nu \epsilon_{ijk} \frac{\partial}{\partial x_j} \omega_k$$

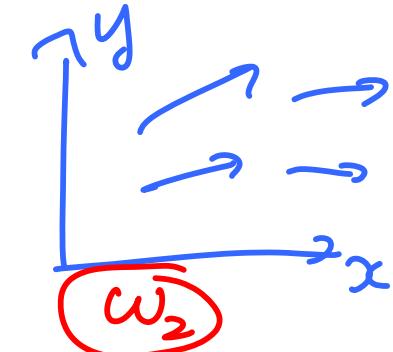
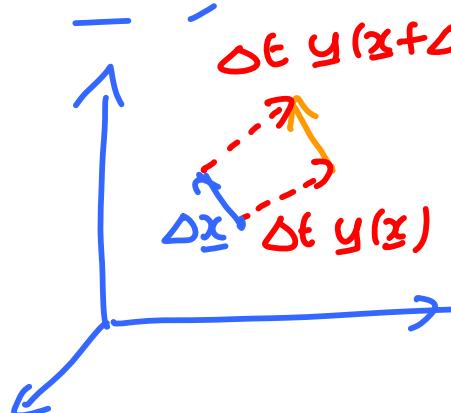
$$\frac{\partial \omega_i}{\partial t} + u_j \frac{\partial \omega_i}{\partial x_j} = \omega_i \frac{\partial u_i}{\partial x_j} + \nu \frac{\partial^2 \omega_i}{\partial x_j^2}$$

$$\frac{D \omega_i}{D t}$$

$$= \left[\omega_j \frac{\partial u_i}{\partial x_j} \right] + \left[\nu \frac{\partial^2 \omega_i}{\partial x_j^2} \right]$$

$$\frac{d(\rho \underline{x})}{dt} = \underline{\delta x} \cdot \nabla \underline{u}$$

$$\frac{d(\delta x_i)}{dt} = \delta x_j \frac{\partial (u_i)}{\partial x_j}$$



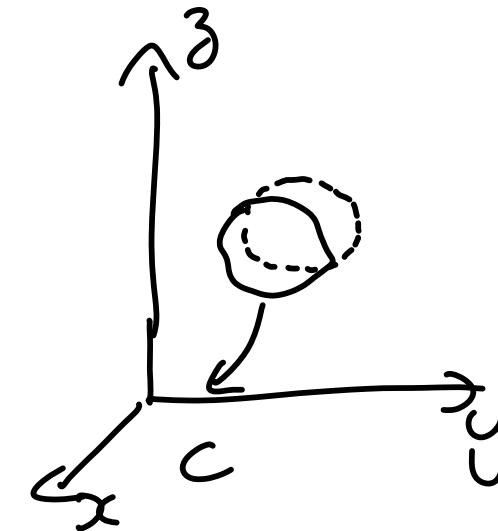
Kelvin's theorem:

$$\Gamma = \oint_C d\zeta \cdot \underline{u}$$

$$\frac{d\Gamma}{dt} = \frac{d}{dt} \left[\oint_C d\zeta \cdot \underline{u} \right]$$

$$= n \oint_C dx_i \left[\frac{\partial^2 u_i}{\partial x_j \partial z} \right]$$

$$= -n \oint_C dx_i \epsilon_{ijk} \frac{\partial}{\partial x_j} (\omega_k)$$

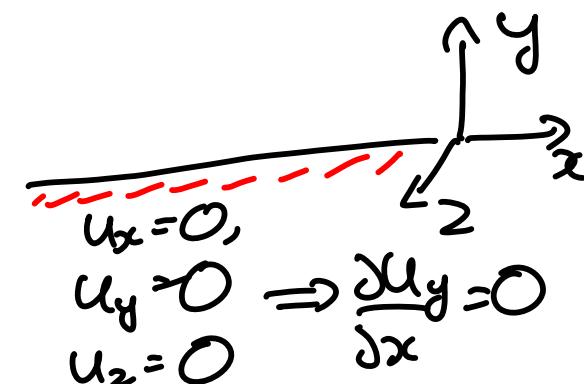


Shear stress at the wall

$$\tau_{xy} = \mu \left(\frac{\partial u_x}{\partial y} \right) = \mu \left(\frac{\partial u_x}{\partial y} - \frac{\partial u_y}{\partial x} \right)$$

$$= -\mu \underline{w}_2$$

$$F_x = \tau_{xy} n_y = -\mu n_y \underline{w}_2$$



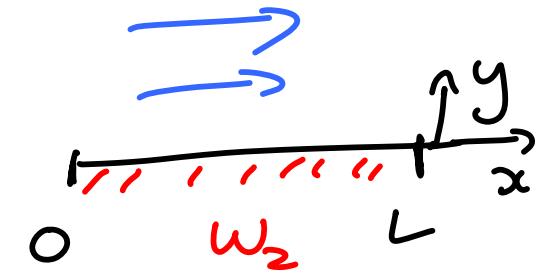
$$E_{vis} = -\mu \vec{v} \times \vec{\omega}$$

$$\int dx j_y^\omega =$$

$$f^\omega = -N \vec{v} \cdot \nabla \vec{w}$$

$$j_y^\omega = -\nu \frac{\partial w_2}{\partial y}$$

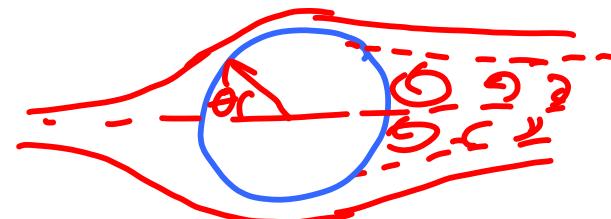
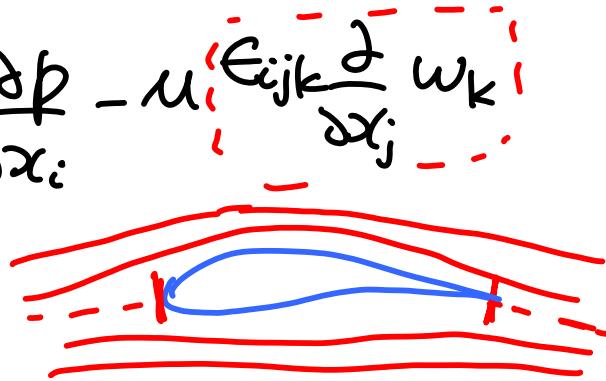
$$\cancel{\int \left(\frac{\partial u_i}{\partial x_i} + \frac{\partial}{\partial x_i} \left(\frac{1}{2} \delta u_i^2 \right) - \delta \epsilon_{ijk} u_j w_k \right)} = -\frac{\partial p}{\partial x_i} - \mu \left(\epsilon_{ijk} \frac{\partial w_k}{\partial x_i} \right)$$

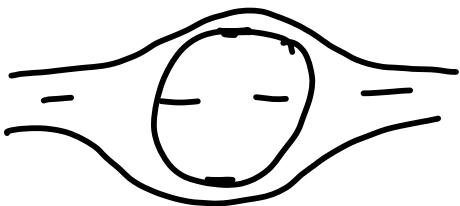
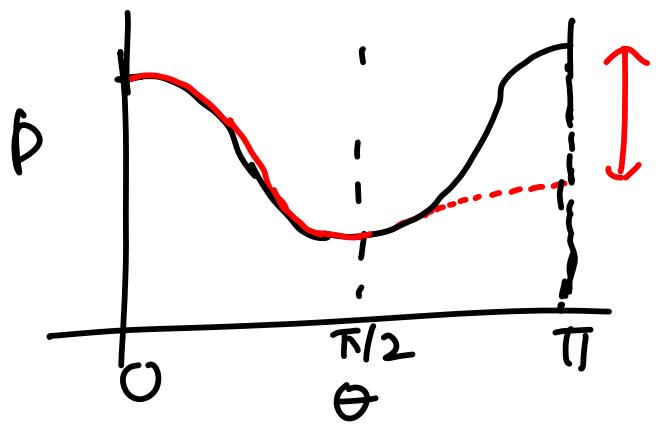


$$\frac{\partial p}{\partial x_i} = -\epsilon_{ijk} \mu \frac{\partial w_k}{\partial x_j}$$

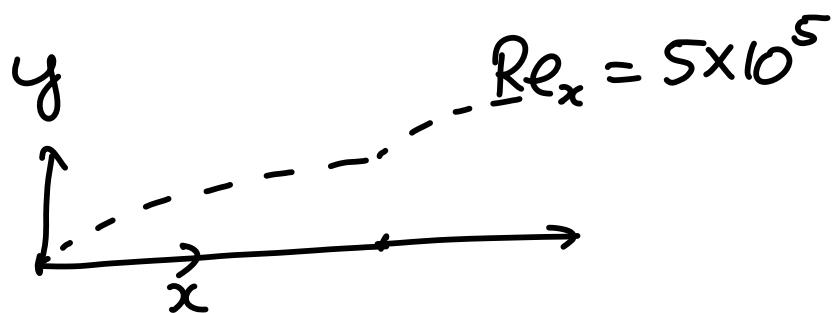
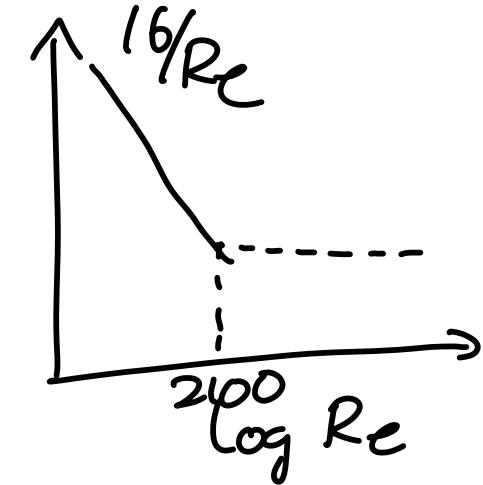
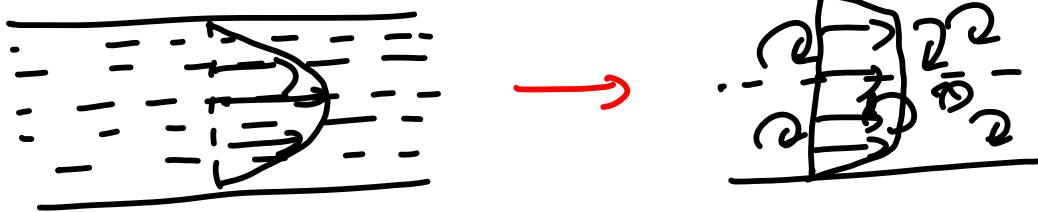
$$\frac{\partial p}{\partial x_j} = -\mu \frac{\partial w_2}{\partial y} = +\frac{\mu}{N} \tilde{j}_y^\omega = \delta j_y^\omega$$

$$\int_0^L dx j_y^\omega = \int_0^L dx \left(\frac{1}{S} \frac{\partial p}{\partial x} \right) = \frac{1}{S} \left[p(x=L) - p(x=0) \right]$$

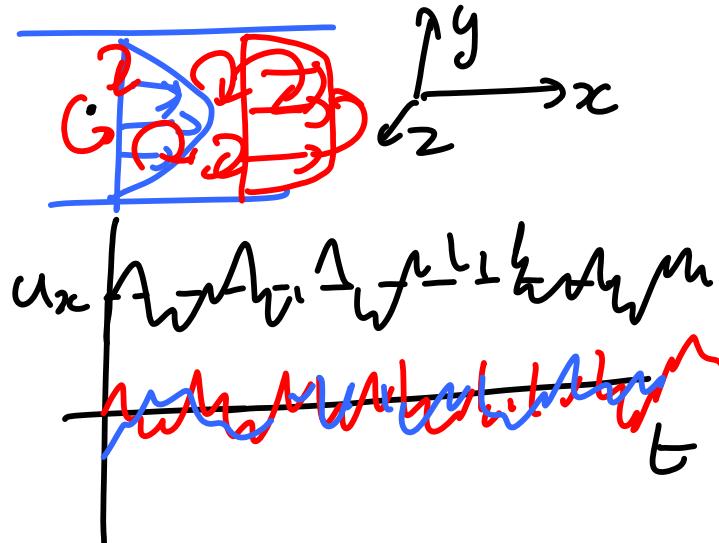
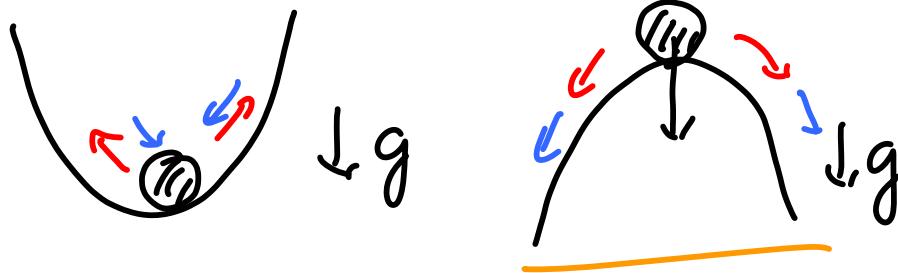




Turbulence:



Laminar profile goes unstable:



Turbulence:

- ① High Reynolds number
- ② Continuum
- ③ Irregular
- ④ Three-dimensional
- ⑤ Diffusive
- ⑥ Dissipation

$$D \propto \lambda \left(\frac{kT}{m} \right)^{1/2}$$

$$D_T \propto \frac{l u'}{---}$$

$$u_i = u_i + u_i'$$

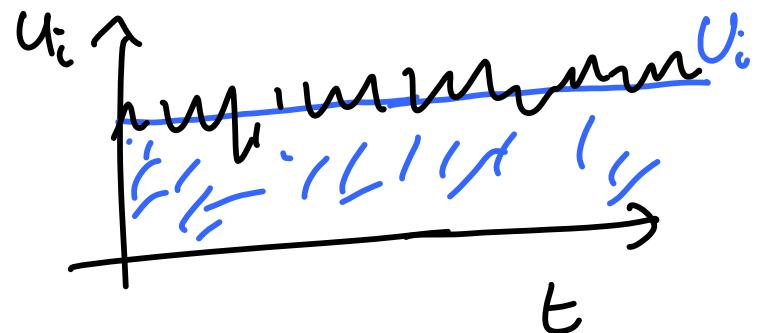
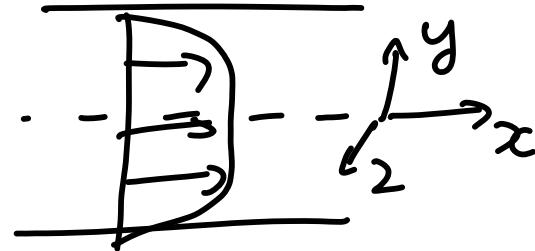
$$\langle \bar{u}_i \rangle = \frac{1}{T} \int_0^T dt \bar{u}_i = \langle u_i \rangle,$$

$$u_i' = u_i - \langle u_i \rangle$$

$$\langle u_i' \rangle = \frac{1}{T} \int_0^T dt u_i'$$

$$= \frac{1}{T} \int_0^T dt (u_i - \langle u_i \rangle) = \left[\frac{1}{T} \int_0^T dt u_i \right] - \langle u_i \rangle$$

$$= 0$$



Turbulence:

$$u_i = U_i + u'_i$$

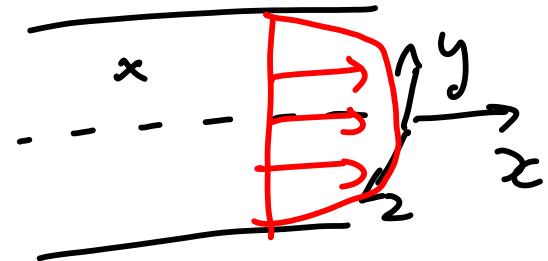
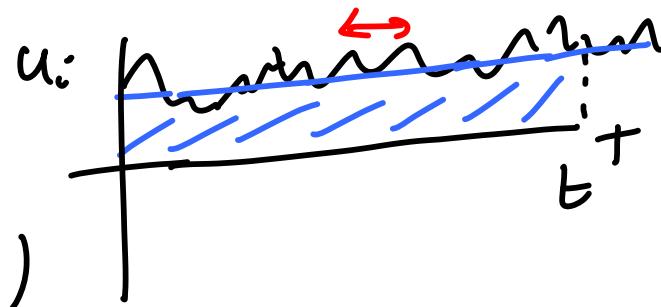
$$p = P + p'$$

$$U_i = \frac{1}{T} \int_0^T dt u_i = \langle u_i \rangle \quad P = \frac{1}{T} \int_0^T dt p$$

$$u'_i = u_i - U_i$$

$$\langle u'_i \rangle = \frac{1}{T} \int_0^T dt (u_i - U_i)$$

$$= 0$$



Mass conservation eqn:

$$\frac{\partial u_i}{\partial x_i} = 0 \Rightarrow \frac{\partial}{\partial x_i} (U_i + u'_i) = 0$$

$$\frac{1}{T} \int_0^T dt \left(\frac{\partial U_i}{\partial x_i} + \frac{\partial u'_i}{\partial x_i} \right) = 0 \Rightarrow \frac{\partial}{\partial x_i} \left[\frac{1}{T} \int_0^T dt U_i \right] + \frac{\partial}{\partial x_i} \left[\frac{1}{T} \int_0^T dt u'_i \right] = 0$$
$$\frac{\partial U_i}{\partial x_i} = 0$$

$$\frac{\partial}{\partial x_i} (U_i + U'_i) = 0 \implies \frac{\partial U'_i}{\partial x_i} = 0$$

$$\frac{\partial U_i}{\partial x_i} = 0 \quad \frac{\partial U'_i}{\partial x_i} = 0$$

$$S U_j \frac{\partial U_i}{\partial x_j} = - \frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_j} \bar{T}_{ij}$$

$$\bar{T}_{ij} = 2\mu e_{ij} = \mu \left(\frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right)$$

$$\langle T_{ij} \rangle = \mu \left(\frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right) \quad \bar{T}'_{ij} = \mu \left(\frac{\partial U'_i}{\partial x_j} + \frac{\partial U'_j}{\partial x_i} \right)$$

$$S(U_j + U'_j) \frac{\partial}{\partial x_j} (U_i + U'_i) = - \frac{\partial}{\partial x_i} (P + P') + \frac{\partial}{\partial x_j} (\langle T_{ij} \rangle + \bar{T}'_{ij})$$

$$S \left(U_j \frac{\partial U_i}{\partial x_j} + U_j \frac{\partial U'_i}{\partial x_j} + U'_j \frac{\partial U_i}{\partial x_j} + \underbrace{U'_j \frac{\partial U'_i}{\partial x_j}}_{= 0} \right)$$

$$= - \frac{\partial}{\partial x_i} (P + P') + \frac{\partial}{\partial x_j} (\langle T_{ij} \rangle + \bar{T}'_{ij})$$

$$u_j' \frac{\partial u_i'}{\partial x_j} = \frac{\partial}{\partial x_j} (u_i' u_j') - u_i' \left[\frac{\partial u_j'}{\partial x_j} \right]$$

$$\rho \left[u_j \frac{\partial u_i}{\partial x_j} + v_j \frac{\partial u_i'}{\partial x_j} + u_j' \frac{\partial u_i}{\partial x_j} + \left[\frac{\partial}{\partial x_j} (u_i' u_j') \right] \right] = - \frac{\partial P}{\partial x_i} - \frac{\partial p'}{\partial x_i} + \left[\frac{\partial}{\partial x_j} (\langle \tau_{ij} \rangle) + \frac{\partial}{\partial x_j} (\bar{\tau}_{ij}') \right]$$

$\int_0^T dt$

$$\rho u_j \frac{\partial u_i}{\partial x_j} + \rho \frac{\partial}{\partial x_j} \langle u_i' u_j' \rangle = - \frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_j} \langle \tau_{ij} \rangle$$

$$\langle u_i' u_j' \rangle = \frac{1}{T} \int_0^T dt u_i' u_j'$$

$$\begin{aligned} \rho u_j \frac{\partial u_i}{\partial x_j} &= - \frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_j} \langle \tau_{ij} \rangle - \frac{\partial}{\partial x_j} (\rho \langle u_i' u_j' \rangle) \\ &= - \frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_j} \langle \tau_{ij} \rangle + \frac{\partial}{\partial x_j} (T_{ij}^R) \end{aligned}$$

where $T_{ij}^R = - \rho \langle u_i' u_j' \rangle$ 'Reynolds stress'

$$T_{xy} = -S \langle u_x' u_y' \rangle$$

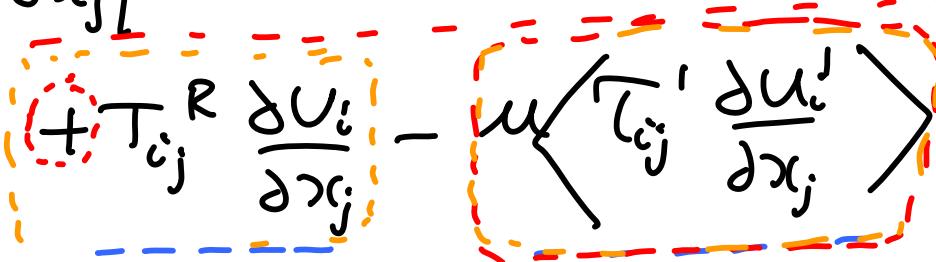
Momentum balance $\times U_i$

$$S U_i U_j \frac{\partial U_i}{\partial x_j} = -U_i \frac{\partial P}{\partial x_i} + U_i \frac{\partial}{\partial x_j} (\langle \tau_{ij} \rangle) + U_i \frac{\partial}{\partial x_j} (T_{ij}^R)$$

$$\begin{aligned} S U_j \frac{\partial}{\partial x_j} (U_i^2) &= -\frac{\partial}{\partial x_i} (P U_i) + P \cancel{\frac{\partial U_i}{\partial x_i}} \\ &\quad + \frac{\partial}{\partial x_j} [\langle \tau_{ij} \rangle U_i] - \langle \langle \tau_{ij} \rangle \frac{\partial U_i}{\partial x_j} \rangle \\ &\quad + \frac{\partial}{\partial x_j} (U_i T_{ij}^R) - \cancel{T_{ij}^R \frac{\partial U_i}{\partial x_j}} \end{aligned}$$

$$D = T_{ij} \frac{\partial U_i}{\partial x_j} \quad D^R = T_{ij}^R \frac{\partial U_i}{\partial x_j} = -S \langle U_i' U_j' \rangle \left(\frac{\partial U_i}{\partial x_j} \right)$$

Fluctuating energy = $\frac{1}{2} \beta \langle u_i'^2 \rangle$

$$8U_j \frac{\partial}{\partial x_j} \left(\frac{1}{2} \langle u_i'^2 \rangle \right) = - \frac{\partial}{\partial x_j} \left[\langle u_j' p' \rangle + \frac{1}{2} \langle u_i'^2 u_j' \rangle - 2\mu \langle u_i' \frac{\partial u_i'}{\partial x_j} \rangle \right]$$


Kolmogorov Equilibrium Hypothesis:

$$\epsilon \approx 8v^2 \left(\frac{v}{L}\right) \approx \frac{8v^3}{L}$$

$$\epsilon \approx \frac{v^3}{L} = L^2 T^{-3}$$

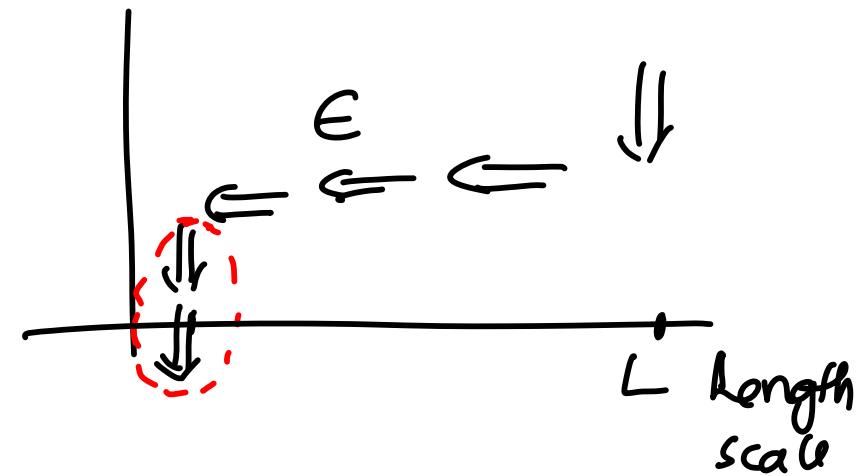
$$\nu \approx L^2 T^{-1}$$

Length scale $\eta = (\nu^3/\epsilon)^{1/4}$

Velocity scale $v = (\nu \epsilon)^{1/4}$

Time scale $\tau = (\nu/\epsilon)^{1/2}$

Kolmogorov scales.



Turbulent flows:

$$\nabla \cdot \underline{u} = 0$$

$$S\left(\frac{\partial \underline{u}}{\partial t} + \underline{u} \cdot \nabla \underline{u}\right) = -\nabla p + \nabla \cdot \underline{\tau}$$

$$\underline{U} = \frac{1}{T} \int_0^T dt \underline{u}$$

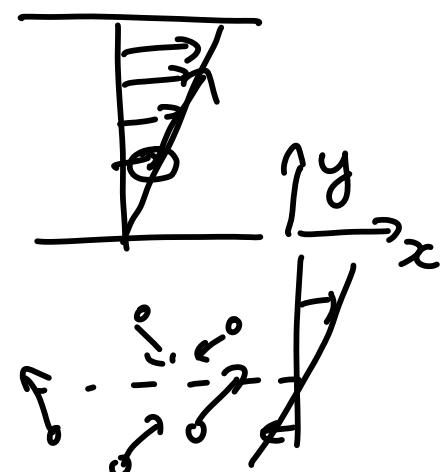
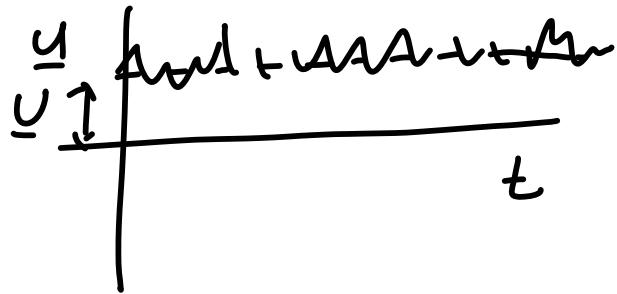
$$\underline{u}' = \underline{u} - \underline{U} \Rightarrow \langle \underline{u}' \rangle = \frac{1}{T} \int_0^T dt (\underline{u} - \underline{U}) = 0$$

$$\underline{u} = \underline{U} + \underline{u}' \quad p = P + p'$$

$$S \underline{U} \cdot \nabla \underline{U} = -\nabla P + \nabla \cdot \underline{\tau} + \nabla \cdot \underline{\tau}^R$$

$$S u_j \frac{\partial u_i}{\partial x_j} = -\frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_j} (\tau_{ij}) + \frac{\partial}{\partial x_j} (\tau_{ij}^R)$$

$$\underline{\tau}_{ij}^R = -S \langle u_i' u_j' \rangle \quad T_{xy} = -S \langle u_x' u_y' \rangle$$



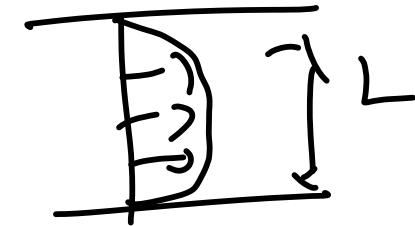
$$k = \frac{1}{2} S U_i^2 ; \quad k' = \frac{1}{2} S \langle U_i'^2 \rangle$$

$$S U_j \frac{\partial}{\partial x_j} \left(\frac{1}{2} U_i^2 \right) = \boxed{- \frac{\partial}{\partial x_i} (P U_i) + P \cancel{\frac{\partial U_i}{\partial x_i}} + \frac{\partial}{\partial x_j} (\langle T_{ij} \rangle U_i) - \langle T_{ij} \rangle \underline{\frac{\partial U_i}{\partial x_j}} + \frac{\partial}{\partial x_j} (T_{ij}^R U_i) - T_{ij}^R \left(\underline{\frac{\partial U_i}{\partial x_j}} \right)}$$

$$S U_j \frac{\partial}{\partial x_j} \left(\frac{1}{2} \langle U_i'^2 \rangle \right) = - \frac{\partial}{\partial x_j} \left[\langle U_j' p' \rangle + \frac{1}{2} \langle U_i'^2 U_j' \rangle - 2\mu \left\langle U_i' \frac{\partial U_i'}{\partial x_j} \right\rangle \right] + \underline{T_{ij}^R \frac{\partial U_i'}{\partial x_j}} - \underline{2\mu \left\langle \frac{\partial U_i'}{\partial x_j} \frac{\partial U_i'}{\partial x_j} \right\rangle}$$

Smallest turbulence scales:

'Kolmogorov universal equilibrium hypothesis'



$$S U_i \frac{\partial}{\partial x_i} \left(\frac{1}{2} U_i^2 \right) \equiv \frac{S U^3}{L}$$

$$P = \left(\frac{U^3}{L} \right) = \frac{L^2 T^{-3}}{L} \equiv \frac{\epsilon}{L}$$

$$\nu = L^2 T^{-1}$$

$$\eta = \left(\nu^3 / \epsilon \right)^{1/4} \quad \sigma = (\nu \epsilon)^{1/4} \quad \tau = (\nu / \epsilon)^{1/2} \quad] \text{ Kolmogorov scales}$$

$$\frac{\eta}{L} = \frac{1}{L} \left(\frac{\nu^3}{\epsilon} \right)^{1/4} = \left(\frac{\nu^3}{U^3 L^3} \right)^{1/4} = Re^{-3/4}$$

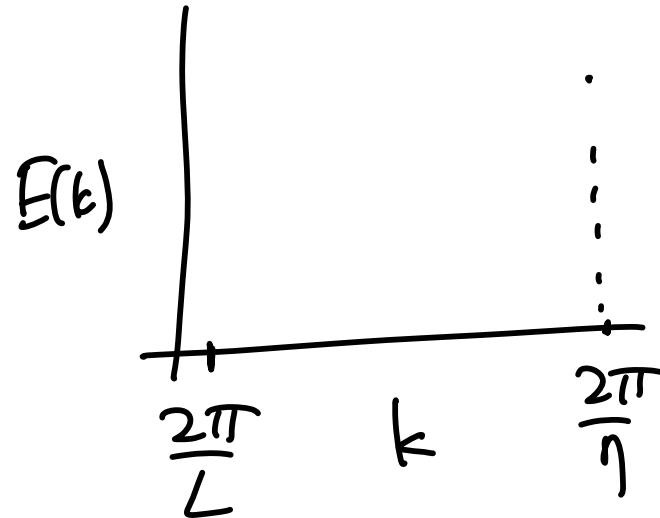
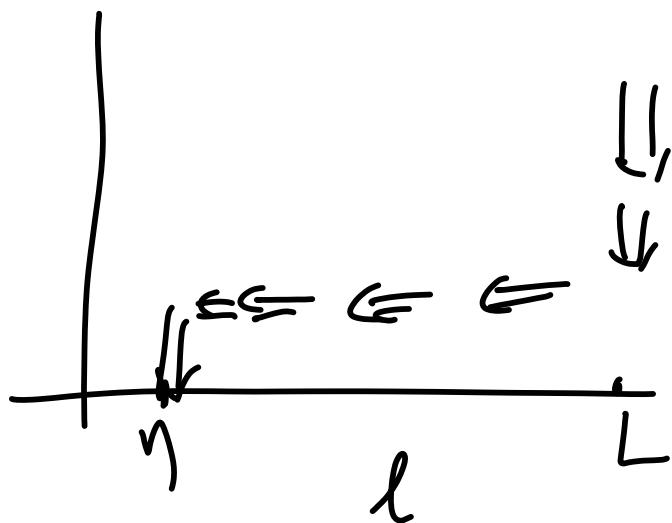
$$\frac{\sigma}{U} = \frac{1}{U} \left(\nu \epsilon \right)^{1/4} = Re^{-1/4}$$

$$S \approx \left(\frac{U}{\eta} \right) = \left(\frac{\epsilon}{\nu} \right)^{1/2} \quad \left| \frac{(U/\eta)}{(U/L)} = \left(\frac{\epsilon}{\nu} \right)^{1/2} \left(\frac{L}{U} \right) = Re^{+1/2} \right.$$

Dissipation rate $\propto \mu s^2$

$$\frac{\text{Dissipation rate (Kolmogorov)}}{\text{Dissipation Rate (Mean flow)}} = Re^{+1}$$

$$Re = \left(\frac{UL}{\nu} \right) \quad Re_k = \left(\frac{U\eta}{\nu} \right) = \frac{(U^3/\epsilon)^{1/4} (\nu\epsilon)^{1/4}}{\nu} \\ \equiv 1$$



Energy spectrum:

$$E \equiv L^2 T^{-2}$$

$$E(k) \approx L^3 T^{-2}$$

$$\underline{E} = \int dk E(k)$$

$k = \frac{2\pi}{\lambda}$ where λ = wavelength of fluctuations

$$E(k) = L^3 T^{-2} \equiv N^{5/4} \epsilon^{4/4} f(k\eta)$$

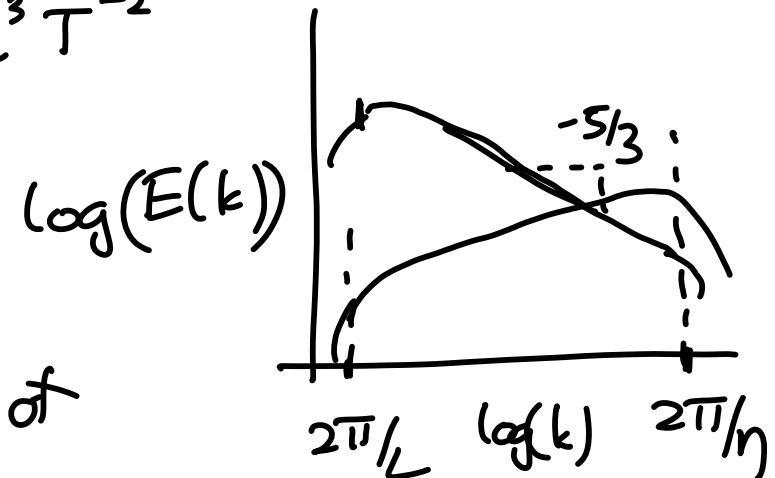
$$E(k) = U^2 L f(kL)$$

Inertial sub-range $E(k)$ depends only on $\epsilon \& k$

$$E(k) \propto \epsilon^{2/3} k^{-5/3}$$

$$D \propto \mu S^2 \propto \mu (U/c)^2 = \int dk D(k)$$

$$D(k) \equiv E(k)/L^2 \propto L T^{-2} \equiv \epsilon^{2/3} k^{+1/3}$$



K-E model:

$$\tau_{ij} = (\mu + \mu_t) \left(\frac{\partial u}{\partial x_j} + \frac{\partial u_i}{\partial x_i} \right)$$

$$\underline{\mu_t = \frac{8C_u k^2}{\epsilon}} = \underline{\underline{8C_u l u'}} = \underline{\underline{8C_u l^2 \left| \frac{\partial u}{\partial y} \right|}}$$

$$\frac{\partial}{\partial t} (8k) + \frac{\partial}{\partial x_j} (8u_j k) = \frac{\partial}{\partial x_j} \left[\left(\mu + \frac{\mu_t}{\sigma_k} \right) \frac{\partial k}{\partial x_j} \right] + P_k - 8\epsilon$$

$$\frac{\partial}{\partial t} (8\epsilon) + \frac{\partial}{\partial x_j} (8u_j \epsilon) = \frac{\partial}{\partial x_j} \left[\left(\mu + \frac{\mu_t}{\sigma_\epsilon} \right) \frac{\partial \epsilon}{\partial x_j} \right] + [C_\epsilon P_k(\epsilon/k)] - [C_{2\epsilon}] \frac{8\epsilon^2}{k}$$

$$P_k = \left(\mu + \underline{\mu_T} \right) \frac{\partial U_i}{\partial x_j} \left(\frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right)$$

$$= 2(\mu + \underline{\mu_T}) S_{ij}^2$$

$$C_u = 0.09; C_{1\epsilon} = 1.44, C_{2\epsilon} = 1.92, \sigma_k = 1.0$$

$$\sigma_\epsilon = 1.3$$

Turbulent flow in a channel:

$$U_j \frac{\partial U_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial P}{\partial x_i} + \nu \frac{\partial^2 U_i}{\partial x_j^2}$$

$$-\frac{\partial}{\partial x_j} (\langle u'_i u'_j \rangle)$$

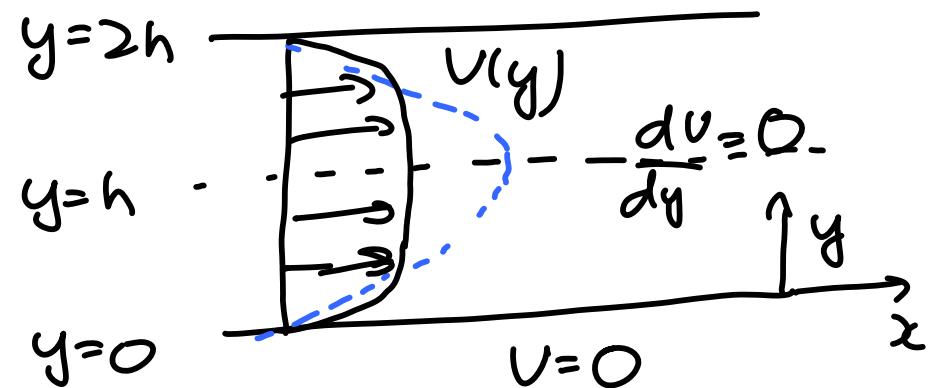
$$\cancel{U_x \frac{\partial U_x}{\partial x} + U_y \frac{\partial U_x}{\partial y}} = -\frac{1}{\rho} \frac{\partial P}{\partial x} + \nu \left[\frac{\partial^2 U_x}{\partial x^2} + \frac{\partial^2 U_x}{\partial y^2} \right]$$

$$-\frac{\partial}{\partial x} (\cancel{\langle u_x'^2 \rangle}) - \frac{\partial}{\partial y} (\langle u_x' u_y' \rangle)$$

$$-\frac{1}{\rho} \frac{\partial P}{\partial x} + \nu \frac{\partial^2 U}{\partial y^2} - \frac{\partial}{\partial y} (\langle u_x' u_y' \rangle) = 0$$

$$\cancel{U_x \frac{\partial U_y}{\partial x} + U_y \frac{\partial U_y}{\partial y}} = -\frac{1}{\rho} \frac{\partial P}{\partial y} + \nu \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) U_y$$

$$-\frac{\partial}{\partial x} (\cancel{\langle u_x' u_y' \rangle}) - \frac{\partial}{\partial y} (\cancel{\langle u_y'^2 \rangle})$$



$$-\frac{1}{\rho} \frac{\partial P}{\partial y} - \frac{\partial}{\partial y} \left[\langle u_y'^2 \rangle \right] = 0$$

$$-\frac{1}{\rho} \frac{\partial P}{\partial x} + \nu \frac{\partial^2 u_x}{\partial y^2} - \frac{\partial}{\partial y} \left(\langle u_x' u_y' \rangle \right) = 0$$

$$\frac{P}{\rho} + \frac{1}{2} \langle u_y'^2 \rangle = \frac{P_0}{\rho} \quad P_0 = \text{wall pressure}$$

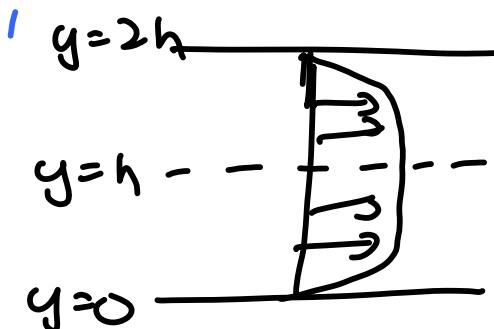
$$\frac{1}{\rho} \frac{\partial P}{\partial x} + \frac{\partial}{\partial x} \left(\frac{1}{2} \langle u_y'^2 \rangle \right) = \frac{1}{\rho} \frac{\partial P_0}{\partial x}$$

$$\frac{\partial P}{\partial x} = \frac{\partial P_0}{\partial x}$$

$$-\frac{1}{\rho} \frac{\partial P_0}{\partial x} + \nu \frac{\partial^2 u_x}{\partial y^2} - \frac{\partial}{\partial y} \left(\langle u_x' u_y' \rangle \right) = 0$$

$$-\frac{1}{\rho} \frac{\partial P_0}{\partial x} + \nu \frac{\partial u_x}{\partial y} - \overline{\langle u_x' u_y' \rangle} - \overline{\langle u_y'^2 \rangle} = 0$$

Take value of this equation at $y=0$



$$+ \nu \frac{\partial U_x}{\partial y} - U_*^2 = 0$$

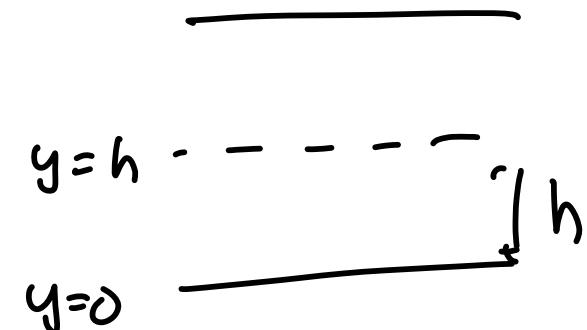
$$\rho U_*^2 = \nu \frac{\partial U_x}{\partial y} = T_{xy}$$

U_* = Friction velocity

Take value of this equation at $y=h$

$$-\frac{h}{g} \frac{\partial P_0}{\partial x} + \nu \frac{\partial U_x}{\partial y} - \langle U_x' U_y' \rangle - U_*^2 = 0$$

$$U_x^2 = -\frac{h}{g} \frac{\partial P_0}{\partial x} \Rightarrow \underline{\underline{\frac{\partial P_0}{\partial x}}} = -\frac{g}{h} U_*^2$$



$$-\langle U_x' U_y' \rangle + \nu \frac{\partial U_x}{\partial y} = U_*^2 (1 - y/h)$$

$$y^* = (y/h)$$

$$-\frac{-\langle U_x' U_y' \rangle}{U_*^2} + \frac{\nu}{U_*^2} \frac{\partial U_x}{h \partial y^*} = (1 - y^*)$$

$$-\frac{\langle u_x' u_y' \rangle}{u_*^2} + \left(\frac{N}{u_* h}\right) \frac{\partial}{\partial y^*} \left(\frac{U_x}{U_*} \right) = 1 - y^*$$

$$\left(-\frac{\langle u_x' u_y' \rangle}{u_*^2} \right) + \left(Re_*^{-1} \frac{\partial}{\partial y^*} \left(\frac{U_x}{U_*} \right) \right) = 1 - y^*$$

$$y^+ = \left(\frac{y}{N} \frac{u^*}{u_*} \right) \Rightarrow y = \frac{Ny^+}{u_*}$$

$$-\frac{\langle u_x' u_y' \rangle}{u_*^2} + \frac{N}{u_*^2} \frac{\partial U_x}{\partial y} = \left(1 - \left(y/h \right) \right)$$

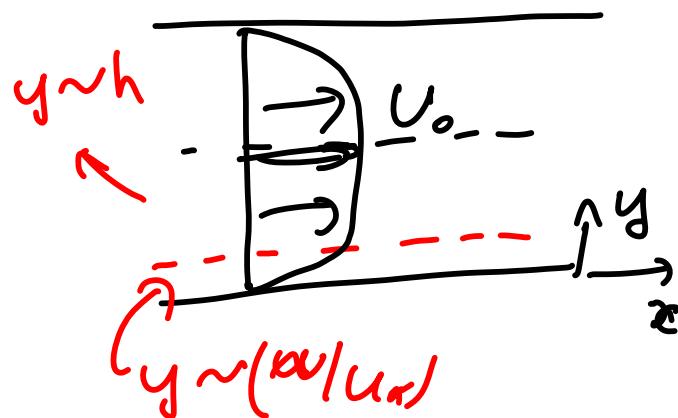
$$-\frac{\langle u_x' u_y' \rangle}{u_*^2} + \frac{\partial (U_x/u_*)}{\partial y^+} = \left(1 - \frac{N}{u_* h} y^+ \right)$$

$$\left(-\frac{\langle u_x' u_y' \rangle}{u_*^2} \right) + \left(\frac{\partial (U_x/u_*)}{\partial y^+} \right) = \left(1 - Re_*^{-1} y^+ \right)$$

$$\frac{dU_x}{dy} = \left(\frac{u_*}{h} \right) \frac{dF(y^+)}{dy^+}$$

$\left[\frac{U_{x_c} - U_0}{u^*} = F(y^+) \right]$

Core of
channel.
 $y \approx h$



$$\frac{dU_x}{dy} = \frac{u_*}{(\nu/u_x)} \frac{df(y^+)}{dy^+} = \frac{u_*^2}{\nu} \frac{df}{dy^+}$$

Wall layer $y \approx (\nu/u_x)$

$$\left[\frac{U_{x_c}}{u_*} = f(y^+) \right]$$

Intermediate region $\nu/u_* \ll y \ll h$

$$y^* = Re_*^{-1}$$

y^*

$$y^* = y/h \ll 1$$

$$y^+ = (y/\nu) \gg 1$$

$$\frac{dU_x}{dy} = \frac{u_*}{h} \frac{dF}{dy^*} = \frac{u_*^2}{\nu} \frac{df}{dy^+}$$

$$y^* \frac{dF}{dy^*} = y^+ \frac{df}{dy^+} = \frac{1}{K}$$

$$K=0.4 \Rightarrow \frac{1}{K}=2.5$$

$$A=5 \quad B=-1$$

$$F = \frac{1}{K} \log(y^*) + B = \left[\frac{U_x - U_0}{U_*} \right]$$

$$f(y^+) = \frac{1}{K} \log(y^+) + A = \left[\frac{U_x}{U_*} \right]$$

$$\frac{U_0}{U_*} = \frac{1}{K} \log(Re_*) + A - B$$

$$\frac{U_0}{U_*} = 2.5 \log(Re_*) + 0.6$$

$$F = 2.5 \log(y^*) - 1 ; f = 2.5 \log(y^+) + 5$$